

**Open File Report 1994 - 16A**

**Aquifer Disposal of  
CO<sub>2</sub> - Rich Gases**

**Phase 1**

**ALBERTA DEPARTMENT OF ENERGY  
AQUIFER DISPOSAL OF CO<sub>2</sub>-RICH GASES**

**MARCH, 1993**

# AQUIFER DISPOSAL OF CO<sub>2</sub>-RICH GASES

Phase I

IN THE VICINITY OF THE SUNDANCE  
AND GENESEE POWER PLANTS

Injectivity, Chemical Reactions, and Proof of Concept

by

W.D. Gunter  
E.H. Perkins  
S. Bachu  
D. Law  
B. Wiwchar  
Z. Zhou

Alberta Research Council

and

T.J. McCann

Stanely Industrial Consultants Ltd.

C-1993-5

March 1993

## DISCLAIMER

This report was prepared as an accounting of work conducted by the Alberta Research Council (ARC). Every possible effort was made to ensure that the work conforms to accepted scientific practice. However, neither ARC, nor any of its employees, makes and warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any of the information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process or services by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favouring by the ARC. The views and opinions of authors expressed herein do not necessarily state or reflect those of the ARC.

## TABLE OF CONTENTS

	<u>Page</u>
Table of Contents	ii
Acknowledgement and Disclaimer	v
Executive Summary	vi
Acknowledgements	ix
<b>1.0 INTRODUCTION</b>	<b>1-1</b>
1.1 GENERAL	1-1
1.2 STUDY TEAM	1-2
<b>2.0 SYSTEM OVERVIEW</b>	<b>2-1</b>
2.1 SETTING	2-1
2.2 SOURCES	2-4
2.3 PURIFICATION AND PRESSURIZING	2-4
2.4 FIELD FACILITIES	2-7
2.4.1 DISTRIBUTION PIPELINE	2-7
2.4.2 WELL SYSTEMS	2-8
2.4.2.1 SURFACE FACILITIES	2-8
2.4.2.2 INJECTION WELLS	2-10
2.4.2.3 MONITORING WELLS	2-13
2.5 SYSTEM COSTS	2-13
2.5.1 ESTIMATES	2-13
2.5.1.1 INTRODUCTION	2-13
2.5.1.2 FIELD FACILITY INVESTMENT COSTS	2-14
2.5.1.3 FIELD OPERATING COSTS	2-21
2.5.2 SYSTEM DEVELOPMENT	2-22
2.5.2.1 GEOLOGICAL AND GEOPHYSICAL DEVELOPMENT	2-22
2.5.2.2 EXTERNAL RELATIONS	2-22
2.5.2.3 LAND ACQUISITION	2-22
2.5.2.4 PROJECT COORDINATION	2-23
2.5.3 COST SUMMARY	2-23
2.6 ENVIRONMENTAL FACTORS	2-24
<b>3.0 REGIONAL GEOLOGY</b>	<b>3-1</b>
3.1 GENERAL	3-1
3.2 AQUIFER PETROPHYSICS	3-3

## TABLE OF CONTENTS

	<u>Page</u>	
3.3	AQUIFER FORMATION WATER CHEMISTRY	3-6
3.4	AQUIFER FORMATION MINERALOGY	3-7
<b>4.0</b>	<b>NUMERICAL SIMULATION OF AQUIFER INJECTABILITY</b>	<b>4-1</b>
4.1	DESCRIPTION OF NUMERICAL SIMULATOR	4-1
4.2	PHYSICAL PROPERTIES OF THE AQUIFER	4-3
4.3	INJECTION STRATEGIES	4-6
4.4	INJECTIVITY OPTIMIZATION	4-6
<b>5.0</b>	<b>MODELLING OF CO<sub>2</sub> RESERVOIR REACTIONS</b>	<b>5-1</b>
5.1	PREAMBLE	5-1
5.2	FORMATION WATER CHEMISTRY ADJUSTMENTS	5-2
5.3	MODELLING OF WATER-ROCK REACTION	5-4
5.4	CO <sub>2</sub> SOLUBILITY IN BRACKISH WATER AND IN BRINE	5-6
5.5	CO <sub>2</sub> SOLUBILITY IN CARBONATE AQUIFERS	5-7
5.6	CO <sub>2</sub> SOLUBILITY IN SILICICLASTIC AQUIFERS	5-14
<b>6.0</b>	<b>VALIDATION OF GEOCHEMICAL MODELLING</b>	<b>6-1</b>
6.1	EXPERIMENTAL DESIGN	6-1
6.2	PRODUCT EXAMINATION	6-3
6.3	KINETICS	6-10
6.4	VALIDATION	6-11
<b>7.0</b>	<b>CONCLUSIONS</b>	<b>7-1</b>
7.1	SYSTEM OVERVIEW	7-1
7.2	AQUIFER OVERVIEW	7-1
7.3	NUMERICAL SIMULATION OF AQUIFER INJECTABILITY	7-1
7.4	MODELLING OF CO <sub>2</sub> RESERVOIR REACTIONS	7-2
7.5	VALIDATION OF GEOCHEMICAL MODELLING	7-3
<b>8.0</b>	<b>RECOMMENDATIONS</b>	<b>8-1</b>
<b>BIBLIOGRAPHY</b>		

## TABLE OF CONTENTS

### APPENDICES

(These are filed with the Alberta Department of Energy)

11.3.1	CORED INTERVALS FOR AQUIFERS OF INTEREST
11.3.2	FORMATION WATER ANALYSES FOR AQUIFERS OF INTEREST
11.3.3	X-RAY DIFFRACTOGRAMS OF AQUIFER MINERALOGY
11.4.1	THERMAL AQUIFER MODEL
11.5.1	GRAPHS GENERATED FROM PATH.UBC OUTPUT
11.5.2	PAPER PRESENTED AT IEA CONFERENCE "CARBON DIOXIDE DISPOSAL"
11.6.1	X-RAY DIFFRACTOGRAMS OF MINERAL REACTANTS
11.6.2	X-RAY DIFFRACTOGRAMS OF REACTION PRODUCTS

## **ACKNOWLEDGEMENT AND DISCLAIMER**

The research project for which this report is submitted was funded in part from the Government of Alberta through the Alberta Office of Coal Research and Technology, Alberta Department of Energy.

This report and its contents, the project in respect of which it is submitted and the conclusions and recommendations arising from it do not necessarily reflect the view of the Government of Alberta, its officers, employees or agents; or the Board of Directors of the Alberta Office of Coal Research and Technology.

Neither the Government of Alberta, its officers, employees or agents nor the Board of Directors of the Alberta Office of Coal Research and Technology, its agents and consultants make any warranty, express or implied, representation or otherwise, in respect of this report or its contents.

The Government of Alberta, its officers, employees and agents and the Alberta Office of Coal Research and Technology, its agents and consultants are exempt, excluded and absolved from all liability for damage for injury, howsoever caused, to any person in connection with or arising out of the use by that person for any purpose of this report or its contents.

The partial funding by Energy, Mines and Resources Canada, Environment Canada, Edmonton Power and TransAlta Utilities Corporation is also acknowledged with thanks. The foregoing clauses are also applicable to those agencies and companies.

The underlying work, conclusions and statements of this study are those of the authors and may not be in agreement with the views of the governments of Alberta and/or Canada, and/or Edmonton Power and/or TransAlta Utilities Corporation.

## EXECUTIVE SUMMARY

### 1. **Aquifers are Important Candidates for CO<sub>2</sub> Disposal**

Currently there is considerable interest in using geological structures (salt domes, brines, coal beds, oil and gas reservoirs, or aquifers), the deep ocean or enhanced oil recovery as sinks for disposal of CO<sub>2</sub>. In the short term, enhanced recovery projects can utilize CO<sub>2</sub> if these projects are near the CO<sub>2</sub> source. However in the longer term, deep aquifers appear to offer the best promise for accepting large quantities of waste gases. Their global distribution and their large *disposal volume* are appealing for disposal of waste fluids or gases, particularly from point emission sources. Carbon dioxide is an ideal candidate for aquifer disposal because of its high density and high solubility in water at the relatively high pressures which may be imposed in aquifers.

### 2. **Aquifer Disposal Pipelines and Wells Small Part of Total CO<sub>2</sub> Disposal Cost**

Aquifer disposal of CO<sub>2</sub> from a site in the Alberta (geologic) Basin containing over two-thirds of Alberta's coal-based electricity generation (i.e. Wabamun, Sundance, Keephills and Genesee power plants) was examined. A coal based power plant with 500 MW of net electricity output and a 30 year life (used as a base case) will generate close to 15,000 tons of CO<sub>2</sub> a day. The CO<sub>2</sub> would be injected as a liquid using a distribution system of 15 disposal wells, with each well accepting 1,000 tons per day. The analysis indicates that capture and compression facilities are the major disposal costs. The CO<sub>2</sub> transfer pipelines and disposal and monitoring well system will have a capital cost in the order of \$2,200 per tonne per day of disposal capacity. However, the aquifer disposal system represents only a small portion of the overall CO<sub>2</sub> capture, purification and compression costs - capital and operating.



### **3. The Alberta Basin Aquifers Can Accept CO<sub>2</sub> Generated by 500 MW Plant**

Over a 30 year period, 0.16 Gt (i.e. gigatons) of CO<sub>2</sub> would be produced from a 500MW coal-fired power plant. Carbonate (i.e. Wabamun) and siliciclastic (Lower Mannville) aquifers were identified in this study area in the Alberta Basin capable of accepting well above this quantity of CO<sub>2</sub>. Modelling of injection into these aquifers concluded that disposal of 1000 tons/well of CO<sub>2</sub> was obtainable.

### **4. The Best CO<sub>2</sub> Traps are Mineral Traps**

Concern about the stability of the long term capture of CO<sub>2</sub> has been addressed. Conventional wisdom has restricted the disposal of CO<sub>2</sub> to the subsurface where there are stratigraphic traps. In what we think is a novel approach, we advocate the consideration of mineral traps in aquifers. Modelling of geochemical reactions between CO<sub>2</sub>-charged water and aquifer mineralogy clearly identified siliciclastic aquifers as capable of trapping large quantities of CO<sub>2</sub> by the precipitation of calcium-magnesium carbonate minerals. These conclusions are general and may be applied to any aquifer. These ideas were presented at the March 1993 IEA Carbon Dioxide Disposal Symposium at Oxford, England. The full context of the paper is contained in Appendix 11.5.2.

### **5. Aquifer Disposal should be Viewed from the Framework of a Sedimentary Basin**

These mineral trapping reactions are kinetically very slow; but given the low regional flow rates (i.e. approximately 2 cm/year) and the large size of the Alberta Basin, the CO<sub>2</sub> would be hydraulically trapped for thousands of years; ample time for the mineral CO<sub>2</sub> trapping reactions to take place. Thus CO<sub>2</sub> disposal in aquifers should be focused on the regional flow in the siliciclastic aquifers in sedimentary basins not on sedimentary traps. The paradigm of mineral trapping, identified in this report, increases tremendously the potential volumes of the subsurface available for CO<sub>2</sub> disposal.

**6. More Detailed Studies of Aquifer Disposal is Warranted**

This study has shown that the potential of subsurface CO<sub>2</sub> capture is very large for certain types of aquifers in the Alberta Basin. This study's extensive mineral reaction work is to be strongly promoted, but further work on long term reaction kinetics is needed to more fully define the increased CO<sub>2</sub> capture potential now indicated. Further geotechnical and geochemical work is essential to fully define the suitability of local aquifers and to select those most appropriate. As a first of a kind project, environmental control specifications, permitting, well design and system optimization will be extensive before an injection system can be put in place.

## **ACKNOWLEDGEMENTS**

Ian Webster, IEA was a great help in identifying and helping with sources of potential funding for this project. Wayne Nesbitt, University of Western Ontario assisted with the clay-exchange calculations and the kinetic data. Daryl Wightman selected the core samples for us during a trip to ERCB. Finally we would like to thank our sponsors and their representatives on the management committee - Alberta Energy (D.E. Macdonald), Environment Canada (V.R. Marwaha), CANMET (F.M. Mourits), TransAlta (M.M. McDonald and D. Drysdale), and Edmonton Power (Doug Heaton).

## 1.0 INTRODUCTION

### 1.1 GENERAL

Currently, there is considerable interest in using geological structures (salt domes, brines, coal beds, oil and gas reservoirs, or aquifers), the deep ocean or enhanced oil recovery as sinks for disposal of waste gas, particularly CO<sub>2</sub>. In the short term, enhanced recovery projects can utilize CO<sub>2</sub> if these projects are near the CO<sub>2</sub> source. However in the longer term, deep aquifers appear to offer the best promise for accepting large quantities of waste gases. Their global distribution and their large *disposal volume* are appealing for disposal of waste fluids or gases, particularly from point emission sources. Carbon dioxide is an ideal candidate for aquifer disposal because of its high density and high solubility in water at the relatively high pressures which may be imposed in aquifers.

This report summarizes experimental and desk studies relative to the potential for CO<sub>2</sub> disposal in certain aquifers in the Lake Wabamun area. The bulk of the effort was expended by the Alberta Research Council in examining the reactions between CO<sub>2</sub> and formation waters and minerals likely present in the specific aquifers.

This study has been financed by the Alberta Office of Coal Research and Technology (50%), Environment Canada (16.5%), Energy, Mines and Resources Canada (16.5%), TransAlta Utilities Corporation (8.5%) and Edmonton Power (8.5%). The latter two companies operate coal-based power plants with a total capacity nearing 4000 MW of net electrical output in the study area, with very major CO<sub>2</sub> capture and disposal potential.

The preliminary results of this study were reported at the Oxford University CO<sub>2</sub> disposal conference organized by the International Energy Agency's Greenhouse Gas Program. During the latter part of the study reported here, the study team carried out a preliminary study on aquifer disposal potential and its costs for the IEA. Each study has contributed to

the other, and the facilities descriptions and costs of this study have been taken from the IEA study, but made specific to the Lake Wabamun area.

The study discussed here was planned as a first phase of a multi-phase program to develop an accurate appraisal of CO<sub>2</sub> disposal costs in the Lake Wabamun area. Further work will be required on many geological aspects in order to select and define a specific aquifer, and to define all facilities needed from power plant flue gas through to the aquifer.

## 1.2 STUDY TEAM

The study team was organized as follows:

- T.J. McCann, SICL Study Manager
- R.B. Ramsay, SICL SICL Facilities
- W.D. Gunter, ARC ARC Coordination, Geochemistry
- E.H. Perkins, ARC Geochemistry
- S. Bachu, ARC (Alberta Geological Survey) Geology
- D. Law, ARC Modelling
- B. Wiwchar, ARC Autoclave Experiments
- Z. Zhou, ARC Mineral Characterization

The team reported to the Owner's Group through a managing committee of Alberta Department of Energy's D.E. Macdonald, Environment Canada's V.R. Marwaha, CANMET's F.M. Mourits, TransAlta's M. McDonald and D. Drysdale, and Edmonton Power's D. Heaton.

## **2.0 SYSTEM OVERVIEW**

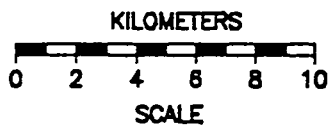
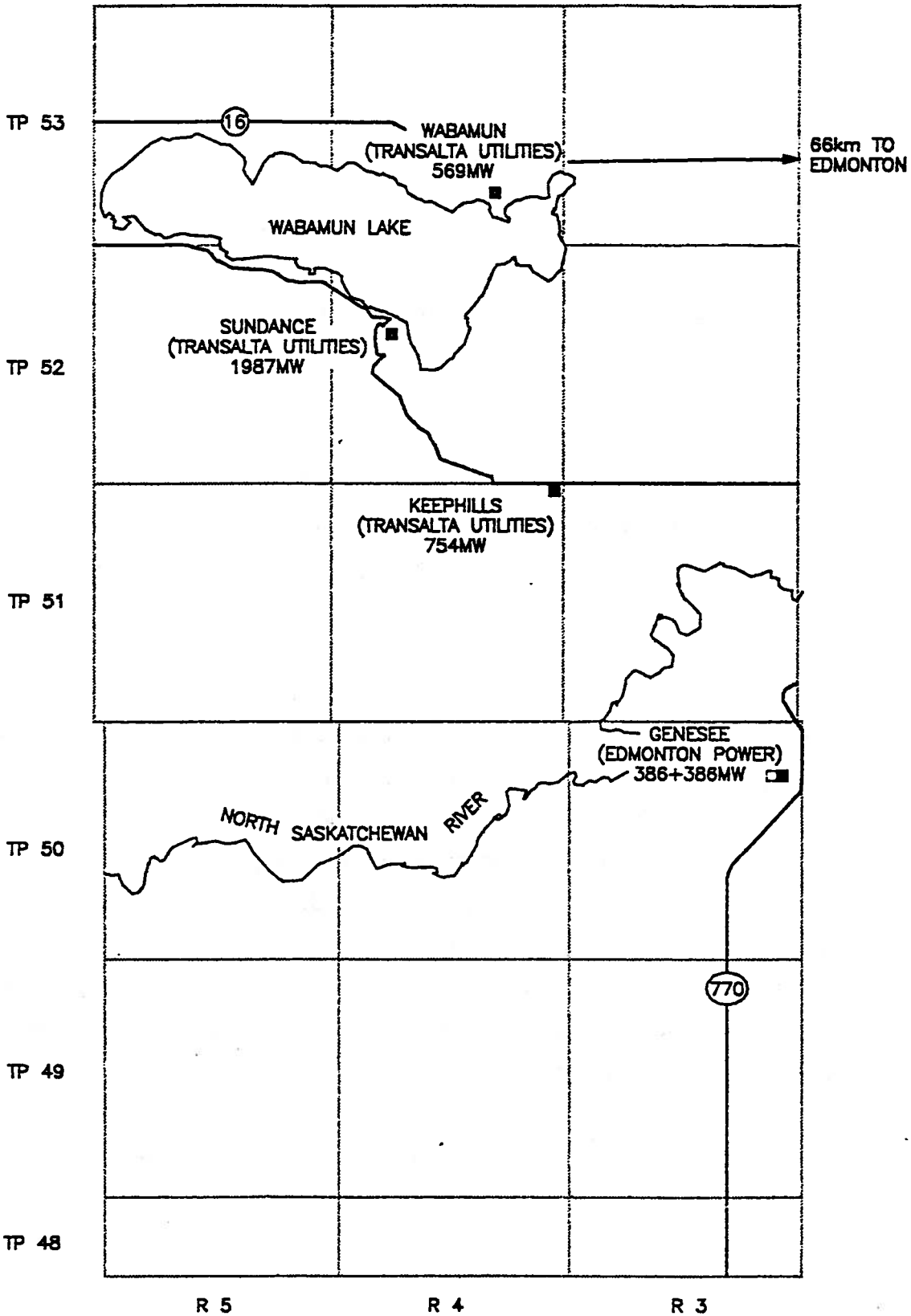
### **2.1 SETTING**

The study area shown in Figure 2.1-1 was selected due to the presence of over two-thirds of Alberta's coal-based electricity generation. The area lies in the western Canadian sedimentary basin which contains many aquifers assumed to be suitable for CO<sub>2</sub> disposal.

While the study examined different types of aquifers, the facility data are based on use of the Lower Mannville aquifer formation as shown in Table 3.2 below. The Wabamun formation was also considered in reaction work as a representative of a carbonate aquifer as compared to a siliciclastic aquifer in the Lower Mannville.

The capital costs of a field disposal system are minor compared to those of an overall CO<sub>2</sub> disposal scheme at a major power plant. Figure 2.1-2 provides a possible configuration assuming a chemical absorption approach to CO<sub>2</sub> capture. In the scheme shown, the impurities carried over from the CO<sub>2</sub> capture process are eliminated prior to CO<sub>2</sub> disposal. This minimizes corrosion potential and enhances the density and partial pressure of the CO<sub>2</sub> in the formation. The former is very important in determining the quantity of CO<sub>2</sub> in the supercritical vapour phase (still two-thirds of stored CO<sub>2</sub> 10 years after injection ceases) and the latter is important in determining the amount of dissolved CO<sub>2</sub> (a slight decrease in solution CO<sub>2</sub> is evident in Figure 4.1-7 after CO<sub>2</sub> injection ceases and pressure declines as the pressure bulb continues to spread).

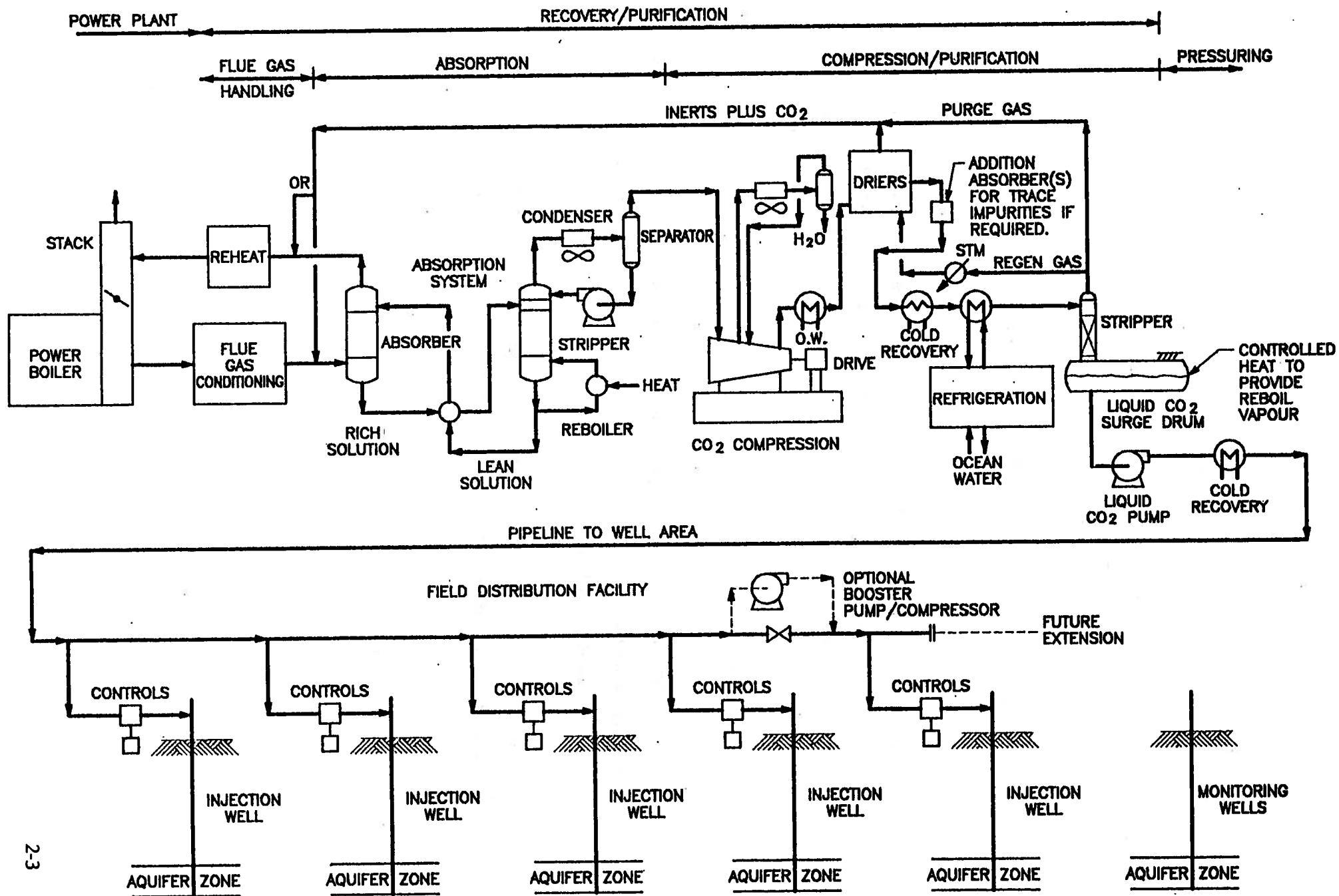
An injection rate of 1,000 tpd per well has been assumed at a station pressure of 21000 kPa.



**LEGEND**

- COAL BASED GENERATING PLANTS
  - OPERATING
  - IN CONSTRUCTION
- (770) — HIGHWAYS

**ALBERTA STUDY AREA**



OVERALL CO<sub>2</sub> DISPOSAL SCHEME  
FIGURE 2.1-2



## **2.2 SOURCES**

The sizes of the power plants in the study area are shown in Figure 2.1-1. The study area contains over two-thirds of the province's coal-based electricity generation with net capacity nearing 4000 MW. 500 MW of net electricity generation results in approximately 13,000 tonnes per day of CO<sub>2</sub> after correction for internal needs for CO<sub>2</sub> capture and production of a raw CO<sub>2</sub> gas stream near atmospheric pressure.

The addition of CO<sub>2</sub> compression and impurity removal itself requires in the order of 50 MW of electricity or equivalent, raising the CO<sub>2</sub> production to the order of 14,000 tpd (4.0 million tonnes a year) for 500 MW of sales to the provincial electrical grid. Thus, 15,000 tonnes per day appears to be a reasonable figure for preliminary system definition.

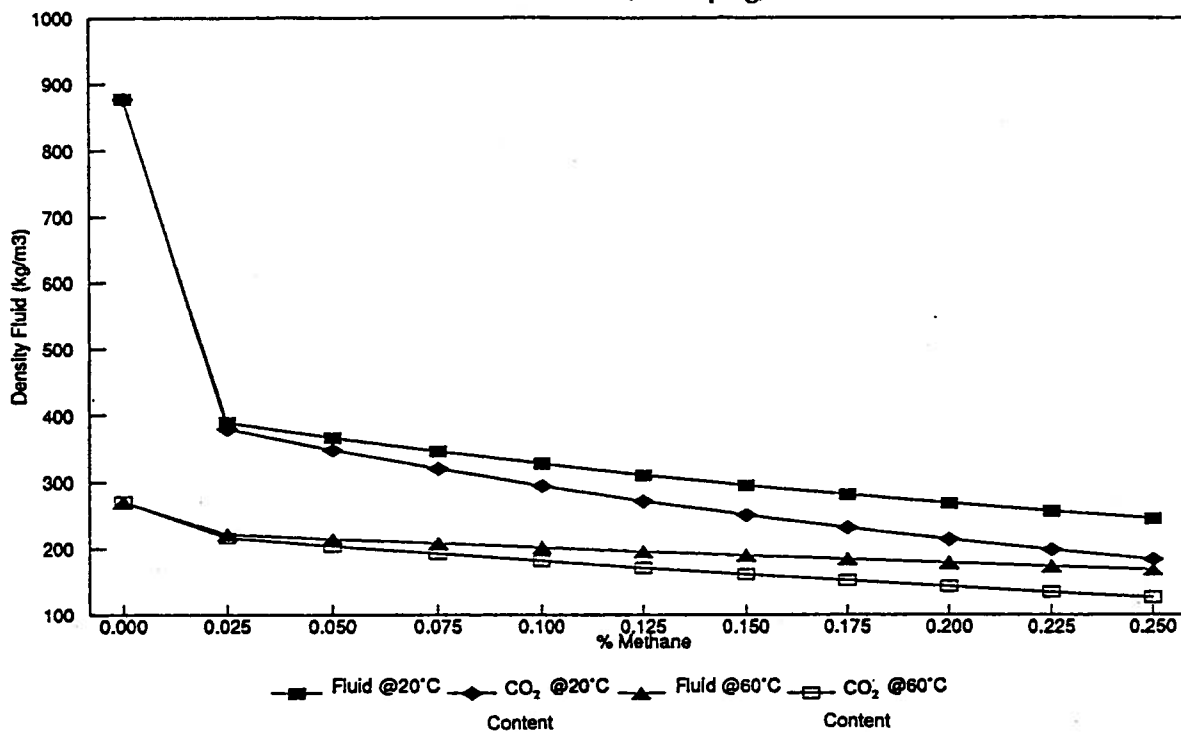
## **2.3 PURIFICATION AND PRESSURIZING**

The above CO<sub>2</sub> rates allow for compression of the CO<sub>2</sub> to the 21000 kPa level required for local aquifer disposal. Figure 2.1-2 shows a possible system including an ability to reduce impurities to a very low level.

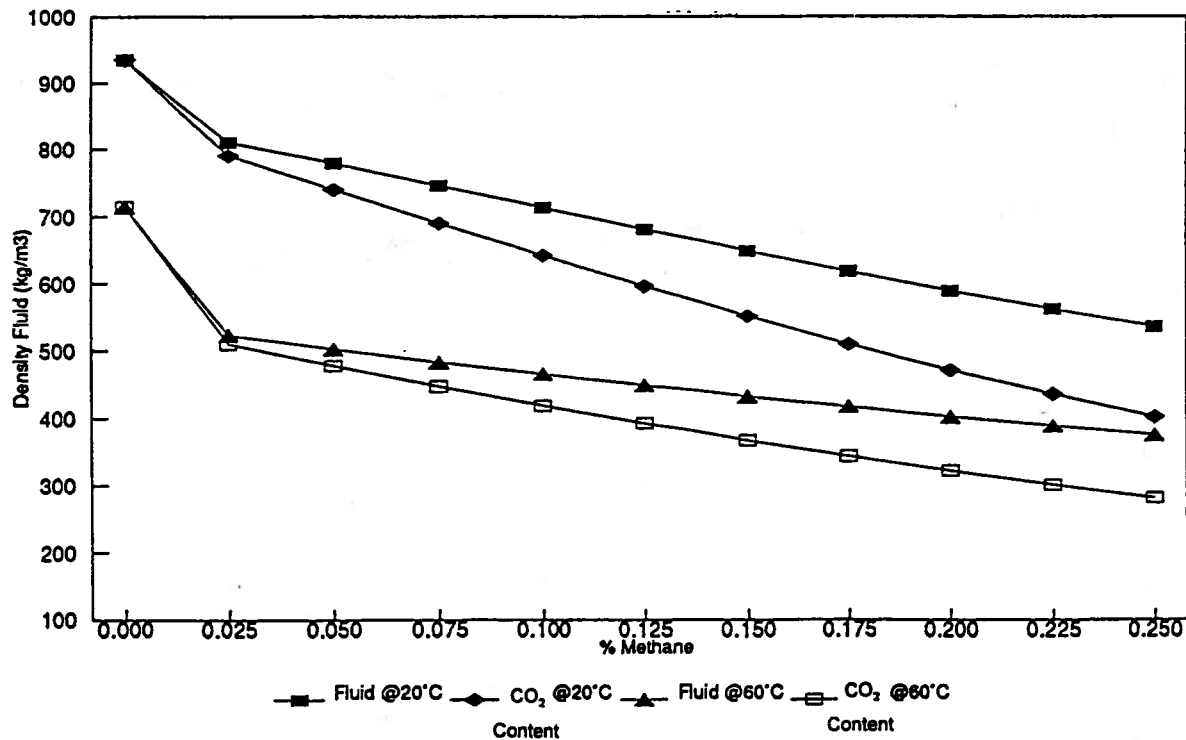
Figures 2.3-1 and 2.3-2 indicate the major impact on CO<sub>2</sub> density and, hence, on volumetric storage needs when traces of nitrogen and methane are present.

Figure 2.3-1  
Impacts of Methane

Density Profile with Changing CH<sub>4</sub> Impurity  
9660 kPa (1400 psig)

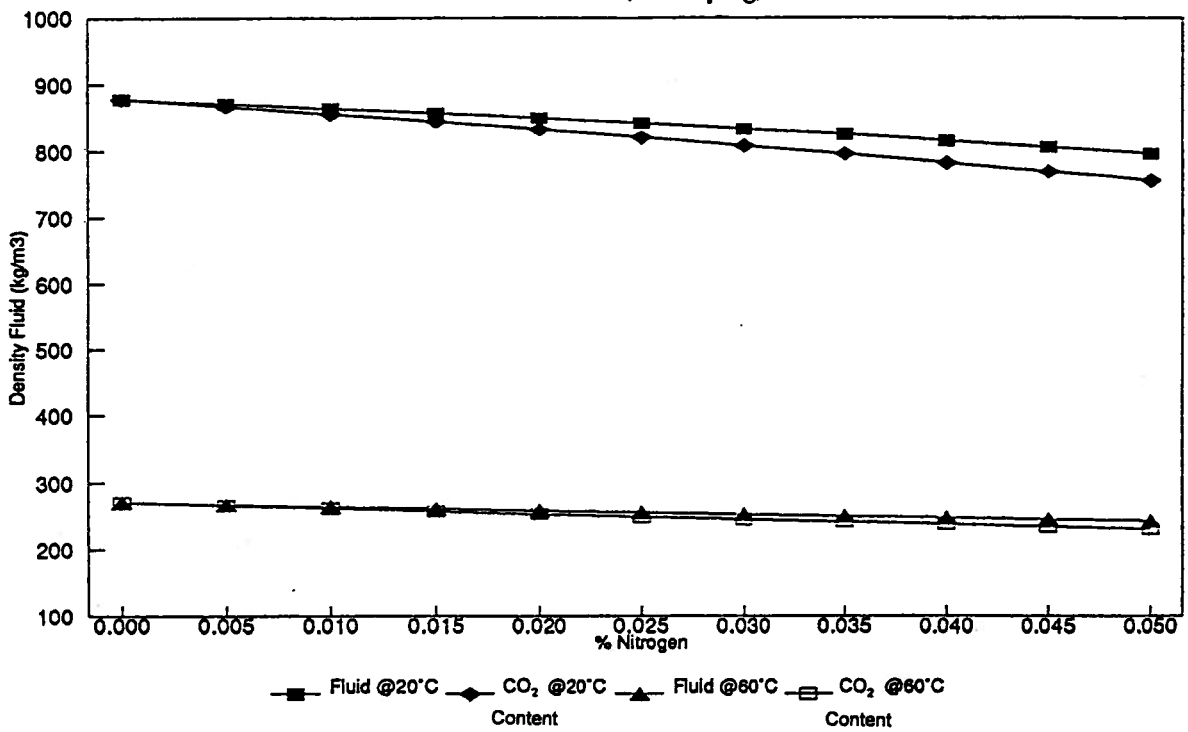


Density Profile with Changing CH<sub>4</sub> Impurity  
19320 kPa (2800 psig)

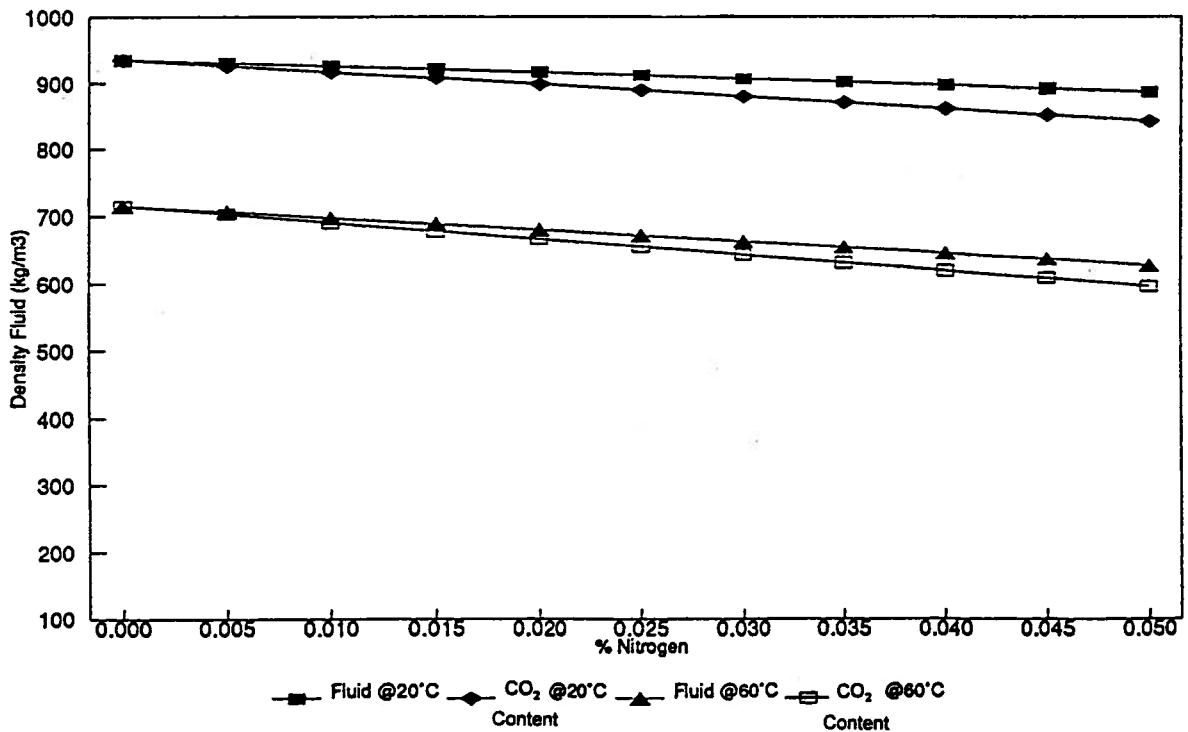


**Figure 2.3-2**  
**Impacts of Nitrogen**

**Density Profile with Changing N<sub>2</sub> Impurity**  
**9660 kPa (1400 psig)**



**Density Profile with Changing N<sub>2</sub> Impurity**  
**19320 kPa (2800 psig)**



The impact is greatest in the well as the "liquid" head is greatly reduced with impurities - requiring much more compression at the station end. One major reason for past use of pure liquid CO<sub>2</sub> in oil and gas well fracturing was its high density - about that of water - minimizing pumping horsepower. There will also be increased pipeline costs when significant impurities are present as line sizes must be increased.

The capture system shown is typical of that used at many breweries and chemical plants, but is for illustration only; there are many optional routes. In such schemes, liquid CO<sub>2</sub> may best be transferred using reciprocating pumps (as proven in well fracturing).

The purification and pressurization system appears to be quite expensive, possibly in the order of \$150 million in capital, broken into 4 or 5 trains. (Flue gas conditioning, CO<sub>2</sub> capture and plant derating costs must be added to that.) As noted above, pressurization is a very major energy user. The compression step is also a major energy user - in the order of 80 kWh/tonne.

## **2.4 FIELD FACILITIES**

### **2.4.1 DISTRIBUTION PIPELINE**

The pipeline itself will be designed to the equivalent of the U.S. ANSI B31.4 or Canadian CSA Z183 oil pipeline specifications, using all provisions for high vapour pressure liquid/supercritical fluid service (as with ethylene and ethane). These codes have different provisions for two areas of different population densities; here "Zone 1" (rural) of the CSA specification will be used.

A corrosion allowance would be added due to the possibility of moisture being present at some stage in the pipelines' life, tentatively 1.6 mm for the line and 3.2 for associated vessels. The depth of cover will vary with the specific code used and nature of the

surrounding area, but a minimum burial of 1 metre is recommended in all areas to protect from farm and other machinery on the surface. Special attention and additional burial in casing will be needed at road and railway crossings to match codes and the risk of freeze bulbs from line breaks.

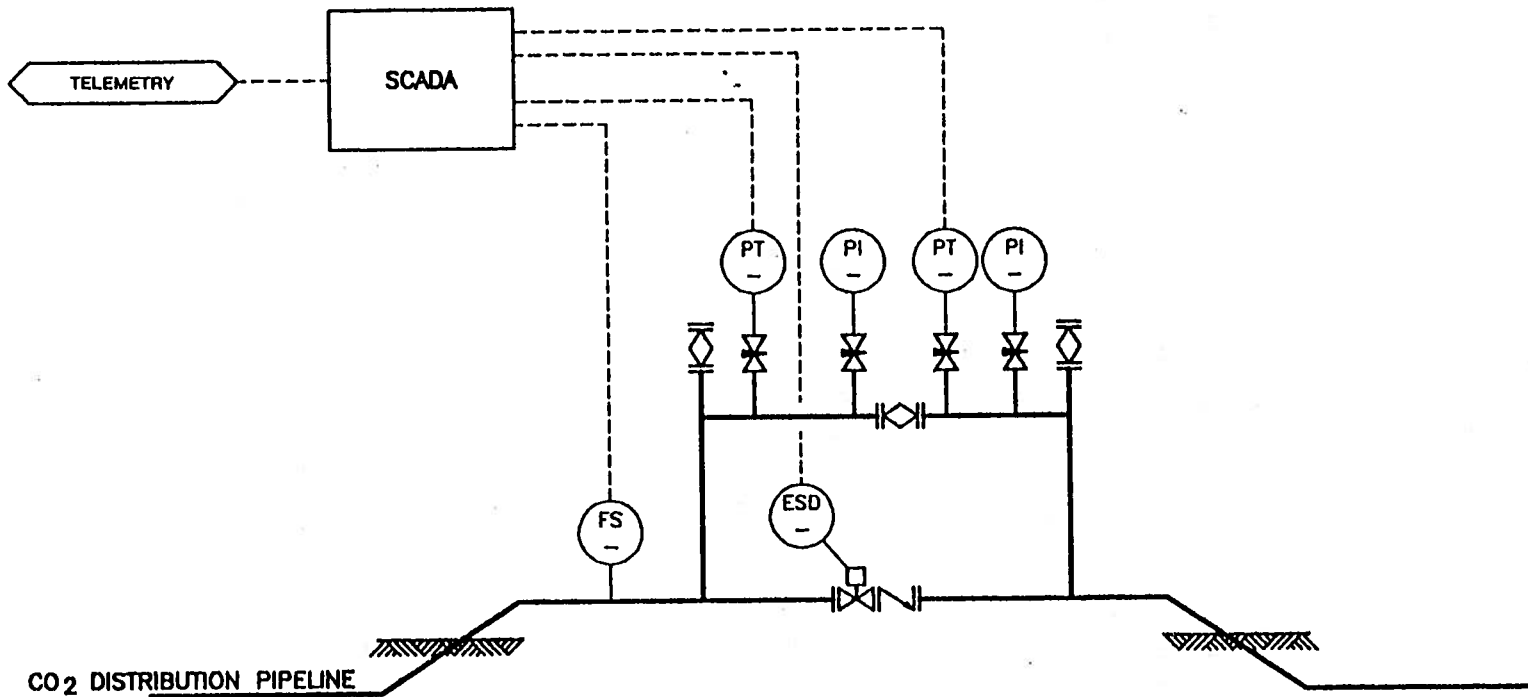
The pipeline will have automated block valves - as illustrated in Figure 2.4-1 - at a maximum spacing of 15 kilometres, on both sides of all river crossings, at major road and rail crossings, and at all transitions from one population zone to another. A SCADA system will regularly scan all valve positions and analyze pressures and flows throughout the system. A pipeline rupture will immediately block in the affected area and the system in general upstream of controls to individual wells.

The line will be sign posted as per normal pipeline practice, and all neighbours will be given educational sessions and literature, and will serve as unofficial monitors. All surface facilities, such as shutdown valves, will have locked, fenced enclosures. Spacing from houses, factories, etc., will follow the applicable codes. The use of high vapour pressure hydrocarbon standards will provide a margin of safety, but the heavy CO<sub>2</sub> vapour/solid from any line break will stay much closer to the ground than will high vapour hydrocarbons.

## **2.4.2 WELL SYSTEMS**

### **2.4.2.1 SURFACE FACILITIES**

The piping at the wells will be equipped as shown in Figure 2.4.2-1. A wellsite ESD valve will provide safety protection in case of a failure; this valve may be activated either locally or remotely through the SCADA system. A filter, with 5 micron elements, will ensure that particulate matter which could otherwise damage the well is removed from the CO<sub>2</sub> stream.

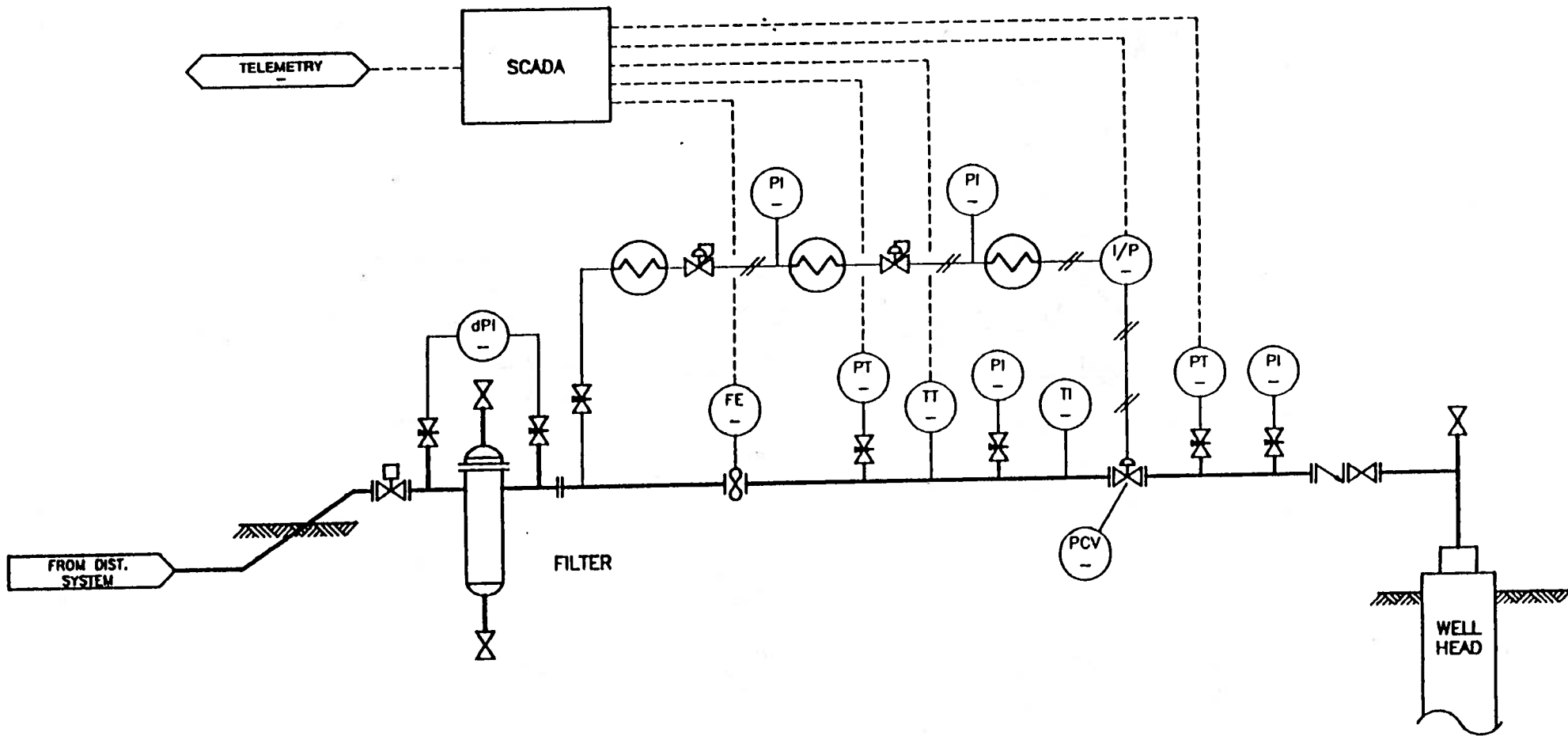


TYPICAL AUTOMATED  
BLOCK VALVE STATION  
FIGURE 2.4-1

The meter measures the quantity of CO<sub>2</sub> being injected, and, via the SCADA system, provides the means to check for material balance for line break control. Pressure and temperature transmitters also form an integral part of the material balance instrumentation and monitor flowing conditions at the well. A control valve accepts signals via the SCADA system to apportion the total system flow to each well as required. This valve is also required for start-up of the injection, and to maintain a back-pressure for proper operation of the flow meter. A discharge check valve is provided for safety, to avoid back-flow production of previously injected CO<sub>2</sub> in an emergency situation. Local SCADA components and telemetry systems will be required, complete with a local uninterruptible power supply, possibly utilizing solar cells.

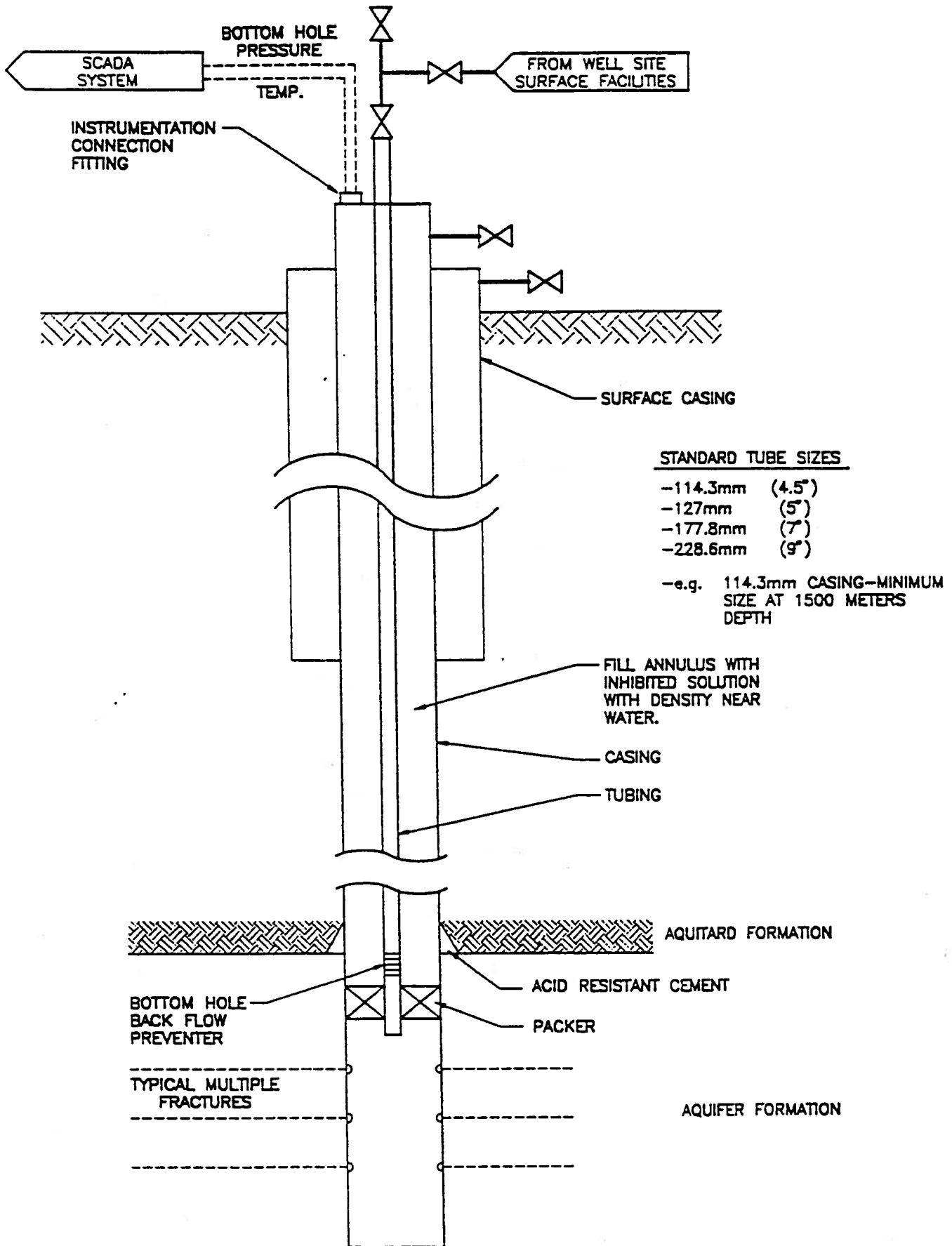
#### **2.4.2.2 INJECTION WELLS**

This system envisages wells similar to that shown in Figure 2.4.2-2. The downhole back pressure flow preventer is essential, protecting against well casing failure. The filling of the annulus with a dense fluid eliminates many stresses on the casing reducing potential corrosion.



SURFACE PIPING  
AND CONTROLS  
FIGURE 2.4.2-1





**STANDARD TUBE SIZES**

- 114.3mm (4.5")
- 127mm (5")
- 177.8mm (7")
- 228.6mm (9")

-e.g. 114.3mm CASING--MINIMUM SIZE AT 1500 METERS DEPTH

**TYPICAL WELL**  
FIGURE 2.4.2-2

### **2.4.2.3 MONITORING WELLS**

There will be two types of monitoring wells - those that will become future injectors and those that will continue as monitors. These wells will have bottom hole and above aquitard pressure sensors as well as a formation water sampling capability. The future injector category will be completed as per the regular injection wells, except that fracturing will be deferred. The monitoring only wells will tentatively have 60.3 mm tubing and 114 mm casing. All wells will be designed to good oil and gas field practice, recognizing the low pH regime in the aquifer, particularly near the well.

## **2.5 SYSTEM COSTS**

### **2.5.1 ESTIMATES**

#### **2.5.1.1 INTRODUCTION**

This section provides guidelines for the preparation of cost estimates for the installation and operation of facilities for the transportation, distribution and injection of CO<sub>2</sub> from a source location to injection wells. This section covers measurement, control, pumping, medium and high pressure pipelines, wellsite facilities and high pressure pipelines, and their operations. Costs are in 1993 Canadian dollars and are based on typical Canadian conditions. No attempt was made to select a specific location or route, nor to identify particular costs which may be associated with a specific location and not to another location. CO<sub>2</sub> capture and purification costs, and well drilling, completion and workover costs are not included.

The costs have been derived from Stanley's extensive data base of costs for similar projects completed, underway, or under study. However, the data have been adjusted to apply specifically to CO<sub>2</sub> injection project use, and are not suitable for other purposes.

The cost data have been assembled to provide a relationship between cost and other parameters, such as pumping power, pipeline size, or throughput capacity. Before attempting to estimate costs, these basic parameters must be determined. Therefore, in the next step, a layout of the proposed system must be prepared, and each of the components identified. The size or capacity of each component is determined from the appropriate sizing charts or other engineering methods. The unit cost for each component is then determined, using the appropriate curve, and this cost multiplied by the quantity included in the project.

The cost curves, in keeping with the nature of this report, are generic only. For any given situation, the costs may be higher or lower due to factors not considered herein. Further, the owner of the facility has many options in selecting plant design, to sacrifice higher operating costs to achieve lower investment costs, and certain design innovations may result in higher or lower costs. Finally, costs may vary to accommodate planned future increases or decreases in throughput volumes.

#### **2.5.1.2 FIELD FACILITY INVESTMENT COSTS**

The investment costs are intended to be total installed costs for the facility, including land acquisition, engineering, inspection, and owner's administration and overhead costs. They do not include costs for feasibility studies or other "pre-project" expenses. However, commissioning and start-up costs are included. Operator training is included in Operations Costs and is therefore not included here.

#### **METERING AND SCADA**

The investment costs for an inlet metering and control station, including system Supervisory Control and Data Acquisition (SCADA), are shown on Figure 2.5.1.2-1. This is assumed to be a shop-fabricated, skid-mounted assembly on a concrete slab base. A separate pre-

fabricated building, also mounted on a concrete slab, houses control and telemetry equipment, and provides a small office. The telemetry communications system is assumed to be via VHF radio, and the base station, with its antenna tower, is included in these costs. It has been assumed that the CO<sub>2</sub> product is dry and pure when received, and no costs for purification are included. The station is assumed to be located on the source plant site property, and no land costs or utility connection costs are included. No provision is made for warehousing of spare parts, nor for a system operations centre with shop and office facilities.

### **HIGH PRESSURE TRANSPORTATION PIPELINE**

The appropriate pipeline size must first be determined based on length and capacity required, from Figure 2.5.1.2-2. The investment costs for a high pressure pipeline to transport CO<sub>2</sub> from the source location to the disposal area are shown on Figure 2.5.1.2-3. These curves cover the typical costs for pipelining in undeveloped low cost (flat pasture land) and in medium cost (acres or forested) areas. The following assumptions were made in developing these curves:

- Pipeline maximum operating pressure 10,000 kPa (use of ANSI 600 rated flanges).
- Corrosion allowance 1.6 mm (1/16 inch).
- Rural location with undulating hills but no steep gullies or other barriers.
- Clay, silt or till overburden with minimal gravel and no rock.
- Depth of cover 1 m on all lines.
- River, highway, railroad crossings are extra to the base cost.
- No restricted right-of-way width or route access.
- Local availability of labour, equipment and materials for construction.

**Figure 2.5.1.2-1**  
**Meter Station and SCADA Costs**

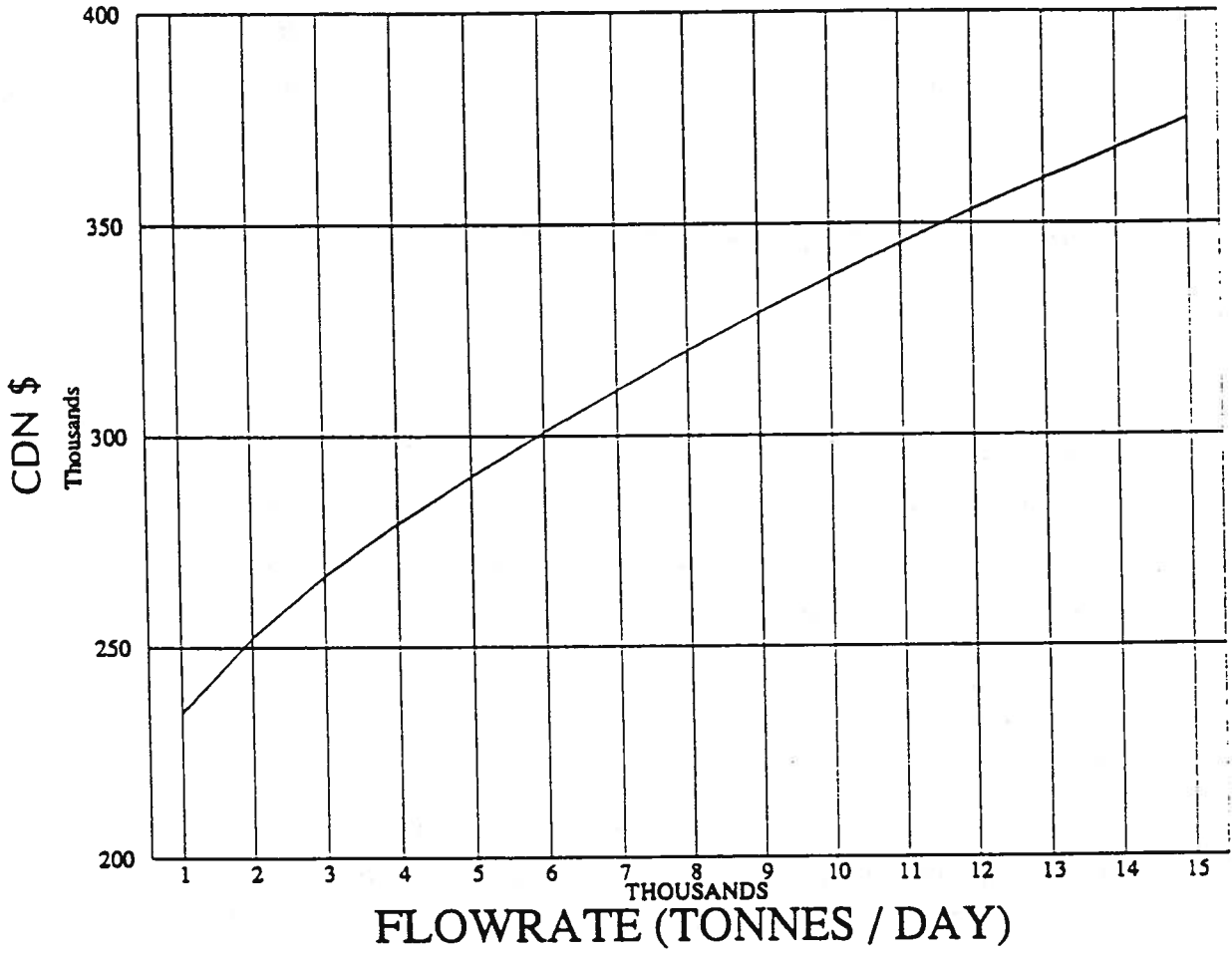


Figure 2.5.1.2-2  
Line Sizing

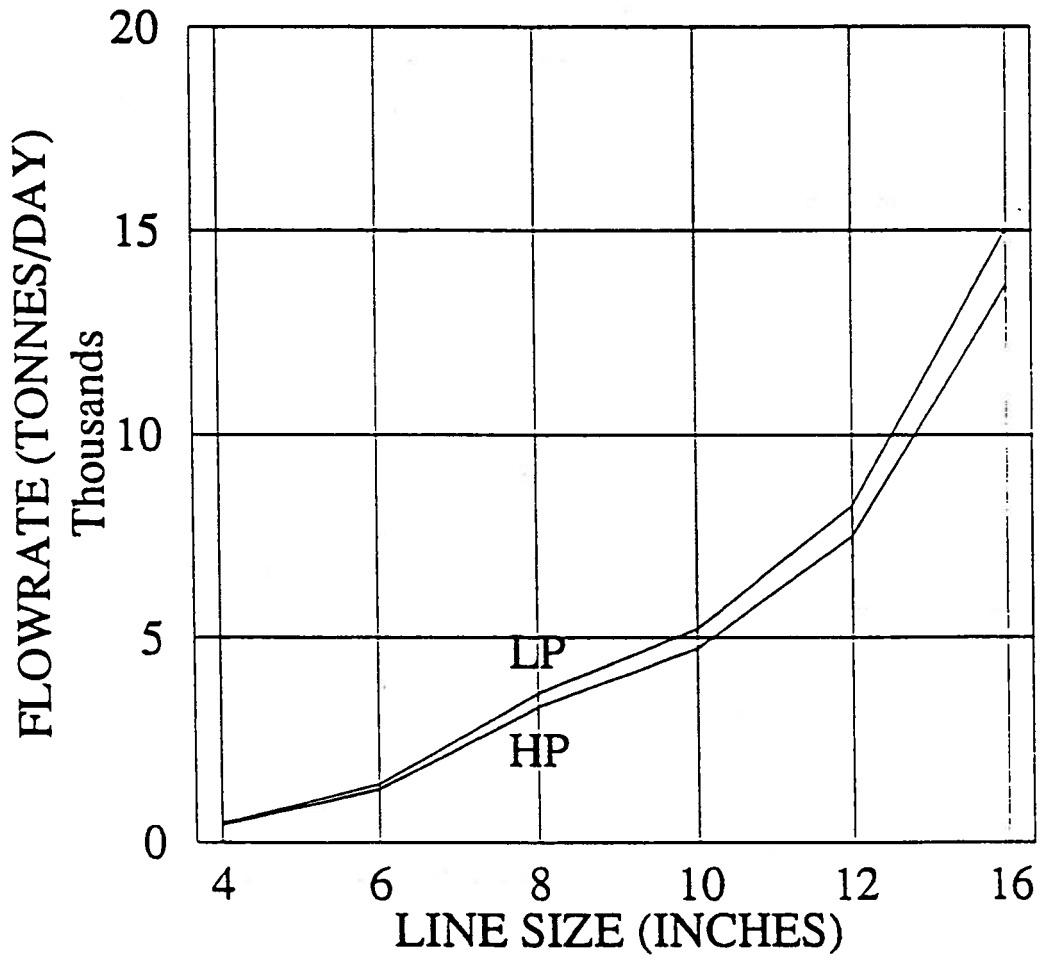
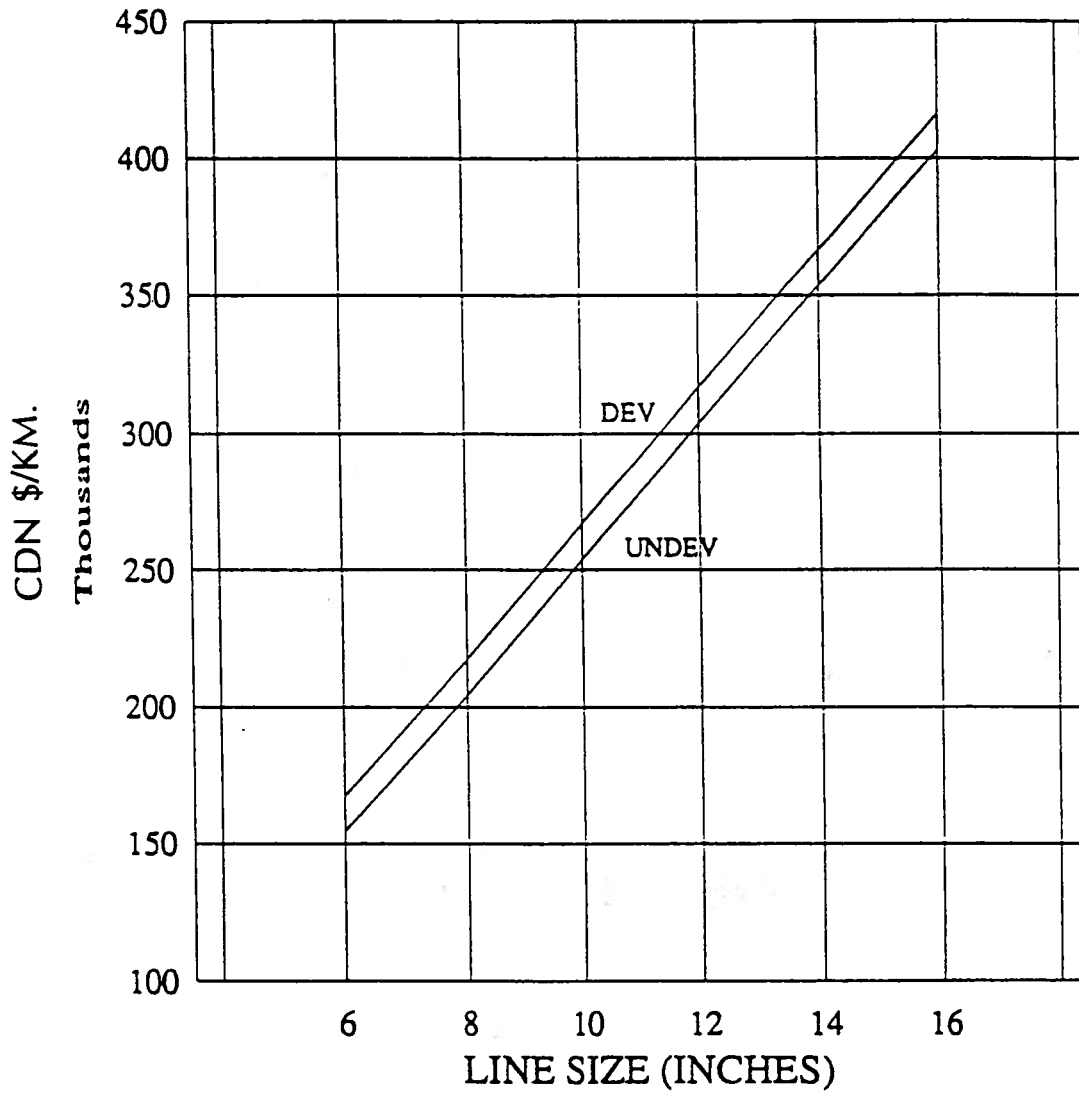


Figure 2.5.1.2-3  
CO<sub>2</sub> Pipeline Costs  
High Pressure Pipeline  
\$ Range Developed Versus Undeveloped Land



- Restoration typical of pasture or farm land.
- Survey, inspection, 100% radiography, cathodic protection, engineering and overhead costs are included. An allowance for an environmental impact assessment and extraordinary permitting costs must be added.
- The base costs include a simple riser at each end, but do not include intermediate block valve assemblies or other appurtenances.

### **MISCELLANEOUS PIPELINE COSTS**

Costs have been obtained from Stanley's data base for specific items, to be added for total pipeline costs. These items have not been included in the premises of this report, as they are somewhat unusual in the pipelines under consideration.; but are presented here for information purposes only:

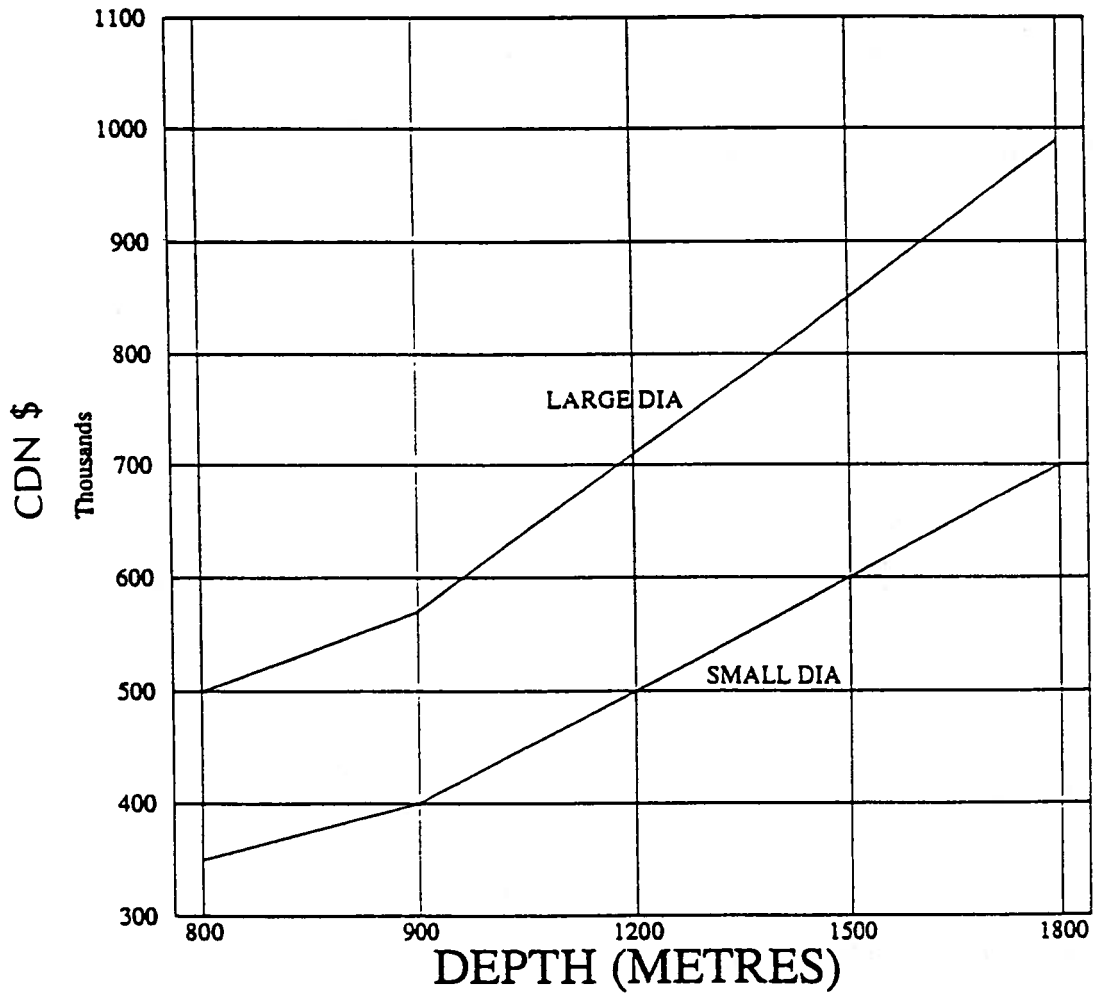
- |   |                                      |
|---|--------------------------------------|
| • Rock Excavation<br>(Blasting or Air Tool Removal) | Add \$180.00/m                       |
| • River Crossing Directionally Drilled              | Add \$1,100.00/m                     |
| • Railroad or Highway Crossing<br>(Bored)           | Add \$200.00/m                       |
| • Automatic (SCADA) Block Valve Assembly            | Add \$10,000.00<br>for each assembly |

### **WELLSITE FACILITY COSTS**

The investment costs for wellsite facilities and individual wells, as a function of well injection capacity, are shown on Figure 2.5.1.2-4. These cover filter assembly, control equipment, SCADA and telemetry equipment, and associated piping and valves.



Figure 2.5.1.2-4  
Well and Wellhead Costs



The figure includes costs for drilling and completing injection wells. These costs may also apply to observation wells if required (with the smallest size to be used). It is assumed that drilling rigs would be available within a reasonable proximity to the well site to minimize mobilization costs. Also, it is assumed that well site access is good, and that environmental and drilling/completion regulations similar to that in Alberta environmental and drilling would apply.

## **DECOMMISSIONING**

All wells but those selected for ongoing monitoring must be properly abandoned at the end of the injection period.

Such costs will be significant at that time, but not on a net present value basis. The scrap value of pipelines is unlikely to be enough to cover the cost of reclaiming land, even in remote areas, and such lines will probably be left in place with concrete or other fill to maintain structural integrity.

While on a present value basis, decommissioning costs are minuscule, future decommissioning must be considered in all designs and operating procedures.

### **2.5.1.3 FIELD OPERATING COSTS**

Supervising labour, maintenance and various insurances will cost approximately 10 percent of the facility capital cost. But such costs are very site specific.

## **2.5.2 SYSTEM DEVELOPMENT**

From the above discussion, it is obvious that much preliminary and detailed effort is needed even before an aquifer disposal system becomes a project. The following is a brief review of key factors in pre-project costs:

### **2.5.2.1 GEOLOGICAL AND GEOPHYSICAL DEVELOPMENT**

These are also discussed later in Section 12. There will be a wide range of costs but a range from \$1,500,000 appears likely for exploratory/confirmation drilling (which will also provide the requisite water and matrix samples), and the related engineering, geological, geophysical and geochemical services.

### **2.5.2.2 EXTERNAL RELATIONS**

A very approximate estimate of \$500,000 is projected for this area, covering environmental studies and impact assessments, regulatory agency negotiations and citizen acceptance programs.

### **2.5.2.3 LAND ACQUISITION**

Land costs will vary more than any other variable between different settings. For this report, land and related acquisition fees have been valued at \$3,000 per hectare. Up to 5 hectares are required per kilometre of pipeline and 3 hectares for each well.

#### 2.5.2.4 PROJECT COORDINATION

The development of a pressurizing, distribution and well system will take project management time and expenses not included elsewhere in the cost estimates. Such costs are expected to be in the order of \$1,000,000 for a Wabamun area project.

#### 2.5.3 COST SUMMARY

**Table 2.5.3-1**  
**Wabamun Area Disposal System Capital Costs**  
**for CO<sub>2</sub> from a 500 MW Power Plant**  
**in Millions of 1993 Canadian Dollars**

<b>Facility</b>	
• Meter Station	0.2
• Pipeline 30 km @ \$300,000	9.0
• Wells 15 @ \$800,000 (Injection)	12.0
• Wells 16 @ \$550,00 (Monitoring)	8.8
<hr/>	
Sub Total	30.0
<hr/>	
<b>Overheads</b>	
• Geotechnical	1.0
• Permitting et al	0.5
• Land Acquisition	0.7
• Project Coordination	1.0
<hr/>	
Sub Total	3.2
<hr/>	
<b>Overall Total</b>	<b>33.2</b>
<hr/>	

The accuracy of the overall costs are expected to be in the order  $\pm 35$  percent.

Operating costs for the disposal pipeline/well system will be in the order of \$2,000,000 a year. Note that the above does not include cost originating inside the power station/capture/compression facility envelope.

## 2.6 ENVIRONMENTAL FACTORS

This study did not investigate environmental factors in any detail, but the following comments came out of this study and the IEA study:

- a) In this area the study team believes that injected CO<sub>2</sub> can be contained in the formation.
- b) Monitoring wells will be needed to ensure no undue fingering of CO<sub>2</sub>-rich materials occurs until pressures have declined to near background levels (in the long future).
- c) The use of high vapour pressure liquid pipeline codes and practises should be used.
- d) SO<sub>2</sub> must be kept to very low levels, as CO<sub>2</sub> leaks will remain close to the surface. In the case of large leaks, dry ice crystals will increase the density of the leaking CO<sub>2</sub> cloud even more than normal.
- e) Valley routing should be avoided and any river crossings have automated valves on either side to minimize CO<sub>2</sub> release.
- f) Only minor biota damage is foreseen from leaks.

## **3.0 REGIONAL GEOLOGY**

### **3.1 GENERAL**

The Alberta Basin comprises a wedge of sedimentary rocks that thickens westward from a zero edge at the Canadian Shield to more than 6 km at the foreland thrustfold belt. The basin can be divided into two distinct tectono-sedimentary realms: the passive margin and the foreland basin. The Cambrian to Jurassic passive-margin phase of basin development consisted of dominantly carbonate sedimentation, with periods of clastic and evaporite deposition. Starting in Jurassic time, the western margin of the basin changed to a site of active compressional tectonism. The Jurassic to Tertiary foreland basin is dominantly comprised of clastic rocks (sandstone and shales) which were shed from the developing orogenic belt to the west. Adjacent to the Canadian Shield, the regional dip of Palaeozoic strata is approximately 4 m/km, while that of the overlying Mesozoic strata is only 1.4 m/km. Approaching the foreland thrustfold belt, the regional dip of the Phanerozoic strata increases to 10 m/km. A more detailed overview of the regional geology in the Alberta Basin is given by Porter et al. (1982).

The above simplified and general description of basin geology is important for understanding the hydrostratigraphy, mineralogy and properties of any aquifer selected for the subsurface disposal of CO<sub>2</sub> in Alberta. Carbonate aquifers are found at greater depths than sandstone aquifers. Any given regional aquifer is found at shallower depths in the east than in the west. Because of pre-Cretaceous to recent erosion, some aquifers present in the west are truncated or absent in the east. The salinity of formation waters in the Palaeozoic aquifers is generally high, while in the Cretaceous aquifers is generally low (Hitchon et al., 1989, 1990; Bachu and Underschultz, 1993). Aquifer properties like porosity and permeability tend to vary with location and depth (Bachu and Underschultz, 1992). Geothermal gradients, hence formation temperature, vary on a regional scale from southwest to northeast (Bachu and Burwash, 1991). Thus, there is no single "characteristic

**Table 3.1**  
**Stratigraphy, Lithology and Hydrostratigraphy of**  
**Selected Sedimentary Strata in the Area Defined as**  
**Tp. 49-52, R3-5, W5Mer, in Alberta**

	STRATIGRAPHY	LITHOLOGY	HYDROSTRATIGRAPHY
CRETACEOUS	Edmonton Gp.	Sandstone/Shale	aquifer
	Belly River Fm.	Sandstone	aquifer
	Lea Park Fm.	Shale	aquitard
	Colorado Gp.	Shale	aquitard
	Upper Mannville	Sandstone	aquifer
	Clearwater	Shale	aquitard
	Lower Mannville	Sandstone	aquifer
CARB.	Rundle Gp.	Dolomitic limestone	aquifer
	Banff Fm.	Limestone/Shale	aquifer/aquitard
	Exshaw Fm.	Shale	aquitard
DEVONIAN	Wabamun Gp.	Limestone	aquifer
	Winterburn Gp.	Dolomite	aquifer
	Ireton Fm.	Shale	aquitard

aquifer" in the Alberta Basin, or no aquifer can be characterized by single values of salinity, pressure, porosity, permeability, and the like.

### 3.2 **AQUIFER PETROPHYSICS**

For the purpose of this study (proof of concept for the subsurface disposal of CO<sub>2</sub>) there is need for some realistic aquifer characteristics in order to perform geochemical and fluid flow numerical modelling of CO<sub>2</sub> injection. Keeping in mind that, for economical and environmental reasons, the captured CO<sub>2</sub> should be disposed of close to the generating power plant, a region west of Edmonton was chosen for aquifer identification and characterization. The area, defined by Tp. 49-52, R 3-5, W5 Mer, is in the immediate vicinity of the Sundance and Genesee power plants. Based on the general stratigraphy of the sedimentary strata in the area, regional siliciclastic and carbonate aquifers were identified in the area at depths between 1400 and 2000 m. These aquifers are deep enough to be part of regional flow systems isolated from the surface by extensive regional aquitards, yet relatively shallow (as much as possible) in order to minimize drilling costs. Table 3.1 presents the stratigraphy, main lithology and hydrostratigraphy of the stratigraphic succession of interest. The aquifers selected for proofing the CO<sub>2</sub> disposal concept are the carbonate Wabamun (Devonian) and the sandstone Lower Mannville (Cretaceous). Major regional confining aquitards in the area are the Colorado, Clearwater, Lower Banff and Ireton shales.

The determination of characteristic values for the geochemical, hydrodynamic and geothermal parameters of interest for the two selected aquifers is based on the extensive data bases, data base management system and data processing software implemented at the Alberta Geological Survey. An electronic data base for all the wells in Alberta is maintained and updated regularly based on the Energy Resources Conservation Board (ERCB) releases. A search through this data base identified 754 wells in the area of



interest. Based on stratigraphic information from these wells, a representative depth and thickness was determined for the Wabamun and Lower Mannville aquifers (Table 3.2).

An electronic data base of cored intervals and core analyses in Alberta wells is maintained at the Alberta Geological Survey based on ERCB public information. The data base was searched first to identify cored intervals in the two aquifers. This information (Appendix 11.3.1) was subsequently used to collect core samples for mineralogical analysis, to be used in geochemical modelling of CO<sub>2</sub> disposal.

A typical core-plug analysis contains information about, among other things, the maximum permeability in the horizontal plane,  $k_m$ , the permeability  $k_{90}$  in the horizontal plane normal to the direction of maximum permeability, the permeability in the vertical direction,  $k_v$ , and porosity  $\phi$ . The core-plug analyses for Wabamun and Lower Mannville rocks in the area of interest were extracted from the data base and culled for erroneous values. The porosity and permeability data obtained from core analyses represent volume-averaged values corresponding to the measurement (plug) scale. In order to characterize the two aquifers, a sequential scaling-up process must be used (Cushman, 1984). The plug-scale porosity and permeability data were scaled-up first to the well scale and then the well-scale values were scaled-up to the formation (aquifer) scale (Bachu and Underschlutz, 1992). Characteristic porosity and permeability values for the two aquifers are presented in Table 3.2. These values are of the same order of magnitude as the characteristic values for the same or similar units elsewhere in the basin (Bachu and Underschlutz, 1992, 1993). Because these representative porosity and permeability values were generated from plug-scale measurements, they are characteristic of the movement of fluids through the pore space only. They do not characterize the movement of fluids through large-scale features such as vugs, caverns or fractures, which are beyond the resolution of plug-scale measurements. Thus, the large-scale permeability and porosity in the carbonate Wabamun aquifer may be larger. Nevertheless, studies based on drillstem

**Table 3.2**  
**Characteristic Properties of Selected Deep Aquifers**  
**in the Area Defined as Tp. 49-52, R3-5, W5Mer, in Alberta**

Aquifer	Wabamun	Lower Mannville
Depth (m)	1,800	1,450
Thickness (m)	170	55
Salinity (mg/l)	160,000	75,000
Pressure (kPa)	15,000	11,300
Max. Permeability $k_m$ (mD)	2.2 n.a.	1.3 4.0
Standard Dev. of $k_m$ (mD)	n.a. 0.82	0.65 0.30
Horizontal anisotropy	8	12
Vertical anisotropy	n.a.	3.5
Porosity $\phi$ (%)		
Standard dev. of $\phi$		

tests elsewhere in the basin (Hitchon et al., 1989; Bachu and Underschultz, 1992) suggest that the order of magnitude is correct.

Other parameters of interest for aquifer characterization and hydrodynamic simulation of CO<sub>2</sub> disposal are formation pressure, temperature and thermal conductivity. The formation pressure for the two aquifers of interest in the area was obtained from the electronic data base of drillstem tests implemented at the Alberta Geological Survey. Representative values are given in Table 3.2. Characteristic temperature values can be calculated based on aquifer depth, an annual average ground temperature of 6°C and a geothermal gradient of 23°C/km in the area (Bachu and Burwash, 1993). Finally, the thermal conductivity of aquifer rocks can be calculated based on rock thermal conductivity values (4.17 W/m°C for sandstone, 3.46 W/m°C for limestone and 3.3 W/m°C for dolomite) corrected for temperature and porosity effects (Bachu, 1993).

### **3.3 AQUIFER FORMATION WATER CHEMISTRY**

An electronic data base of approximately 150,000 analyses of formation waters in British Columbia, Alberta and Saskatchewan is maintained at the Alberta Geological Survey. Previous studies in the Basin (Hitchon, 1989, 1991; Hitchon et al., 1987, 1989, 1990) have shown that as few as one-fifth of standard formation water analyses in any particular area may be suitable for consideration after culling by appropriate automatic and manual procedures. Typically, analyses can be contaminated, mixed with other samples, or be incomplete. The automatic cull takes into account the presence and values of OH, CO<sub>3</sub>, Ca, Mg, Cl, SO<sub>4</sub>, HCO<sub>3</sub>, acceptable ranges of pH and density, and mixing of formation waters from several intervals. The formation water analyses for the Wabamun and Lower Mannville aquifers in the area of interest were culled mechanically and screened manually resulting in 135 representative analyses (Appendix 11.3.2). Representative TDS (Total Dissolved Solids) values are shown in Table 3.2.

The TDS contents of the formation waters in the potential disposal horizons are usually high and increase significantly with depth. They range from 70,000 mg/L in the Cretaceous formations to well over 170,000 mg/L in the Devonian formations. Several formations in this region have anomalous formation water compositions when compared to the rest; for example, the Glauconitic formation with a TDS in the range of 4200 mg/L.

The formation water compositions vary significantly with depth and laterally, but the dominant cation is almost always sodium. The maximum sodium concentration is in excess of 50,000 mg/L, the maximum potassium concentration exceeds 30,000 mg/L and the maximum calcium concentration exceeds 10,000 mg/L. Typical calcium concentration ranges are in the hundred mg/L range. Except in the dilute fluids, the dominant anion is chloride which can reach levels in excess of 100,000 mg/L in the brines. Sulphate can reach levels of 5,000 mg/L which appears to correlate to high potassium levels. Total alkalinity levels are typically in the 600 mg/L range, with highs over 1,100 mg/L and lows less than 100 mg/L. For most of the waters, the milli-equivalent range for alkalinity is less than that of calcium. The pHs for these waters are typically in the high 7 to low 8 range; however, extreme values down to 6.1 and up to 9.1 are reported. The analyses were used subsequently in the geochemical modelling of CO<sub>2</sub> disposal.

#### **3.4 AQUIFER FORMATION MINERALOGY**

Ten core samples were selected from the cored intervals of siliciclastic and limestone aquifers listed in Appendix 11.3.1 and were collected from the ERCB core facility in Calgary as potential material for the validation experiments. Only seven core samples were available and their formations are listed in Table 3.3. Thin sections and bulk XRD were made from each of the samples. XRD tracings for the seven samples are included in Appendix 11.3.3. The mineralogy is listed in Table 3.4. The modal mineral concentrations for all 7 samples are estimated from XRD peak intensity.

Table 3.3  
Aquifer Formation  
Samples from ERCB

CO2 INJECTION STUDY--SAMPLES

SAMPLE #1	4-14-51-4W5 DEPTH 6410.5 FT(1953.8M) POROUS CARBONATE
SAMPLE#2	02/16-18-49-4W5 DEPTH 1775.95M POROUS CARBONATE (SANDY IN PT.)  NO CORE @ 1725M IN 02/16-18-49-4W5
SAMPLE#3	02/16-18-49-4W5 DEPTH 1777.28M CALCAREOUS SAND(UNDERLIES CARB.-SAMPLE#2)
SAMPLE#4	6-18-50-3W5 DEPTH 1555.65M BIOTURBATED SANDSTONE
SAMPLE#5	1-6-50-3W5 DEPTH 1610.05M CALCAREOUS SANDSTONE 1607-1609.75M = SHALE WELL LOG OR CORE POSSIBLE OFF DEPTH
SAMPLE#6	10-2-50-3W5 DEPTH 1566.25 CALCAREOUS SAND  NO CORE @1548M 10-2-50-3W5 CORE STARTS @ 1564M
SAMPLE#7	16-9-51-4W5 DEPTH 1580.0M CALCAREOUS SAND
8-31-49-5W5	NO SAMPLE TAKEN -ZONE =TIGHT CARBONATE(NO POROSITY)- 3M BELOW=30CM CHERT CONGLOMERATE ALSO TIGHT  NO CORE @ 1940M-WABAMUN(8-31-49-5W5)

Sample #1 is a siliciclastic dolostone; dolomite dominates in the sample with about 5% of quartz and 1% K-feldspar. Samples #2, #5, and #7 are siliciclastic limestone. Calcite is the dominant mineral in these three samples, with some quartz and fluorapatite. Sample #3 has complex lithology, varying from highly phosphatic, siliciclastic limestone to highly calcareous, siliciclastic phosphate rock. Major minerals in Sample #3 are quartz, calcite, and fluorapatite. Sample #4 is a calcite cemented, well sorted quartz sandstone. Clay minerals in the sample cannot be detected by XRD method but can be seen under optical microscope. Sample #6 is a calcareous sublitharenite, containing mainly quartz and calcite with minor amounts of siderite and dolomite.

Sample #4 was chosen for the validation experiments because it represented most closely the formation mineralogy expected in a good siliciclastic aquifer.

**Table 3.4  
Mineral Composition**

Sample	Calcite	Dolomite	Quartz	Fluorapatite	Others
#1	--	94	5	--	K-feldspar: 1
#2	90	--	5	5	--
#3	35(33)	--	45(25)	20(39)	--
#4	5(16)	--	95(70)	--	Clays: (3)
#5	92	--	5	3	--
#6	30(40)	2(2)	65(47)	--	Siderite: 5(5)
#7	95	--	2	3	--

Note: Mineral concentrations are shown in terms of relative peak intensities. Numbers in brackets are the modal fraction estimated from optical microscopy.

## 4.0 NUMERICAL SIMULATION OF AQUIFER INJECTABILITY

### 4.1 DESCRIPTION OF NUMERICAL SIMULATOR

The numerical model used in this study was the STARS 4.0.2 developed by the Computer Modelling Group (CMG) in Calgary, Alberta. STARS 4.0.2 is a four-phase, multi-component thermal STeam and Additive Reservoir Simulator. Some of the novel features of STARS, including fully implicit wells and thermal aquifer model, were used in this study (STARS, 1990).

The numerical simulation was a 2-D cylindrical pattern simulation based on a Lower Mannville siliciclastic aquifer in the Wabamun Lake area in Alberta. The numerical simulation was isothermal at the average temperature of the aquifer.

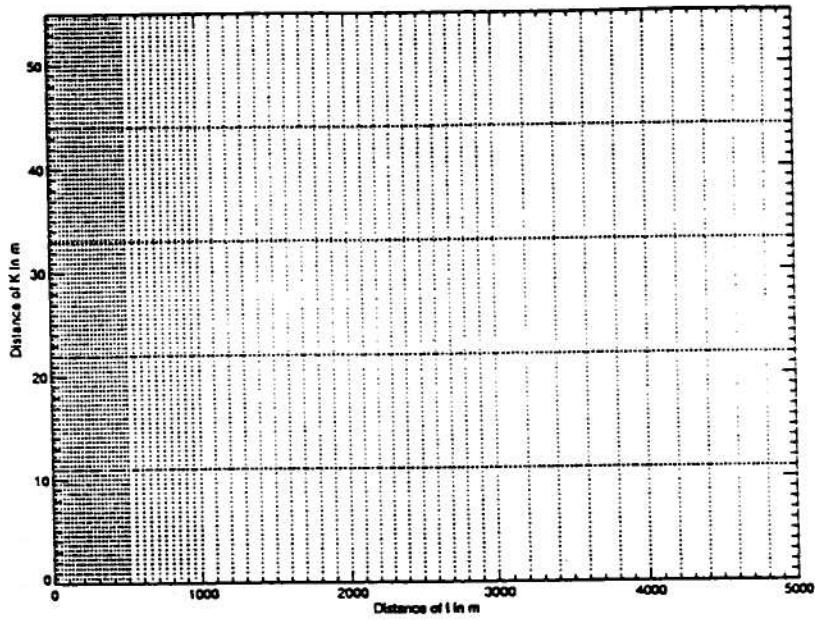
A 2-D cylindrical grid pattern with 330 ( $I = 66, J = 1, K = 5$ ) grid blocks was used to subdivide a region of the aquifer into discrete segments, with a radius of 5 km (Figure 4.1a) around a vertical injector. At the outflow boundary, a semi-analytical thermal aquifer model (Appendix 11.4.1) was used to calculate the water flow from this region to an infinite aquifer. There was a finer grid resolution near the injector which was located at the axis of symmetry ( $I = 1$ ). The grid block sizes in the radial direction ( $I$ -direction) were varied from 1 m near the injector to 200 m near the outflow boundary. On the other hand, the grid block sizes in the angular ( $J$ -direction) and the axial direction ( $K$ -direction) were uniform with dimensions of  $360^\circ$  and 11 m, respectively.

In some numerical runs, a 2-D cylindrical grid pattern with 140 ( $I = 28, J = 1, K = 5$ ) gridblocks was used to blow up a region of aquifer with a radius of 0.65 km (Figure 4.1b) around the injector. All numerical runs were performed on a Sun Workstation, SPARC station 2. Typical runs with 330 and 140 gridblocks took approximately 6 and 2.5 CPU hours, respectively.

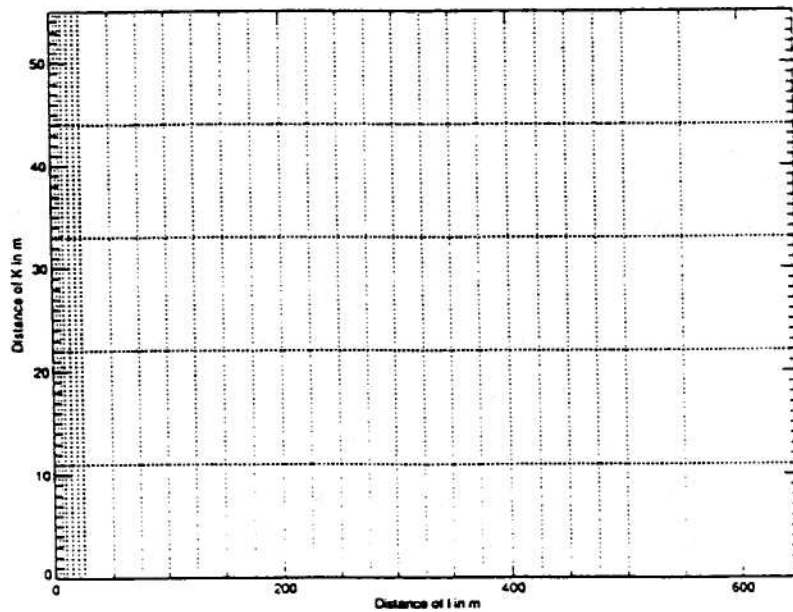


**Figure 4.1**  
**Grid Pattern**

Gridblock sizes not in scale



(a)  $66 \times 1 \times 5$  (Location of Aquifer Outflow Boundary = 5 km)



(b)  $28 \times 1 \times 5$  (Location of Aquifer Outflow Boundary = 0.65 km)

## 4.2 PHYSICAL PROPERTIES OF THE AQUIFER

The objective of this numerical study is to investigate the potential for subsurface disposal of CO<sub>2</sub> in Alberta. The aquifer selected is a Lower Mannville siliciclastic aquifer in the Wabamun Lake area, Alberta.

The aquifer which is 1450 m underground and 55 m thick was assumed to be homogeneous in this study. The absolute permeabilities in the horizontal and the vertical directions were 1.3 and 0.39 mD, respectively, and the porosity is 12%. The pressure at the top of the aquifer is 11.3 MPa. The average temperature of the aquifer is 40°C, which was estimated based on a ground surface average temperature of 6°C and a geothermal gradient in the area of 23°C/km.

A density of 2643 kg/m<sup>3</sup> and a compressibility of 4.7 × 10<sup>-7</sup>/kPa were used for the sandstone in the numerical simulation. The fracture pressure at the top of the formation was 32.8 MPa. It was estimated based on a gradient of 22.61 kPa/m (i.e. 1 psi/ft) that related the minimum principal stress to the weight of the overburden (Tremblay, 1993).

The thermal conductivity of the sandstone could be estimated using the following correlation:

$$k_{th}(T) = k_{th}(20) \times 293 / (T + 273) \quad (1)$$

where  $k_{th}(20)$  is the thermal conductivity at 20°C and T is temperature in °C. For sandstone,  $k_{th}(20) = 4.17$  W/m-°C and  $k_{th}(40)$  could be estimated as 3.9 W/m-°C.

The carbon dioxide in the aquifer was in supercritical conditions and was treated as a single phase fluid in the numerical simulation. The densities of CO<sub>2</sub> at 40°C varied from 638 kg/m<sup>3</sup> at 10 MPa to 907.7 kg/m<sup>3</sup> at 30 MPa (Clark, 1966). The viscosity of CO<sub>2</sub> at

40°C and 20 MPa was 0.077 cp (McHugh and Krukoni, 1986). The effect of pressure over a range of 10 to 30 MPa on the viscosity of CO<sub>2</sub> was neglected in this study.

The CO<sub>2</sub> was allowed to dissolve in water in the numerical simulation due to the high solubility of CO<sub>2</sub> in water. However, the solubility of water in CO<sub>2</sub> was relatively small and was neglected in the numerical simulation. The K values for CO<sub>2</sub> in water at 40°C could be estimated from SOLMINEQ.88 using the following correlation (Kharaka et al., 1988):

$$\log K = -2.419 + 0.9838 \log P \quad (2)$$

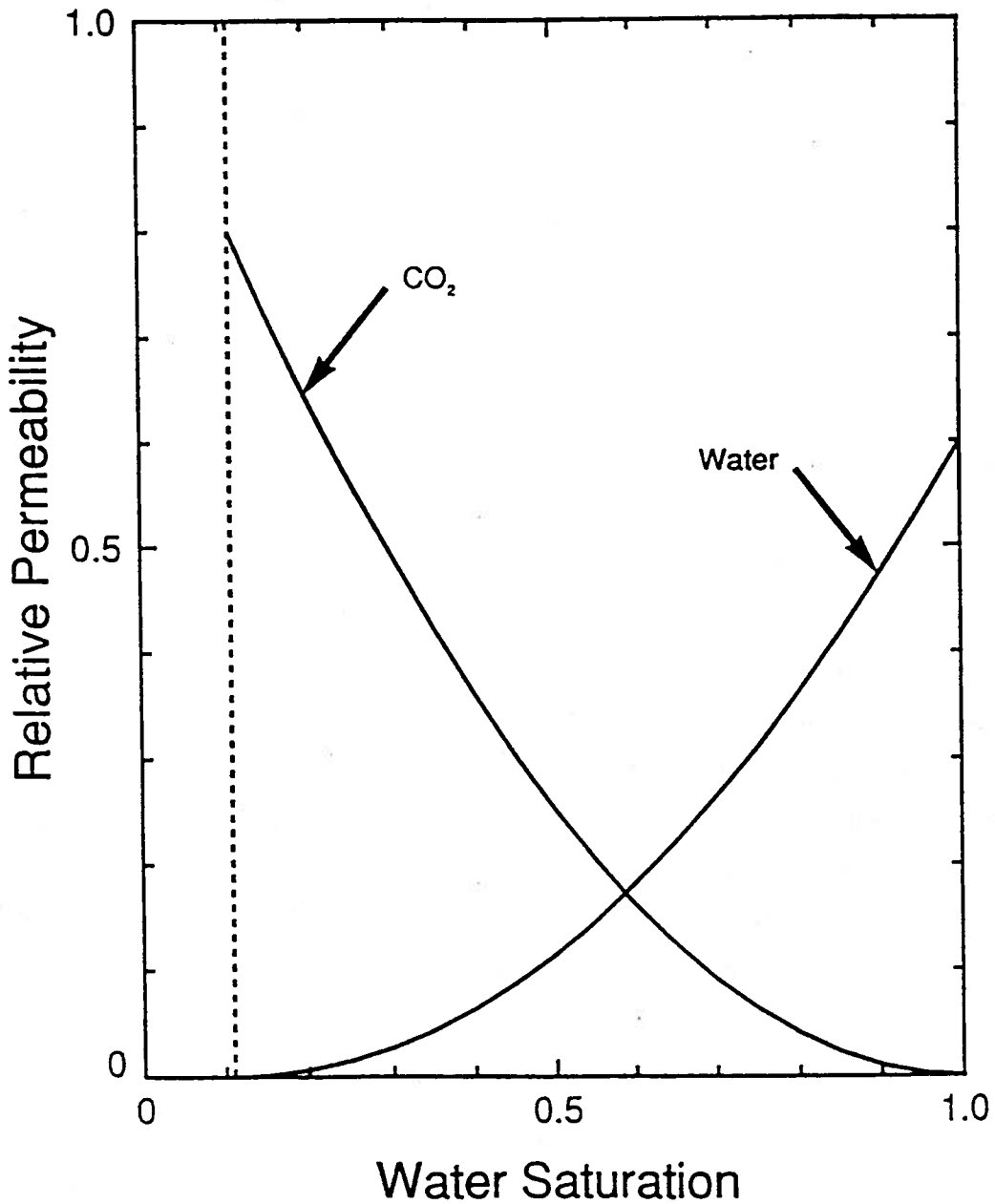
where K is the mole fraction of CO<sub>2</sub> dissolved in water and P is the pressure in MPa. From Equation (2), the K values for CO<sub>2</sub> in water varied from 0.0367 at 10 MPa to 0.1082 at 30 MPa. It is noted that the density of the CO<sub>2</sub> in water phase was set to the same density of the water.

The relative permeability curves for the water-CO<sub>2</sub> system are given in Figure 4.2. The supercritical CO<sub>2</sub> was treated as a single fluid which had behaviour between a gas and a liquid. Hence, a zero residual saturation was chosen for the CO<sub>2</sub> relative permeability curve. It is noted that the relative permeability curves were not measured but typical curves for the water-oil system in Alberta oil reservoirs.

The capillary pressure effect was neglected in the numerical simulation. Firstly, the capillary pressures of the water-CO<sub>2</sub> system in the aquifer were unknowns. Secondly, capillary pressure effect may not be significant as the pressure changes (in the order of 1-10 MPa) during the CO<sub>2</sub> injection were one or two order of magnitude higher than the estimated capillary pressures.

Figure 4.2  
Relative Permeability Curves for Water-CO<sub>2</sub> System

End Point for CO<sub>2</sub> Relative Permeability Curve = 0.8  
End Point for Water Relative Permeability Curve = 0.6  
Residual CO<sub>2</sub> Saturation = 0  
Irreducible Water Saturation = 0.11



### 4.3 INJECTION STRATEGIES

In the numerical simulation, 100% CO<sub>2</sub> at 40°C was injected at a constant injection pressure of 29.5 MPa (i.e. 90% of the fracture pressure of 32.8 MPa at the top of the aquifer). The vertical injector penetrated the entire thickness of the aquifer. In all numerical runs, the injector was either completed at an interval of 11 m at the bottom of the aquifer (I = 1, K = 5) or at an interval of 55 m covering the entire thickness of the aquifer (I = 1, K = 1→5). The injector radius was either 3 inch or 4 inch.

A list of the numerical runs is given in Table 4.1. Numerical runs CO<sub>2</sub>\_6-9 which all simulated a 30-year CO<sub>2</sub> injection period, were conducted to investigate the effects of location of aquifer outflow boundary, injector size and injector completion. Numerical run H<sub>2</sub>O\_4 which simulated a 30-year water injection period, was conducted to investigate the effect of injected fluid. Numerical run CO<sub>2</sub>\_12, which simulated a 30-year CO<sub>2</sub> injection period plus a 10-year period after the shut-in of the injector in a hypothetical aquifer with absolute permeabilities 10 times those of the Wabamun Lake aquifer, was conducted to investigate the effect of permeability.

### 4.4 INJECTIVITY OPTIMIZATION

Numerical predictions of cumulative CO<sub>2</sub> injection, CO<sub>2</sub> injection rate and CO<sub>2</sub> saturation contours as a function of time are given in Figures 4.3-4.10 for numerical runs CO<sub>2</sub>\_6-9. In general, CO<sub>2</sub> propagated less than 600 m away from the injector after an injection period of 30 years. Approximately 26 to 29 wt % of the injected CO<sub>2</sub> dissolved into water. There was evidence of CO<sub>2</sub> override to the top of the aquifer when the injector was completed near the bottom of the aquifer (runs CO<sub>2</sub>\_6 and CO<sub>2</sub>\_7). The override of CO<sub>2</sub> was more significant when the completion of the injector covered the entire thickness of the aquifer (runs CO<sub>2</sub>\_8 and CO<sub>2</sub>\_9).

The effect of aquifer outflow boundary location could be studied by comparing the results from runs CO2\_6 and CO2\_7. The location of the aquifer outflow boundary had very little effect on the amount of CO<sub>2</sub> injected as shown in Figure 4.11. A comparison of pressure distribution after 30 years at a depth of 45.9 m from the top of the aquifer (i.e. the centre of gridblocks at K=5) as shown in Figure 4.12 also indicated that by moving the outflow boundary from 5 km to 0.65 km, there was very little effect on the numerical predictions. By moving the outflow boundary from 5 km to 0.65 km, the number of gridblocks could be reduced from 330 to 140 and the CPU time of the numerical run could be reduced by more than half. The numerical results indicated that choosing a 3 inch radius injector with a completion of 11 m near the bottom of the aquifer, an average of approximately 100 t/day of CO<sub>2</sub> could be injected into the Wabamun Lake area aquifer without fracturing. At this CO<sub>2</sub> injection rate, the average water rate due to the CO<sub>2</sub> injection at 5 km from the injector was less than 0.11 cm/year as shown in Figure 4.13. This indicated that the CO<sub>2</sub> disposal operation had an insignificant effect on the natural flow of the aquifer (approximately 1 cm/year) far away from the injector.

The effect of injection radius and completion could be studied by comparing the results from runs CO2\_7-9. It is noted that the injection rate is directly proportional to the completion interval of the injector and is inversely proportional to  $\ln(1/\text{injector radius})$ . As shown in Figure 4.14, by increasing the completion interval from 11 m to 55 m, the average CO<sub>2</sub> injection rate increased from 100 t/day to approximately 180 t/day. On the other hand, by increasing the injector radius from 3 inch to 4 inch, there was very little effect on the amount of CO<sub>2</sub> injected. Slightly more CO<sub>2</sub> could be injected when a 4 inch radius injector was chosen. A comparison of pressure distribution after 30 years at a depth of 45.9 m from the top of the aquifer as shown in Figure 4.15 indicated that aquifer was pressurized faster when a larger completion interval was chosen due to the higher injection rate.

**Table 4.1  
Numerical Runs**

All runs simulated a 30-year CO<sub>2</sub> injection period.

---

**Grid Pattern: 66 X 1 X 5 (Location of Aquifer Outflow Boundary = 5 km)**

<u>Run No.:</u>	<u>Injected Fluid:</u>	<u>Injector Radius:</u>	<u>Injector Completion:</u>
CO2_6	CO <sub>2</sub>	3"	11 m
CO2_12	CO <sub>2</sub>	3"	55 m
H2O_4	H <sub>2</sub> O	3"	11 m

For Run CO2\_12, the absolute permeability in the horizontal and the vertical directions were 13 and 3.9 mD, respectively. Run CO2\_12 simulated a total of 40 years that included a 10-year period after the shutin of the injector.

---

**Grid Pattern: 28 X 1 X 5 (Location of Aquifer Outflow Boundary = 0.65 km)**

<u>Run No.:</u>	<u>Injected Fluid:</u>	<u>Injector Radius:</u>	<u>Injector Completion:</u>
CO2_7	CO2	3"	11 m
CO2_8	CO2	3"	55 m
CO2_9	CO2	4"	55 m

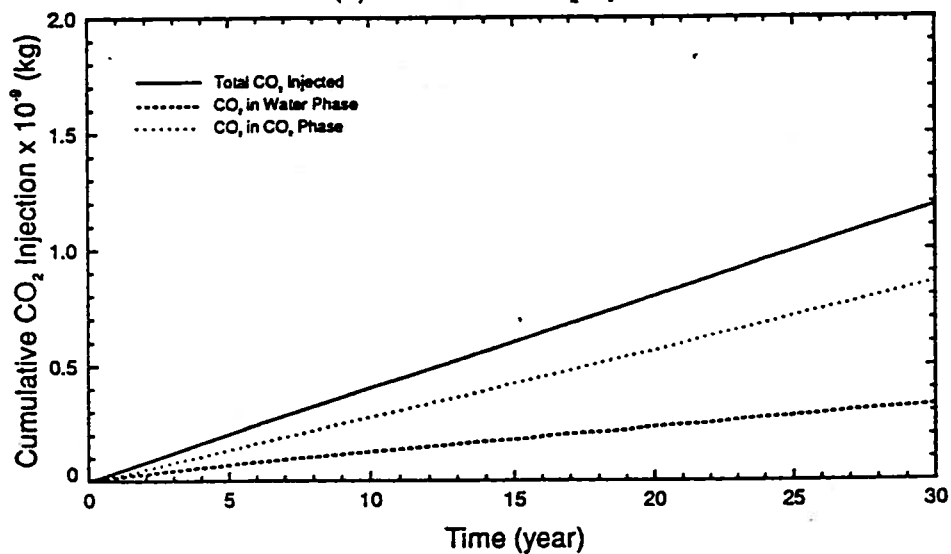
---

Figure 4.3  
CO<sub>2</sub> Injection for Numerical Run CO2\_6

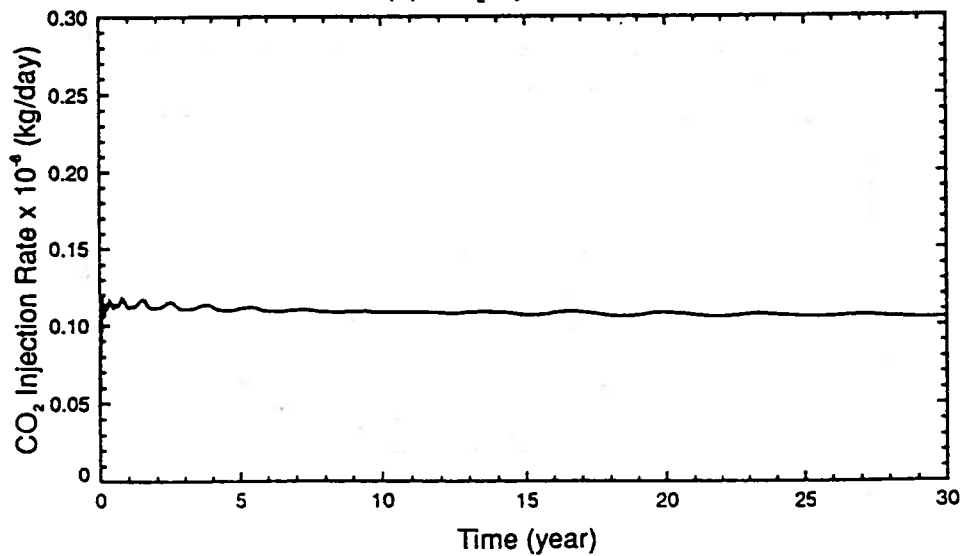
Location of Aquifer Outflow Boundary = 5 km

Injector Radius = 3"    Injector Completion = 11 m (Bottom)

(a) Cumulative CO<sub>2</sub> Injection



(b) CO<sub>2</sub> Injection Rate



1000 kg = 1 t

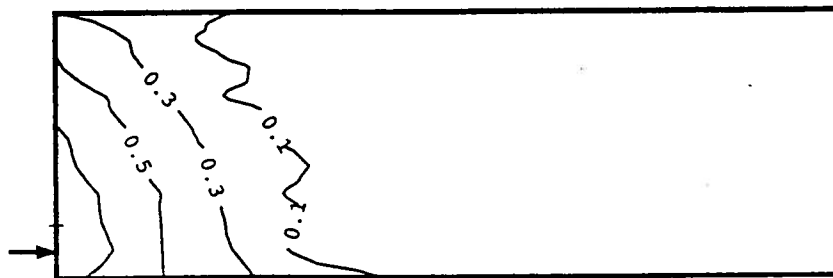


Figure 4.4  
CO<sub>2</sub> Saturation Contours for Numerical Run CO2\_6

Location of Aquifer Outflow Boundary = 5 km

Injector radius = 3" Injector Completion = 11 m (Bottom)

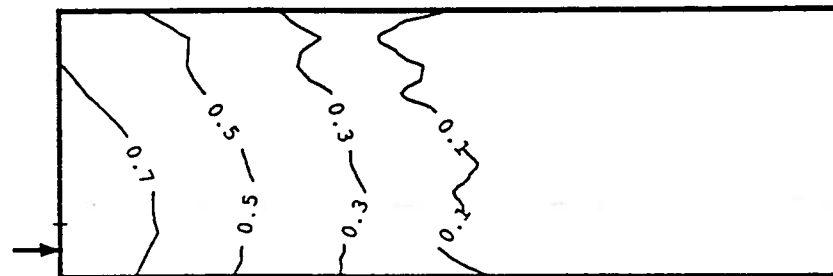
Vertical Dimension = 55 m Horizontal Dimension = 650 m



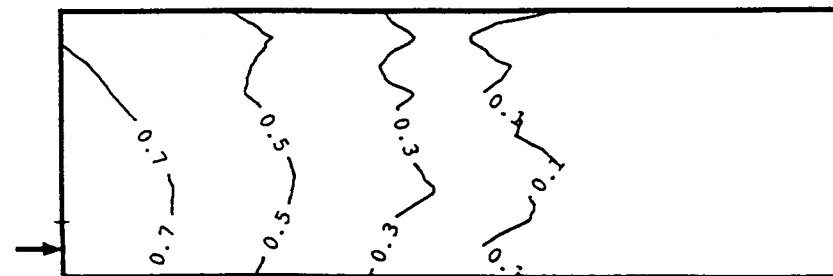
(a) after 5 years



(b) after 10 years



(c) after 20 years



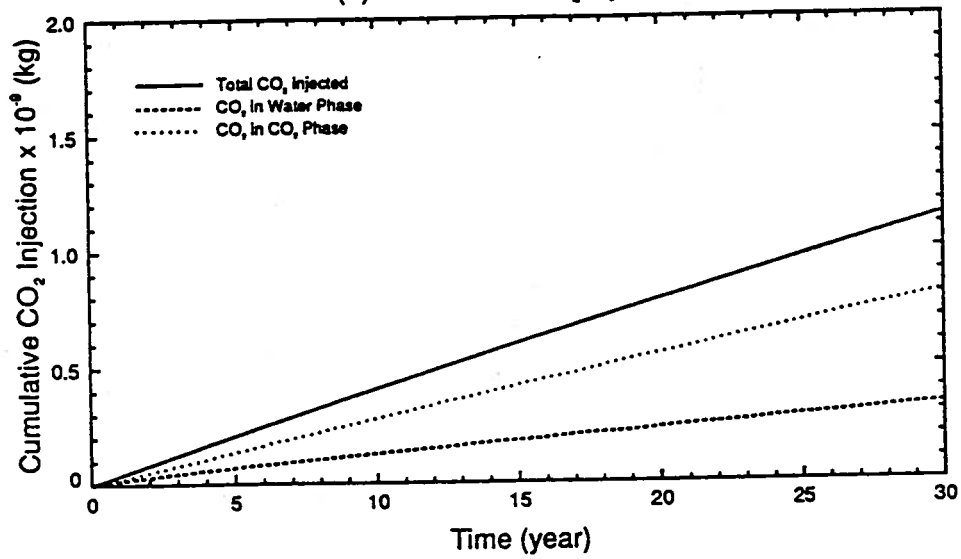
(d) after 30 years

Figure 4.5  
CO<sub>2</sub> Injection for Numerical Run CO2\_7

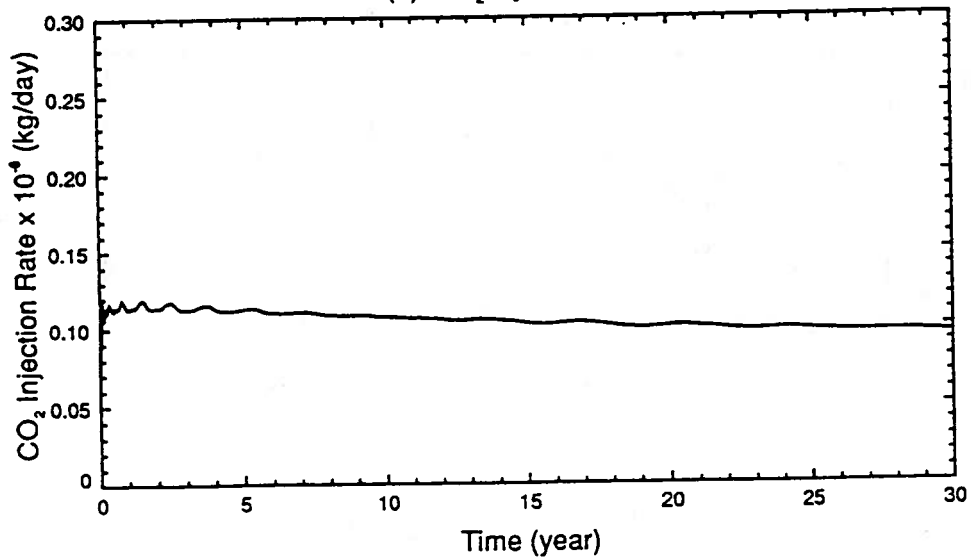
Location of Aquifer Outflow Boundary = 0.65 km

Injector Radius = 3" Injector Completion = 11 m (Bottom)

(a) Cumulative CO<sub>2</sub> Injection



(b) CO<sub>2</sub> Injection Rate



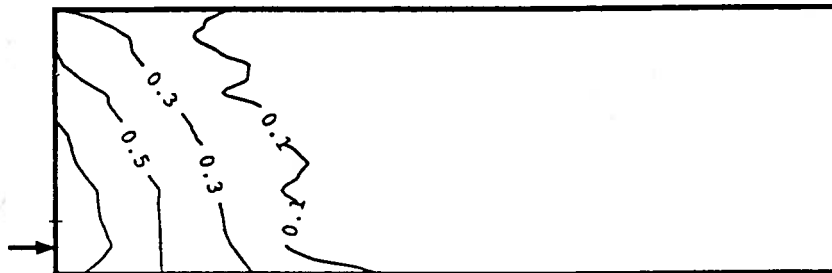
1000 kg = 1 t

**Figure 4.6**  
**CO<sub>2</sub> Saturation Contours for Numerical Run CO2\_7**

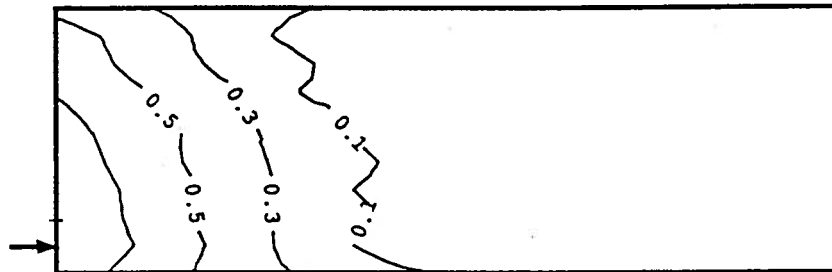
Location of Aquifer Outflow Boundary = 0.65 km

Injector radius = 3"    Injector Completion = 11 m (Bottom)

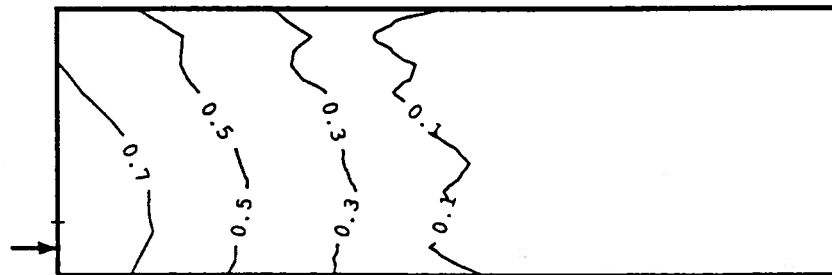
Vertical Dimension = 55 m    Horizontal Dimension = 650 m



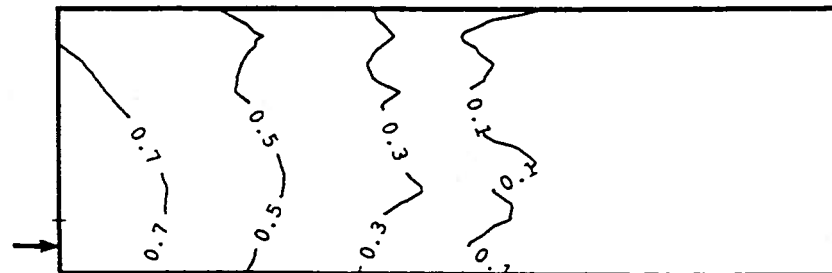
(a) after 5 years



(b) after 10 years



(c) after 20 years



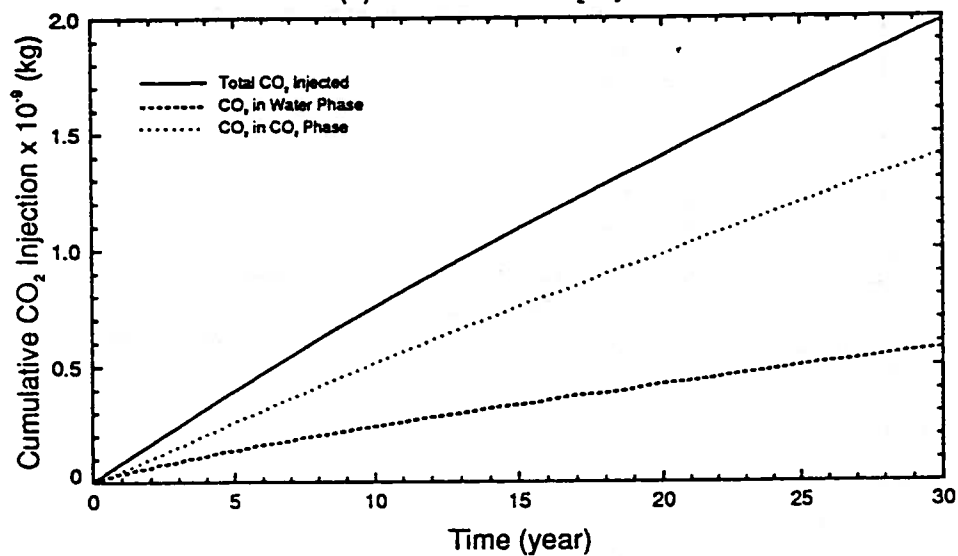
(d) after 30 years

Figure 4.7  
CO<sub>2</sub> Injection for Numerical Run CO2\_8

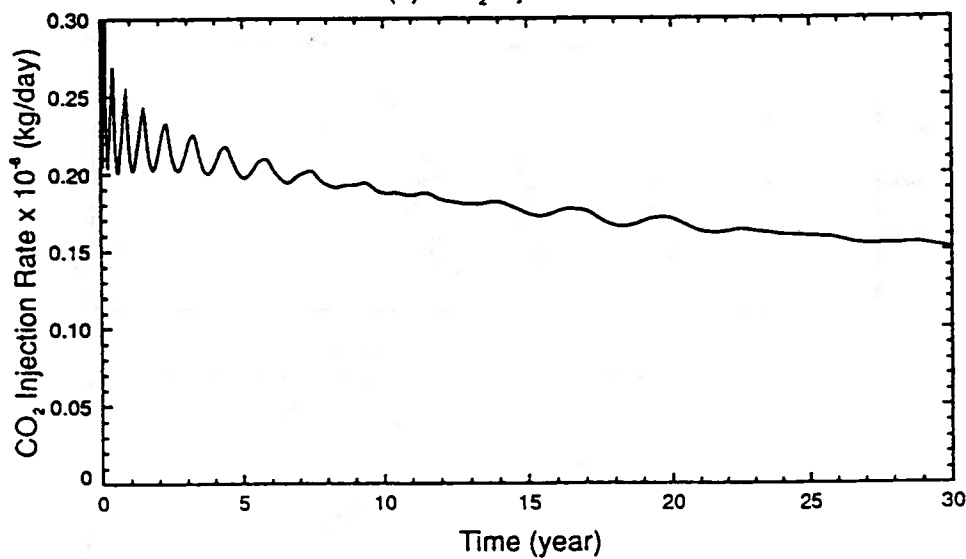
Location of Aquifer Outflow Boundary = 0.65 km

Injector Radius = 3"    Injector Completion = 55 m

(a) Cumulative CO<sub>2</sub> Injection



(b) CO<sub>2</sub> Injection Rate



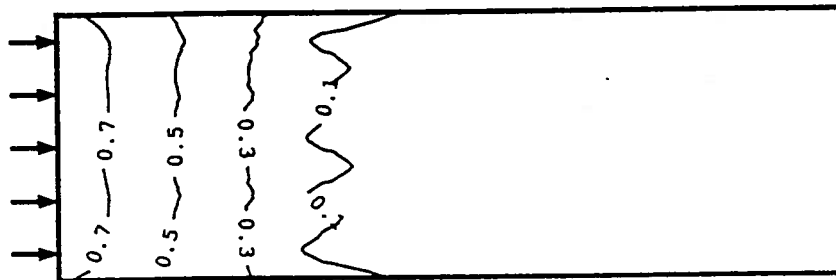
1000 kg = 1 t

Figure 4.8  
CO<sub>2</sub> Saturation Contours for Numerical Run CO2\_8

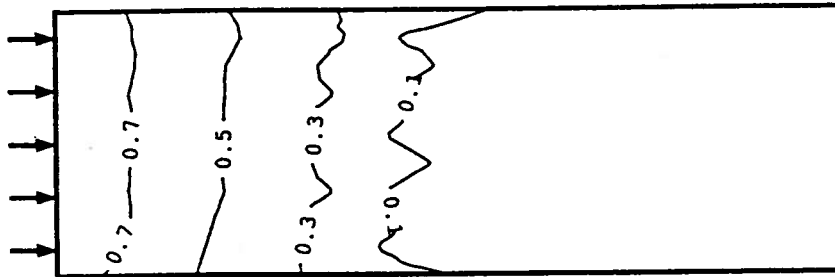
Location of Aquifer Outflow Boundary = 0.65 km

Injector radius = 3"    Injector Completion = 55 m

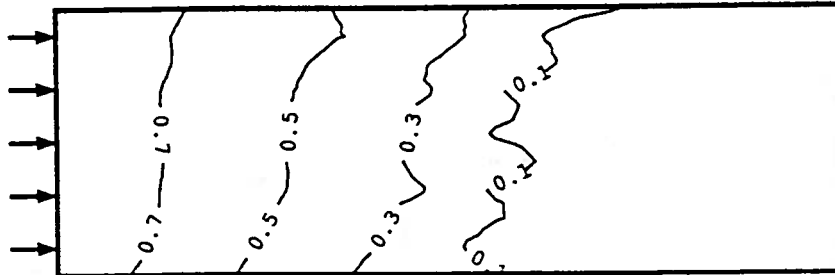
Vertical Dimension = 55 m    Horizontal Dimension = 650 m



(a) after 5 years



(b) after 10 years



(c) after 20 years

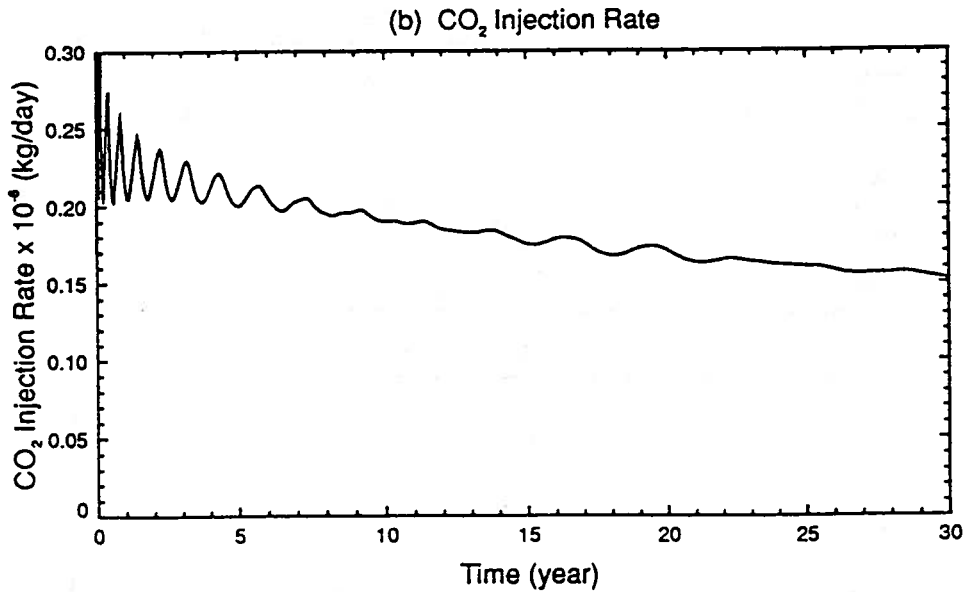
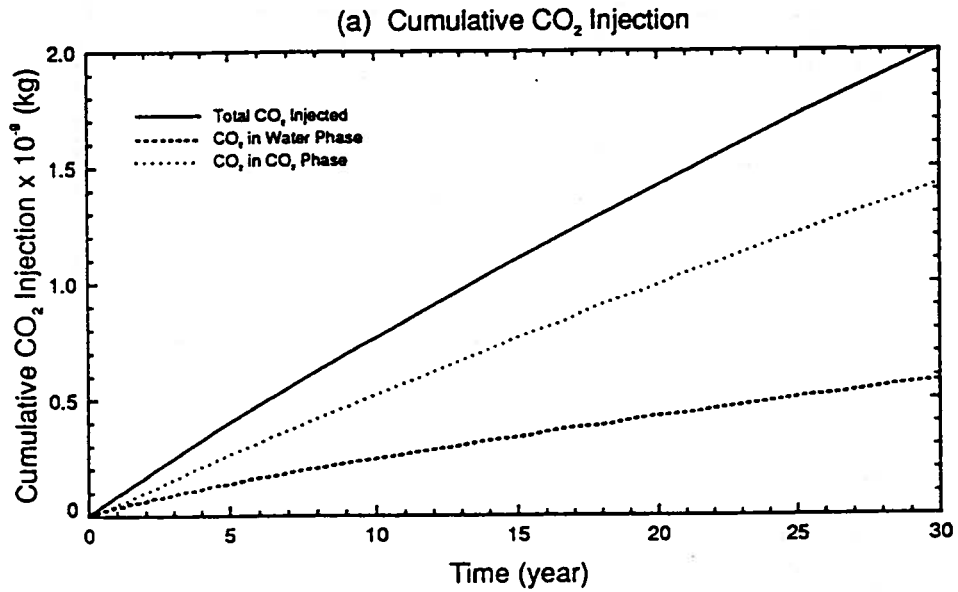


(d) after 30 years

**Figure 4.9**  
**CO<sub>2</sub> Injection for Numerical Run CO2\_9**

Location of Aquifer Outflow Boundary = 0.65 km

Injector Radius = 4"    Injector Completion = 55 m



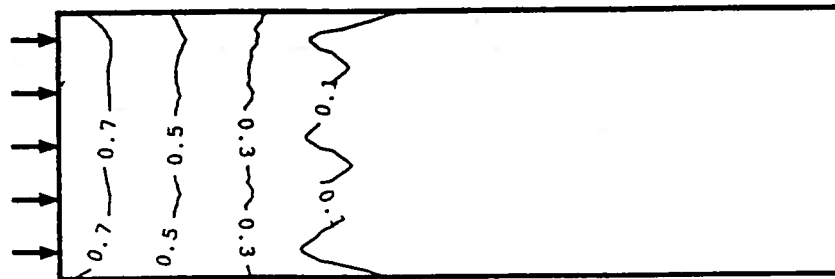
1000 kg = 1 t

**Figure 4.10**  
**CO<sub>2</sub> Saturation Contours for Numerical Run CO2\_9**

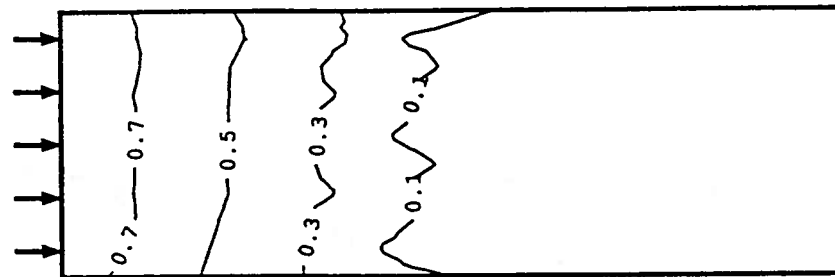
Location of Aquifer Outflow Boundary = 0.65 km

Injector radius = 4"    Injector Completion = 55 m

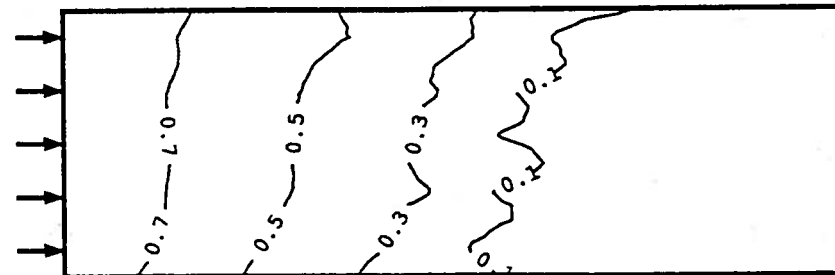
Vertical Dimension = 55 m    Horizontal Dimension = 650 m



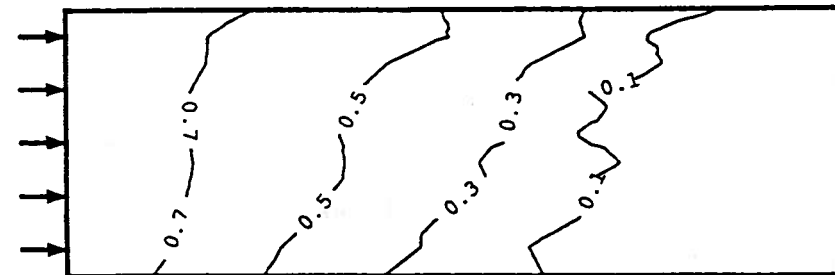
(a) after 5 years



(b) after 10 years



(c) after 20 years

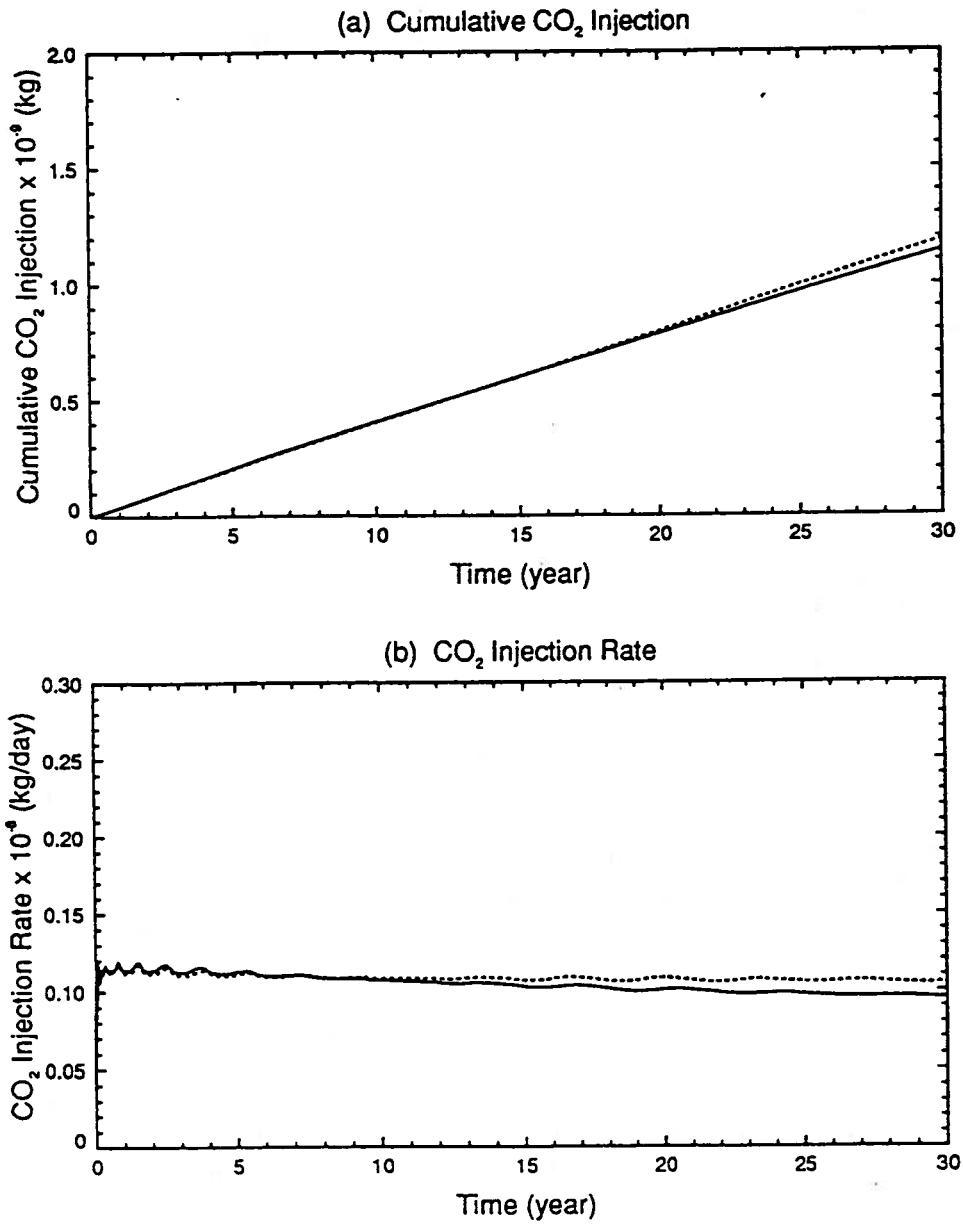


(d) after 30 years

**Figure 4.11**  
**Effect of Aquifer Outflow Boundary Location on CO<sub>2</sub> Injection**

Injector Radius = 3"    Injector Completion = 11 m (Bottom)

— Aquifer Outflow Boundary = 0.65 km  
- - - Aquifer Outflow Boundary = 5 km



1000 kg = 1 t



**Figure 4.12**  
**Effect of Aquifer Outflow Boundary Location**  
**on Pressure Distribution After 30 Years**

Injector Radius = 3"    Injector Completion = 11 m (Bottom)

—— Aquifer Outflow Boundary = 0.65 km

..... Aquifer Outflow Boundary = 5 km

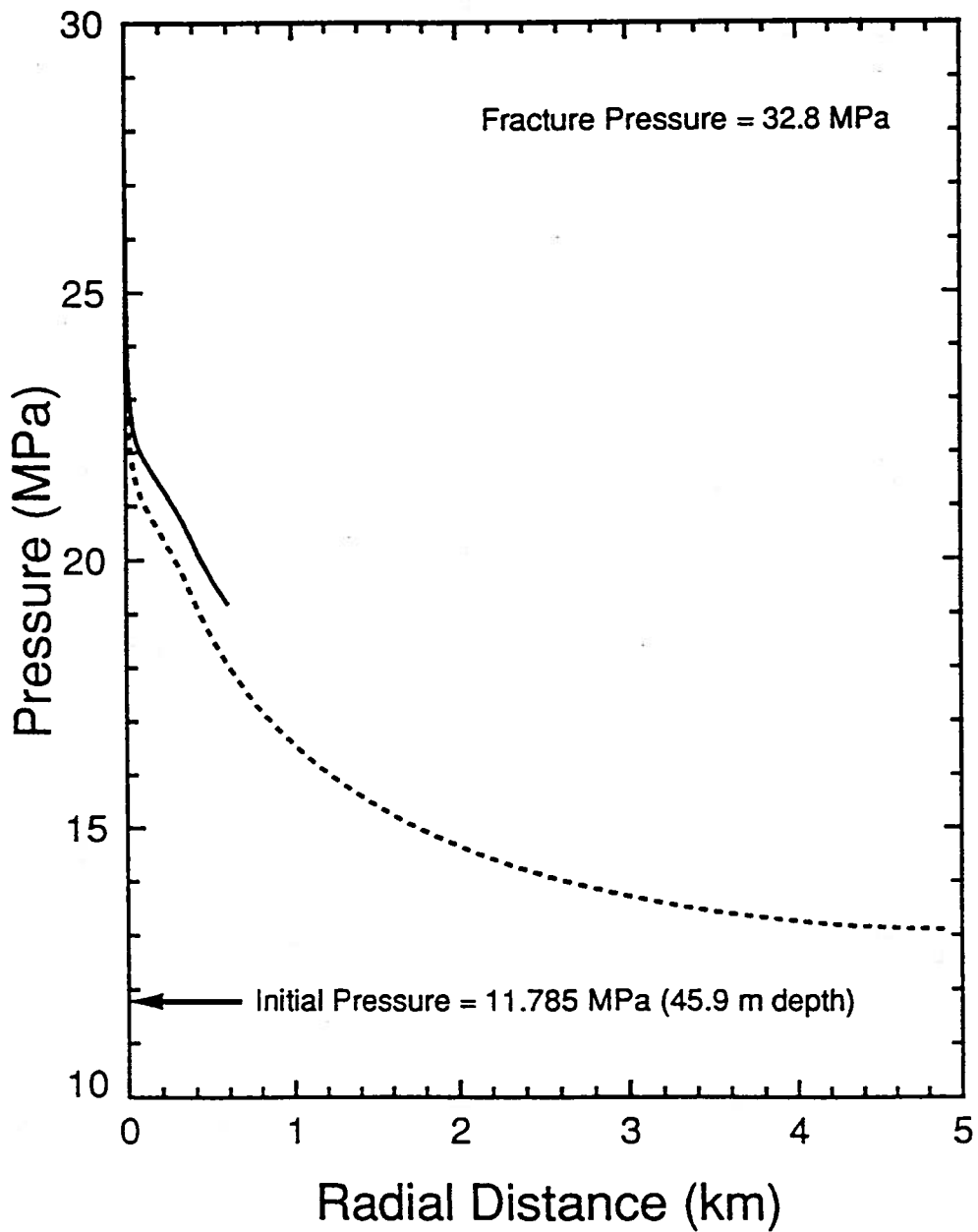
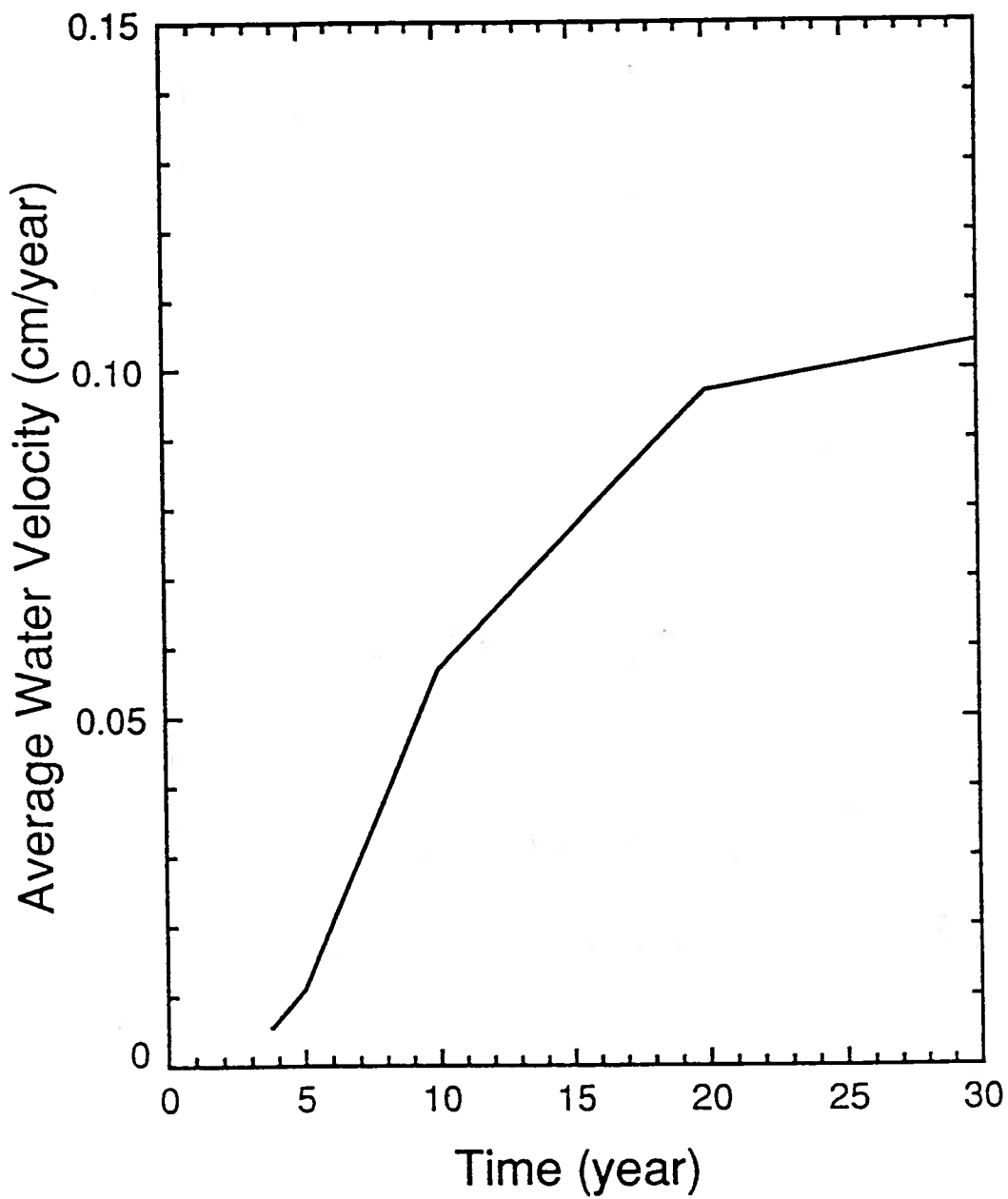


Figure 4.13  
Average Water Velocity at 5 km from Injector (Run CO2\_6)

Location of Aquifer Outflow Boundary = 5 km

Injector Radius = 3" Injector Completion = 11 m (Bottom)

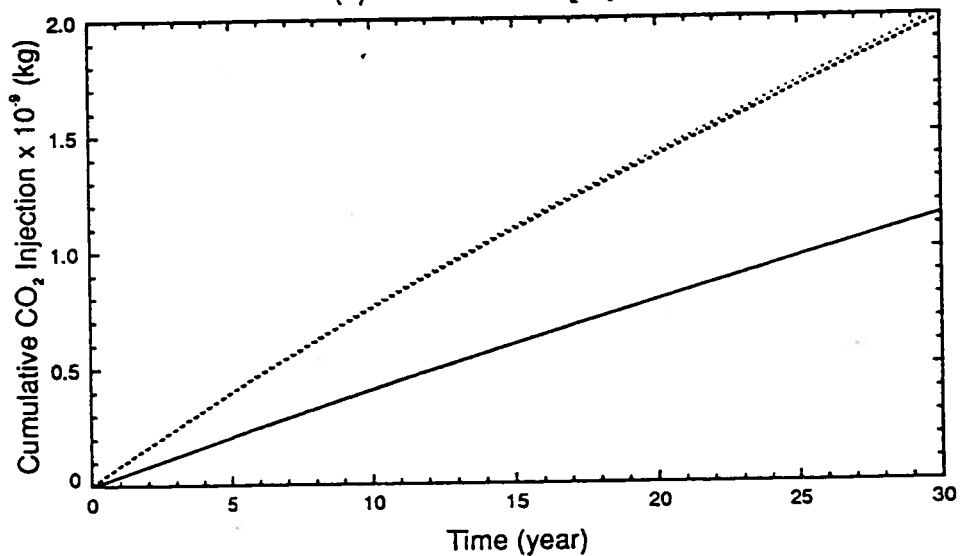


**Figure 4.14**  
**Effect of Injector Radius and Completion on CO<sub>2</sub> Injection**

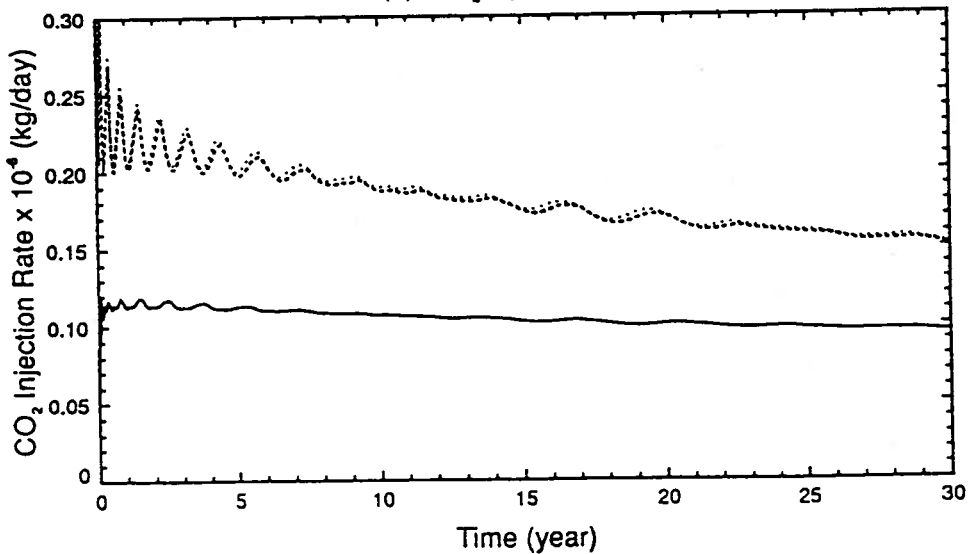
Location of Aquifer Outflow Boundary = 0.65 km

- Injector Radius = 3" Injector Completion = 11 m (Bottom)
- - - Injector Radius = 3" Injector Completion = 55 m
- · · Injector Radius = 4" Injector Completion = 55 m

(a) Cumulative CO<sub>2</sub> Injection

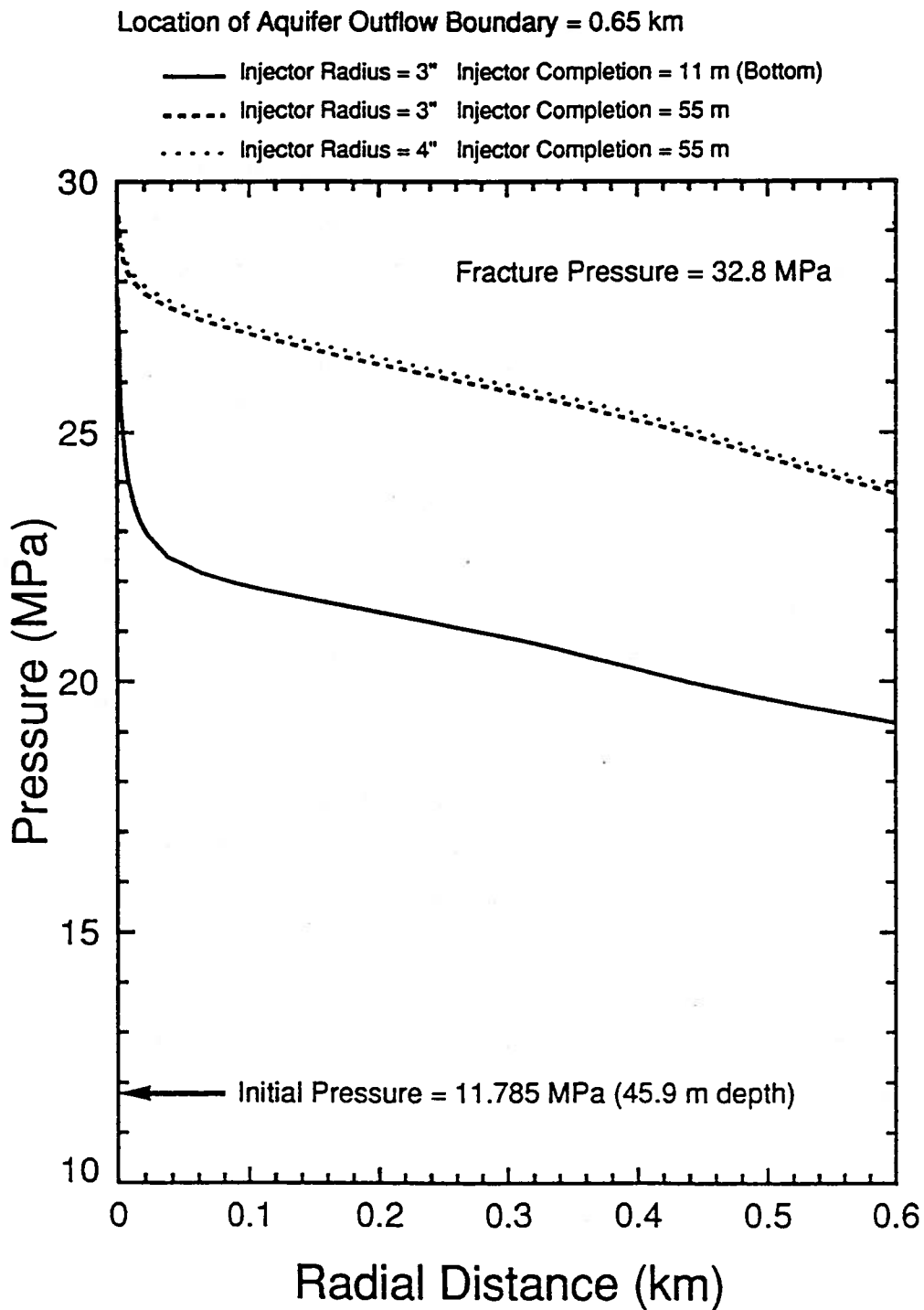


(b) CO<sub>2</sub> Injection Rate



1000 kg = 1 t

**Figure 4.15**  
**Effect of Injector Radius and Completion**  
**on Pressure Distribution After 30 Years**



The effect of injected fluid could be studied by comparing the results from runs CO2\_6 and H2O\_4. As shown in Figure 4.16, under the same operating conditions, the amount of CO<sub>2</sub> injected was almost 5.5 times that of water mainly because the viscosity of CO<sub>2</sub> was almost two orders of magnitude lower than that of water. This indicated that an alternative by dissolving CO<sub>2</sub> into water first before injection was not as feasible as injecting the CO<sub>2</sub> under supercritical conditions.

The effect of absolute permeability of the aquifer could be studied by comparing the results from runs CO2\_8 and CO2\_12. Numerical predictions of cumulative CO<sub>2</sub> injection, CO<sub>2</sub> injection rate, CO<sub>2</sub> saturation contours and pressure distribution as a function of time for run CO2\_12 are given in Figure 4.17-4.21. As shown in Figure 4.17, by increasing the absolute permeabilities in all directions by 10 times, the average CO<sub>2</sub> injection rate increased from 180 t/day (Figure 4.14) to 1735 t/day. Due to this high injection rate, CO<sub>2</sub> override was significant and CO<sub>2</sub> propagated almost 2 km away from the injector after 30 years (see Figure 4.18). Even 10 years after the shut-in of the injector, the profile of the CO<sub>2</sub> saturation remained almost the same (see Figure 4.19). Under the same operating conditions, the aquifer with a higher absolute permeability (see radial distance = 0.6 in Figure 4.20) pressurized faster than the aquifer with a lower absolute permeability (Figure 4.15). After the shut-in of the injector, the aquifer depressurized rather slowly (Figure 4.21). Even 10 years after the shut-in of the injector, the pressure at a depth of 49.5 m from the top of the aquifer was approximately 19 MPa compared to the initial value of 11.785 MPa. At the high CO<sub>2</sub> injection rate, the average water rate due to CO<sub>2</sub> injection at 5 km from the injector reached as high as 28 cm/year as shown in Figure 4.22. Even 10 years after the shut-in of the injector, this water rate only reduced to 10 cm/year. This indicated that the CO<sub>2</sub> disposal operation in a relatively high permeability aquifer (13 mD) had a significant effect on the natural flow of the aquifer even 5 km away from the injector.

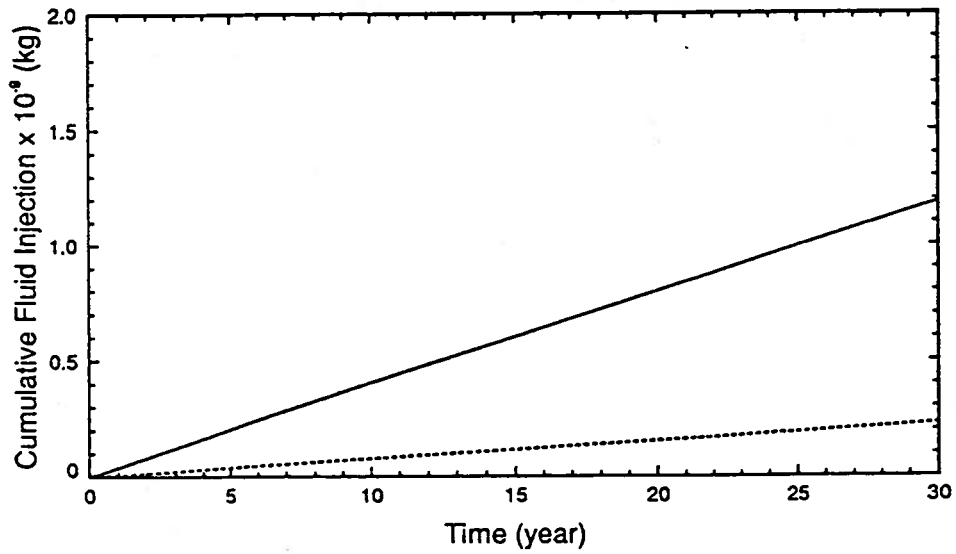
**Figure 4.16**  
**Effect of Injected Fluid on CO<sub>2</sub> Injection**

Location of Aquifer Outflow Boundary = 5 km

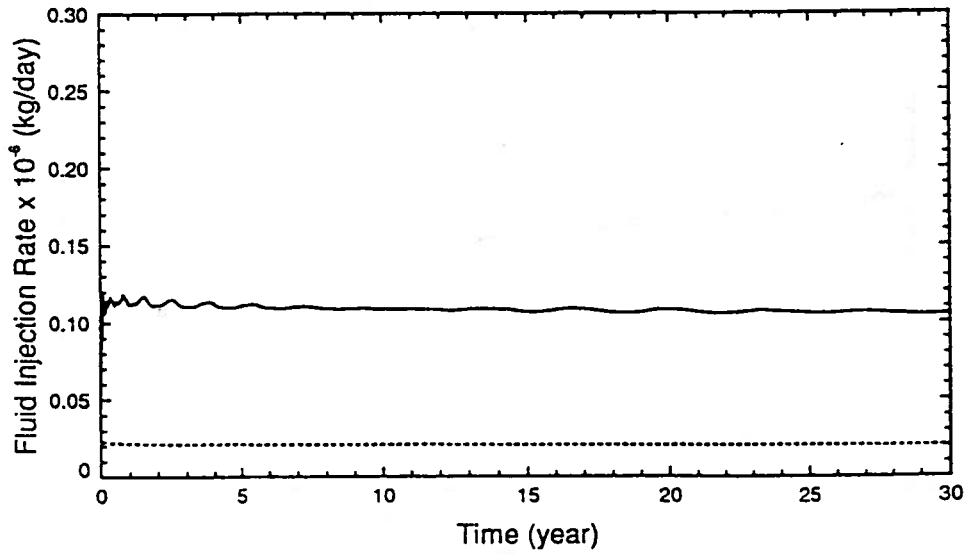
Injector Radius = 3"    Injector Completion = 11 m (Bottom)

— Injected CO<sub>2</sub>  
- - - - - Injected H<sub>2</sub>O

(a) Cumulative Fluid Injection



(b) Fluid Injection Rate



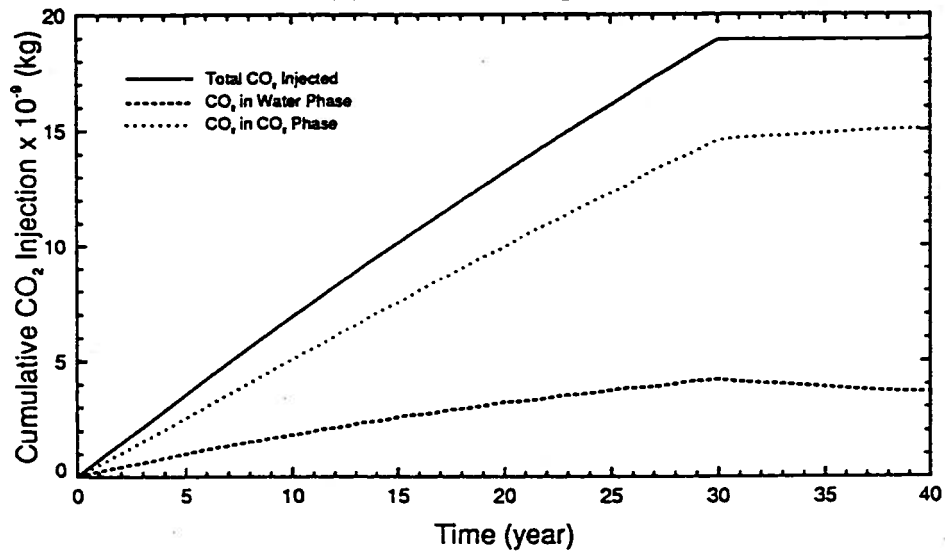
1000 kg = 1 t

Figure 4.17  
CO<sub>2</sub> Injection for Numerical Run CO2\_12

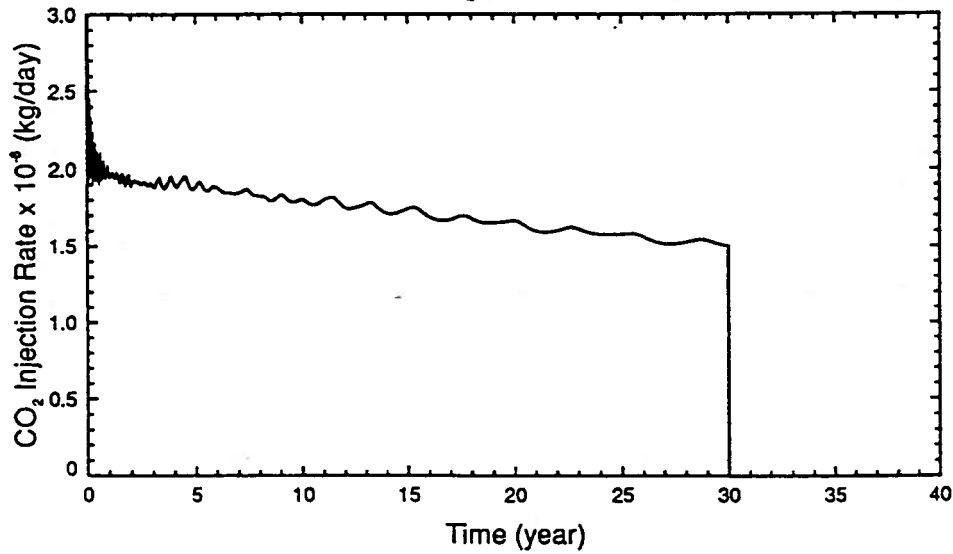
Location of Aquifer Outflow Boundary = 5 km

Injector Radius = 3"    Injector Completion = 55 m

(a) Cumulative CO<sub>2</sub> Injection



(b) CO<sub>2</sub> Injection Rate



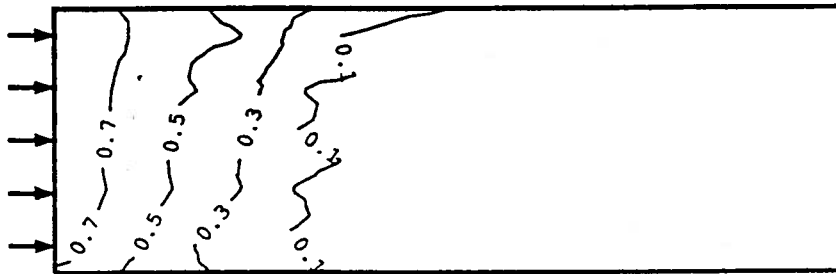
1000 kg = 1 t

**Figure 4.18**  
**CO<sub>2</sub> Saturation Contours for Numerical Run CO2\_12**

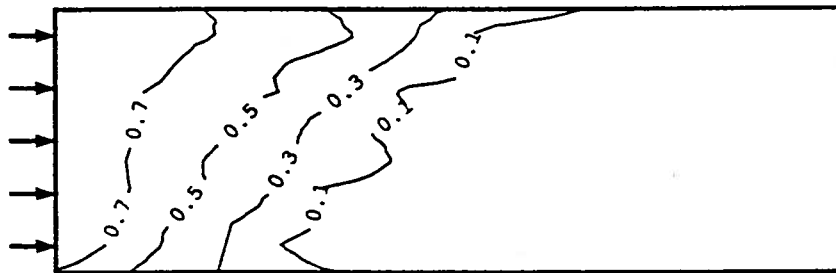
Location of Aquifer Outflow Boundary = 5 km

Injector radius = 3"    Injector Completion = 55 m

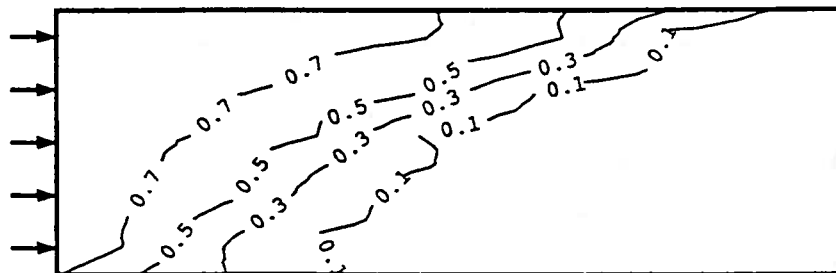
Vertical Dimension = 55 m    Horizontal Dimension = 2 km



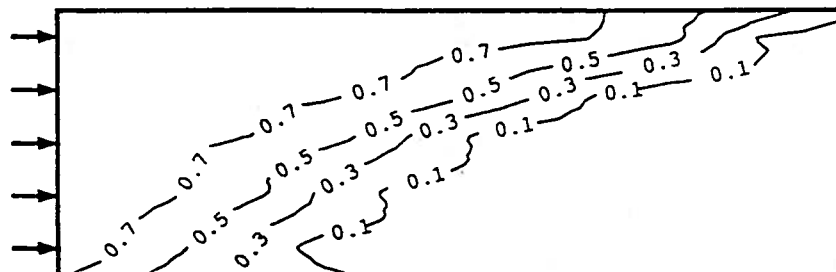
(a) after 5 years



(b) after 10 years



(c) after 20 years



(d) after 30 years

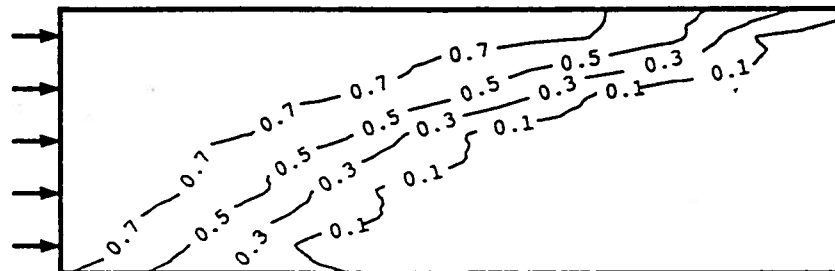


**Figure 4.19**  
**CO<sub>2</sub> Saturation Contours for Numerical Run CO2\_12**  
**(After Shut-in)**

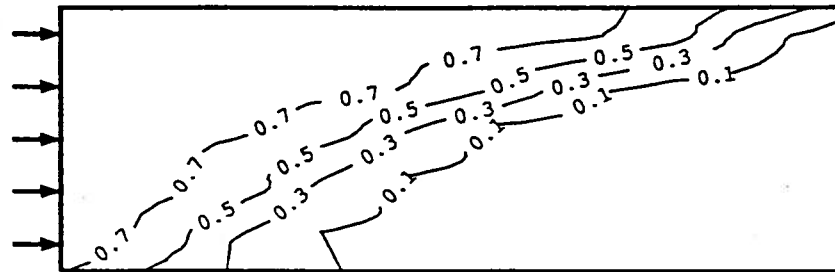
Location of Aquifer Outflow Boundary = 5 km

Injector radius = 3"    Injector Completion = 55 m

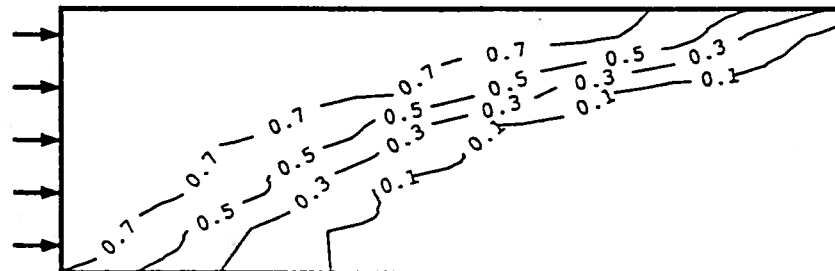
Vertical Dimension = 55 m    Horizontal Dimension = 2 km



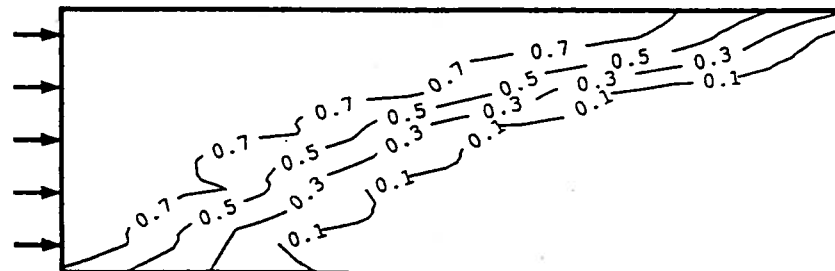
(a) after 30 years (injector shutin)



(b) after 32 years



(c) after 35 years



(d) after 40 years

Figure 4.20  
Pressure Distribution for Numerical Run CO2\_12

Location of Aquifer Outflow Boundary = 5 km

Injector Radius = 3" Injector Completion = 55 m

..... After 10 years

----- After 20 years

———— After 30 years

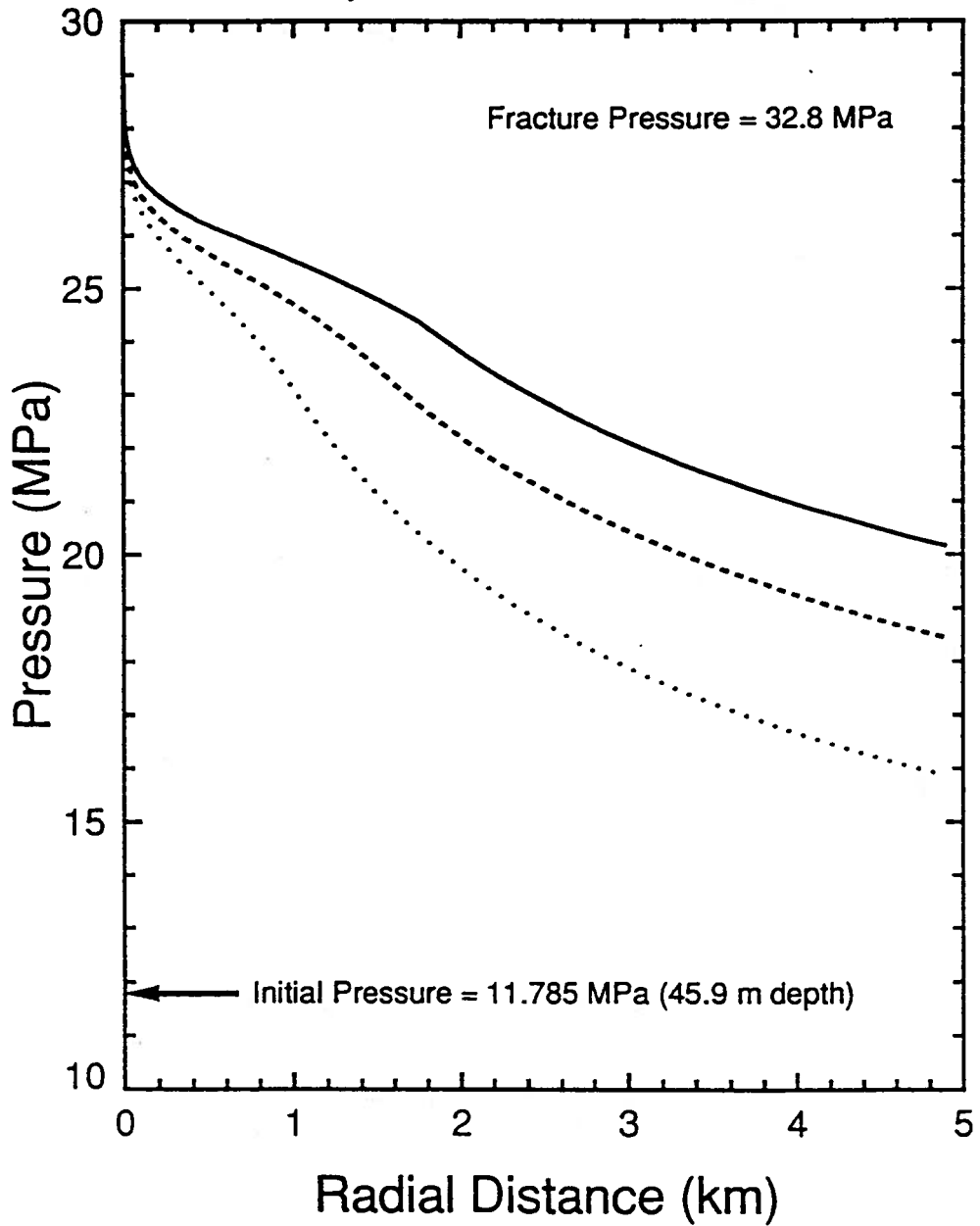
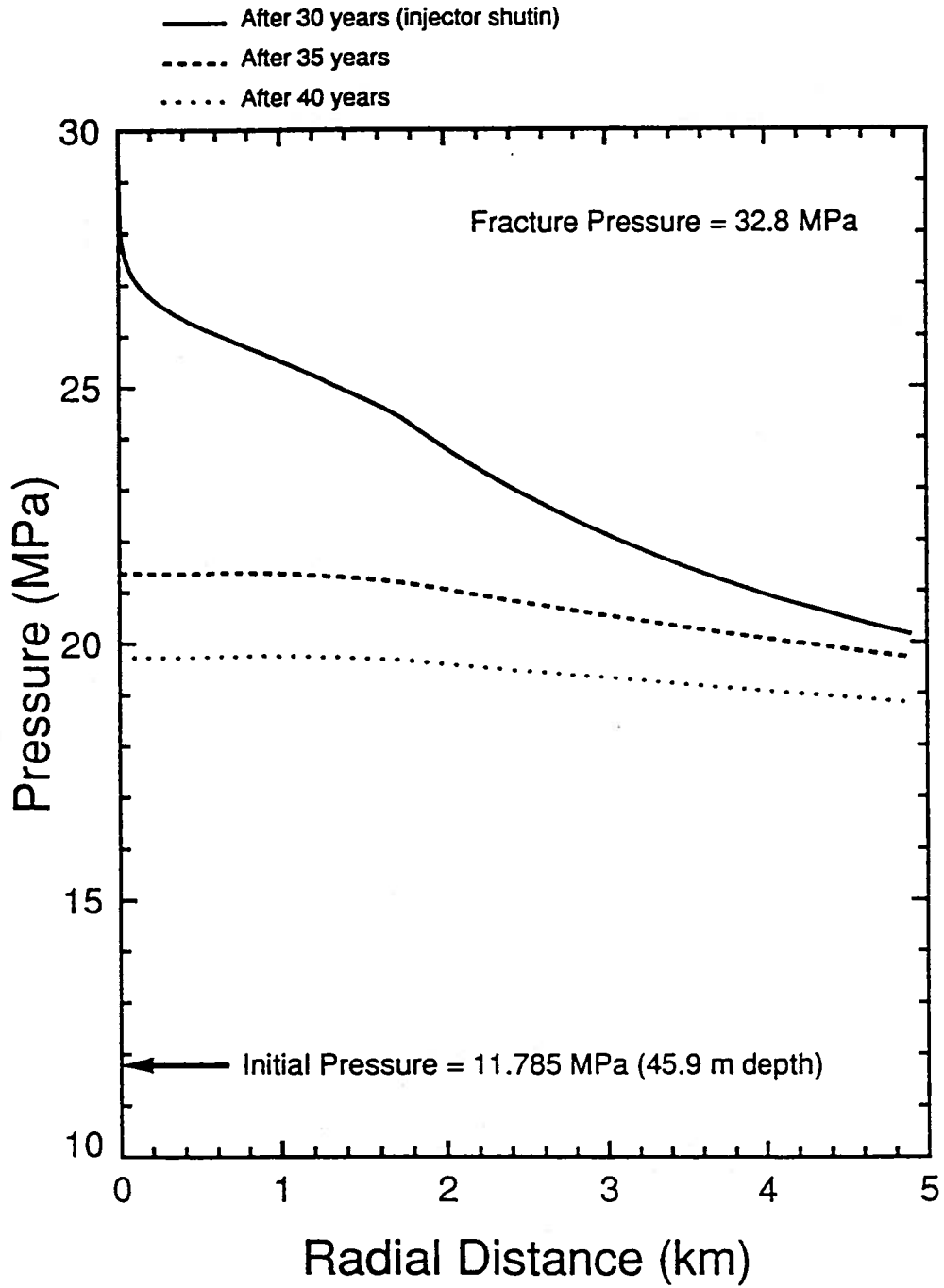


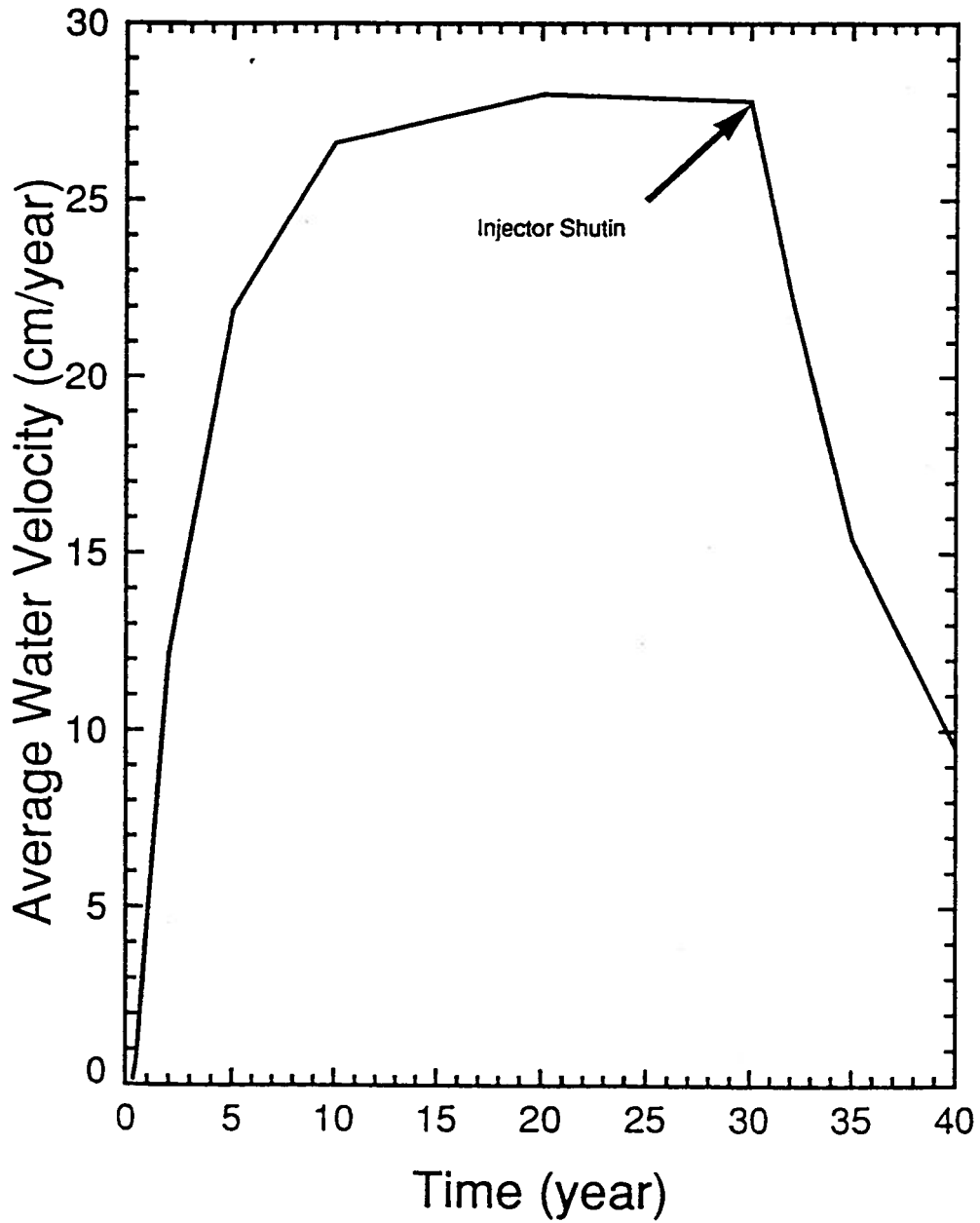
Figure 4.21  
Pressure Distribution for Numerical Run CO2\_12  
(After Shut-in)

Location of Aquifer Outflow Boundary = 5 km  
Injector Radius = 3" Injector Completion = 55 m



**Figure 4.22**  
**Average Water Velocity at 5 km from Injector (Run CO2\_12)**

Location of Aquifer Outflow Boundary = 5 km  
Injector Radius = 3" Injector Completion = 55 m



## 5.0 MODELLING OF CO<sub>2</sub> RESERVOIR REACTIONS

### 5.1 PREAMBLE

Geological CO<sub>2</sub> sinks, depending upon the time scale, may be classified as reactive or inert. Clearly, reactive sinks are the most effective for permanent, long-term disposal. Injection into aquifers, and the subsequent dissolution into the water, increases the reactivity of CO<sub>2</sub> considerably. In addition, flow through porous media in the crust promotes natural mixing and exposure of the dissolved CO<sub>2</sub> to additional grain surfaces where reactions can take place.

In this section, the primary focus is on the generic documentation of the enhancement of CO<sub>2</sub> capture by aquifer water-rock interaction. We distinguish three scenarios in the use of aquifers for the disposal of CO<sub>2</sub>:

- 1) The solution of CO<sub>2</sub> into a formation fluid in the absence of formation mineralogy;
- 2) The solution of CO<sub>2</sub> and reaction with the minerals present in a carbonate aquifer;
- 3) The solution of CO<sub>2</sub> and reaction with the minerals in a dominantly siliciclastic aquifer.

These scenarios are tested on aquifers in an area close to the Sundance and Genesee power plants.

## 5.2 FORMATION WATER CHEMISTRY ADJUSTMENTS

The formation water analyses described earlier are often limited with sodium or chloride values calculated by difference. Silica and other potentially important components were never measured. Even in the best analyses, the only anions directly measured were chloride and sulphate; with a total alkalinity assumed to represent carbonate and bicarbonate ion concentrations. This assumption can lead to significant error in the calculated amounts of total inorganic carbon (TIC) when other anions (ammonium and organic acids among others) are present.

Many of the samples are above or near equilibrium with atmospheric carbon dioxide partial pressure, thus implying that the formation water sample has probably released carbon dioxide between the time of sampling and the time of analysis. A number of samples are also supersaturated with carbonate minerals, notably calcite. This is impossible in the formation due to the extremely fast rates of reactions of carbonate minerals and the low residency time of the formation waters. Corrections for these two *sampling* errors can be undertaken if sufficient information is known or can be assumed.

Two waters (brackish and a brine) were chosen as the basis for the modelling, each representing an extreme in TDS (i.e. approximately 4,000 versus 100,000 ppm). Sodium, potassium, calcium, magnesium and chloride are all more than an order of magnitude higher in the brine while sulphate is three times higher and bicarbonate is actually lower (Table 5.1). The actual composition chosen for modelling depended on corrections as discussed below and simplification of the formation water chemistry pertinent to the end member mineralogy being modeled.

## Representative Brine H<sub>2</sub>O

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73666 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1545304

CORE LABORATORIES CANADA LT. Lab. Sample ID. C84-5196-4

Well identifier Well name KB elev. Gr. elev  
 0495051416020 PROPHET ET AL PEMBINA 16-14-49-5 799.60 795.60

Interval Sampled from: 1739.00 to: 1746.00 meters KB

Formation Sampled: MISS SYS

Sample produced by: DST # 1 Sampling point: DOWN HOLE SAMPLE  
 DST Recovery

58.00 M CLEAN OIL  
 258.00 M OIL- AND GAS-CUT SALT WATER

Date: Sampled: 1984/06/08 Received: 1984/06/18 Analyzed: 1984/06/21

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	33900.	41.029	1474.6	Cl	63000.	49.444	1777.0
K	813.	0.579	20.8	HCO3	944.	0.430	15.5
Ca	4084.	5.670	203.8	SO4	689.	0.399	14.3
Mg	1069.	2.448	88.0				

Specific gravity 1.0680 @ 25. C Refractive Index 1.34950 @ 25. C  
 PH 7.20 @ 25. C Resistivity ohm/m 0.07900 @ 25. C

Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 34835. Calculated TDS: 104141.  
 TDS by Evapor. @ 110 C: 116200. TDS at Ignition: 101700.

Sample appearance:

A LYNES UNITED DOWNHOLE SAMPLER 214. WAS REC'D UNDER 689 KPA PRESSURE. RECOVERED FROM THE CHAMBER WAS GAS AND 1.9 L OF OIL STAINED MUDDY SALT WATER.

Remarks:

Fe PRESENT

## Representative Brackish H<sub>2</sub>O

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80735 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44545

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E80-13493-3

Well identifier Well name KB elev. Gr. elev  
 0515040313000 ANDEX ET AL HIGHVALE 13-3-51-4 764.30 760.20

Interval Sampled from: 1578.00 to: 1586.00 meters KB

Formation Sampled: OSTRACODE

Sample produced by: DST # 1 Sampling point: 0 M ABO TOOL  
 DST Recovery

948.00 M CLEAN OIL  
 2.00 M SALT WATER

Date: Sampled: 1980/11/16 Received: 1980/11/25 Analyzed: 1980/12/16

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	1715.	48.734	74.6	Cl	1717.	31.639	48.4
K	18.	0.301	0.5	HCO3	1434.	15.353	23.5
Ca	21.	0.685	1.0	SO4	222.	3.020	4.6
Mg	5.	0.269	0.4				

Specific gravity 1.0030 @ 25. C Refractive Index 1.33360 @ 25. C  
 PH 8.40 @ 21. C Resistivity ohm/m 1.36000 @ 25. C

Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 1726. Calculated TDS: 4397.  
 TDS by Evapor. @ 110 C: 4530. TDS at Ignition: 4125.

Remarks:

FE NIL.

**Table 5.1  
 Representative Formation  
 Water Analyses of a  
 Dilute Water and Brine**

A number of corrections were made to these two waters. If a carbonate mineral was supersaturated, the TIC (total inorganic carbon) levels were increased through the addition of carbon dioxide until the mineral was at equilibrium with the solution. This modified the formation pH to more acid conditions. The concentration of missing components, if considered significant, was estimated by calculating what concentration would be in equilibrium with the reservoir mineralogy. For example, the concentration of dissolved silica was estimated by assuming equilibrium with quartz, yielding a concentration of approximately  $10^{-4}$  moles per litre.

These corrections to the brackish and brine formation waters provided the basis of the fluid compositions for the modelling. When modelling the interactions between the injected  $\text{CO}_2$ , the formation mineralogy and a formation fluid, the formation fluid should be in equilibrium with the formation mineralogy. As is discussed in more detail below, a range of stoichiometric formation mineralogies was used for the simulations, which were not necessarily in equilibrium with the corrected brackish and brine formation waters. When this occurred, the corrected brine and brackish formation waters were further modified in order to be closer to equilibrium with the formation mineralogies. These modifications would not be necessary if the appropriate formation water and the mineralogy of the injection horizon were being used for a site-specific study.

### 5.3 MODELLING OF WATER-ROCK REACTION

Modelling of water-rock reactions was carried out at an aquifer temperature of  $25^\circ\text{C}$  on stoichiometric end member mineralogies (i.e. pure Na-, K-, Ca- and Mg- minerals) using the mass transfer geochemical computer code PATH.ubc (Perkins, 1980) and GeoCalc (Brown et al., 1989). PATH.ubc calculates the path of water-rock reaction for a given set of reactants as a function of the progress variable, 'XI' which is proportional to the log of time. 'XI' is used to define the molar amount of reactant phases added to the aqueous phase per step. This effectively results in linear kinetics. The relative reaction rate for each reactant



are defined by a user-specified factor with the default of one normally being used. The modelling does not take into account the effects of solid solution on the size of each of the mineral stability fields, even though the end-member feldspars, zeolites and clays generally do form solid solutions with the other end-members in the same mineral group. The reason for this assumption is simplicity; the thermodynamic data for solid solution minerals is non-existent or poor, and the numerical methods for calculating dynamic equilibria for solid solution minerals are intractable. These reasons also explain why the GeoCalc and PATH.ubc calculations do not include the effects of solid solution equilibria.

The initial conditions for PATH.ubc comprise the formation water chemistry, the number of grams of each of the formation minerals in equilibrium with the formation water (equilibrium phases) and the reactant phases ( $\text{CO}_2$  is a reactant phase in the context of the modelling). As 'XI' progresses, the reactants dissolve into the formation water, resulting in a different formation water composition. The change in formation water composition may be buffered by the precipitation (or dissolution) of the equilibrium phases or by the formation of new equilibrium phases. Often an equilibrium phase is formed but later completely reacts, and none is left in the system. PATH.ubc terminates when equilibrium has been achieved with all of the reactant phase(s) and/or when all of the reactant phase(s) have reacted.

Several formation water chemistries have been chosen to represent the spectrum of water chemistry as described above. The equilibrium phases used for the initial conditions were based upon the observed formation mineralogy, but modified to obtain the necessary *end member composition* constraints. The amount of equilibrium minerals present is calculated from the porosity. Assuming an average porosity of 10% and an average rock density of 2.5, there are approximately 22,000 grams of rock per 1000 grams of water. Even if the porosity is doubled to 20%, the weight of rock would only be reduced to 10,000 grams. For the former case, the presence of 5 wt% of a mineral phase would account for 1000 grams of that phase being contacted by 1000 grams of water.

Final equilibrium with the injected CO<sub>2</sub> is defined as when the partial pressure of CO<sub>2</sub> in equilibrium with the formation fluid is 15 MPa. This value was chosen as it is representative of the minimum injection pressure for liquid CO<sub>2</sub> necessary for injection into the deep aquifers below the Genesee and Sundance power stations.

#### 5.4 CO<sub>2</sub> SOLUBILITY IN BRACKISH WATER AND IN BRINE

If carbon dioxide is dissolved into either a brine water (i.e. TDS is greater than 100,000 mg/l) or brackish water (i.e. TDS lies between 1000 and 10,000 mg/l) with no formation minerals present, no new minerals are precipitated. The water becomes more acidic and the amount of dissolved carbon dioxide is a function of pressure and fluid composition. A salting out effect occurs as the water becomes more concentrated. The basis for these results is shown through the following model simulations.

CO<sub>2</sub> was numerically dissolved stepwise into the brackish formation water of ionic strength 0.063 (Table 5.2) at 25°C. Figure 5.1, curve "a" (Figure 11.5.1a - note that Figures identified by the prefix '11' are found in Appendix 11.) shows the rise in CO<sub>2</sub> pressure as increments of CO<sub>2</sub> are added. The amount of CO<sub>2</sub> added is directly proportional to the progress variable, 'XI', as shown on Figure 11.5.1a. A CO<sub>2</sub> pressure of 15 MPa was reached after 4 moles of CO<sub>2</sub> had been added to each 1000 grams of water (compare Figures 11.5.1a and 11.5.1b). The change in the distribution of species in the formation water is plotted in Figure 11.5.1c. Bicarbonate ion is the dominant carbonate species in the formation water initially. As CO<sub>2</sub> is added, H<sub>2</sub>CO<sub>3</sub> becomes dominant while the pH decreases; bicarbonate ion concentration remains nearly constant.

For the brine formation water (ionic strength 4.00), the total CO<sub>2</sub> added to reach a CO<sub>2</sub> pressure of 15 MPa is approximately 2 moles per 1000 grams of water (Figure 11.5.2); about one half the amount added to the brackish formation water. This *salting out effect*

is due to the increasing importance of hydration with salt content. As the ionic strength of the formation water increases to that of a brine, the activity coefficient of  $\text{H}_2\text{CO}_3$  increases from 1 to 2. Obviously to maximize  $\text{CO}_2$  solubility, dilute formation waters are favoured.

## 5.5 $\text{CO}_2$ SOLUBILITY IN CARBONATE AQUIFERS

If carbon dioxide is dissolved in a fluid in equilibrium with a carbonate formation (the formation mineralogy comprises calcite and/or dolomite, possibly with minor amounts of quartz present), the total amount of  $\text{CO}_2$  dissolved into the fluid is greater than the previous case, but no new minerals are precipitated. In fact, the formation carbonate minerals dissolve into the fluid and partially neutralize the acid created by the addition of the carbon dioxide. The dominant reaction can be written as:



Two aquifers were chosen to model this reaction: a pure dolomite-calcite aquifer and a dolomite-calcite-quartz aquifer. Both were reacted with the brackish formation water (Table 5.2). The pure dolomite-calcite aquifer is considered in Figure 5.2 (or Figure 11.5.3). The curves are almost identical to those of the pure formation water example (compare Figure 5.2a to Figure 5.1, curve "a") because only small amounts of calcite and dolomite have dissolved by the time equilibrium is reached (0.004 moles of dolomite and 0.05 moles of calcite; see Figure 5.2c (or Figure 11.5.3b2) and Table 5.2). This causes the concentration of bicarbonate ion to increase substantially (Figure 5.2b (or Figure 11.5.3c)) which results in an increase of approximately 1.5% or 0.06 moles of  $\text{CO}_2$  gas dissolved (Figure 5.2d) compared to the pure formation water case. The amount of additional  $\text{CO}_2$  which can be added to a calcite-dolomite-quartz aquifer is identical. The quartz dissolves to saturation. Its solubility is unaffected by the addition of the  $\text{CO}_2$  (Figure 11.5.4). No new phases are formed and the amounts of calcite and dolomite dissolved are identical.

In the case of a calcium-rich brine (see Figure 11.5.5), the same conclusions hold except the amount of CO<sub>2</sub> and calcite dissolved is less. Consequently, depending upon the specific formation water chemistry, reaction of a carbonate formation can result in an increase of dissolved carbon dioxide by 1 to 4 percent.

The formation waters in carbonate aquifers may be dilute or concentrated, but generally they are dominated by sodium and chloride. The calcium and magnesium concentrations can be quite low (particularly if the pH of the formation water is basic) as they are controlled by the solubility of the carbonate minerals. Dissolution of calcite or dolomite will increase the calcium and magnesium concentration in the water. This increase will be offset by the buffering effect provided by the cation exchange equilibria with the clays. This effect is most pronounced for low ionic strength formation waters.

Clays have a large exchange capacity and can have an important effect on water composition. The cation exchange capacity (i.e. CEC) are largest for the smectite group, which have a range of 100 to 140 milli-equivalents per 100 grams of smectite. The average CEC's for illites is 20 to 40 milli-equivalents per 100 grams and for kaolinites is 10 milliequivalents per 100 grams. For a rock containing 10% clay which is composed of equal amounts of smectite and illite, the CEC would be approximately 6 to 9 meq per 100 grams of rock. If the carbonate formation contains 5 wt% clay (1000 grams of clay per litre of water) which is comprised of equal amounts of illite and smectite, then the CEC would be 800 meq per litre of water. In this formation, a calcite-saturated brine passing over a Na-exchanged clay, would exchange Ca for Na by a reaction similar to:

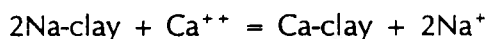


TABLE 5.2a STARTING MINERALOGY FOR PATH.UBC MODEL RUNS

Run =	Dilute	Brine	Cc Dol	Cc Dol	CC Dol	Cc Dol	Cc Dol	Anorth	Anorth	Anorth	Anorth	Anorth	Chlorite	Albite	Kspar	Amount
Brackish	✓		✓	✓		✓		✓					✓	✓	✓	
Brine		✓			✓		✓	✓	✓	✓	✓					
Calcite			100/ Equil	100/ Equil	1/ Equil	100/ Equil	1/ Equil				1/ Equil					grams rate
Dolomite			100/ Equil	100/ Equil	1/ Equil	100/ Equil	1/ Equil			1/ Equil	1/ Equil	1/ Equil				grams rate
Na <sub>2</sub> X						1/ Equil	1/ Equil									moles rate
Quartz			100/ Equil					1000/ Equil	1000/ Equil	1000/ Equil	50/ Equil	50/ Equil	1000/ Equil	1000/ Equil	1000/ Equil	grams rate
Anorthite								1000/ 100	1000/ 100	1000/ 100	1000/ 1	90/ 1				grams rate
Ca Smectite											1000/ 1	110/ 1				grams rate
Kspar															1000/ Equil	grams rate
Illite/ Muscovite								1000 Equil			500/ Equil	5/ Equil		1000/ Equil	1000/ Equil	grams rate
Albite														1000/ 1000		grams rate
Clinochlore													1000/ 1000			grams rate

TABLE 5.2B WATER CHEMISTRY FOR PATH.UBC MODEL RUNS

Run =	Dilute	Brine	Cc Dol	Cc Dol	CC Dol	Cc Dol	Cc Dol	Anorth	Anorth	Anorth	Anorth	Anorth	Chlorite	Albite	Kspar	Compositlon
IS	0.063/ 0.068	4.00/ 4.12	0.063/ 0.248	0.063/ 0.248	6.57/ 6.74	0.069/ 0.295	6.59/ 6.77	0.063/ 0.263	3.74/ 4.03	4.19/ 4.75	3.47/ 4.16	3.47/ 3.32	0.063/ 0.24	0.063/ 4.41	0.063/ 0.74	Start End
Na	1420/ 1207	746/ 70362	1420/ 1208	1420/ 1208	285/ 27266	1405/ 4024	27938/ 26777	1420/ 1324	37904/ 40549	38197/ 45275	29640/ 33780	29640/ 28196	1420/ 1270	1420/ 68977	1421/ 1237	ppm, Start ppm, End
K	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	13/ 2.44	1052/ 1892	3/ 3	954*/ 6234	954*/ 1579	0.0/ 0.0	13/ 35	28/ 20266	ppm, Start ppm, End
Mg	0.2/ 0.2	0.3/ 0.3	0.3/ 83.	0.3/ 83.	1779/ 1713	0.3/ 30	1763/ 1701	0.3/ 0.0	3594/ 590	398/ 379	3461*/ 718	3461*/ 622	0.3/ 1333	0.3/ 0.1	0.3/ 0.2	ppm, Start ppm, End
Ca	5.5/ 4.8	9.4/ 8.9	5.5/ *1772	5.5/ 1772	49358/ 47613	5.6/ 642	48911/ 47271	5.5/ 1253	13667/ 15826	23447/ 22576	16608* 19333	16608* 16452	3.5/ 0.0	5.5/ 1.3	5.5/ 4.5	ppm, Start ppm, End
pH	8.23/ 3.55	8.23/ 3.67	8.23/ 4.68	8.23/ 4.68	5.60/ 4.01	8.23/ 4.90	5.60/ 4.01	8.23/ 4.75	4.60/ 4.29	5.60/ 4.01	6.70/ 4.24	6.70/ 4.28	8.23/ 5.16	8.23/ 6.29	8.23/ 5.37	ppm, Start ppm, End
Cl	1868/ 1588	114645/ 108250	1868/ 1587	1868/ 1588	136322/ 130793	1439/ 1224	134742/ 129408	1880/ 1824	93789/ 92754	102529/ 111911	85565/ 92613	85565/ 74081	1867/ 1648	1880/ 1402	1895/ 1580	ppm, Start ppm, End
SO <sub>4</sub>	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	649* 456	649* 576	0.0/ 0.0	0.0/ 0.0	0.0/ 0.0	ppm, Start ppm, End
HCO <sub>3</sub>	555/ 500	455/ 479	555/ 6289	555/ 6287	24/ 839	548/ 10507	24/ 819	555/ 7536	481/ 2096	8.5/ 281	4.5/ 1872	4.5/ 2285	555/ 7229	555/ 180547	555/ 32207	ppm, Start ppm, End
CO <sub>2</sub>	9.3x10 <sup>-5</sup> 4.32	4.1x10 <sup>-5</sup> 1.71	9.3x10 <sup>-5</sup> 4.13	9.3x10 <sup>-5</sup> 4.13	8.5x10 <sup>-4</sup> 1.22	9.3x10 <sup>-5</sup> 4.04	8.5x10 <sup>-4</sup> 1.21	9.3x10 <sup>-5</sup> 4.11	0.185 1.78	4.7x10 <sup>-4</sup> 0.64	1.4x10 <sup>-5</sup> 1.74	1.4x10 <sup>-5</sup> 2.05	9.3x10 <sup>-5</sup> 1.33	9.3x10 <sup>-5</sup> 1.64	9.3x10 <sup>-5</sup> 3.62	molality, Start molality, End
H <sub>2</sub> O	51.49	53.85	51.61	51.61	54.30	51.65	54.31	44.84	47.12	47.77	43.12	52.61	57.66	50.79	51.52	molality, End
a CO <sub>2</sub>	4.41	3.98	4.41	4.41	4.01	4.36	3.98	4.39	4.08	1.45	4.10	4.18	1.41	4.01	4.34	activity, End
Cc Dol	0/ 0	0/ 0	-0.05/ -0.004	-0.05/ -0.004	-0.0081/ -0.00035	-0.09/ -0.006	-0.0081/ -0.0035	3.56/ 0.00	3.31/ 0.14	3.59/ 0.06	3.83/ 0.14	0.10/ 0.14	0/ 8.9**	0/ 0	0/ 0	moles ppt., End moles ppt., End

\* SO<sub>4</sub> complexes not included

\*\* refers to magnesite

Figure 5.1

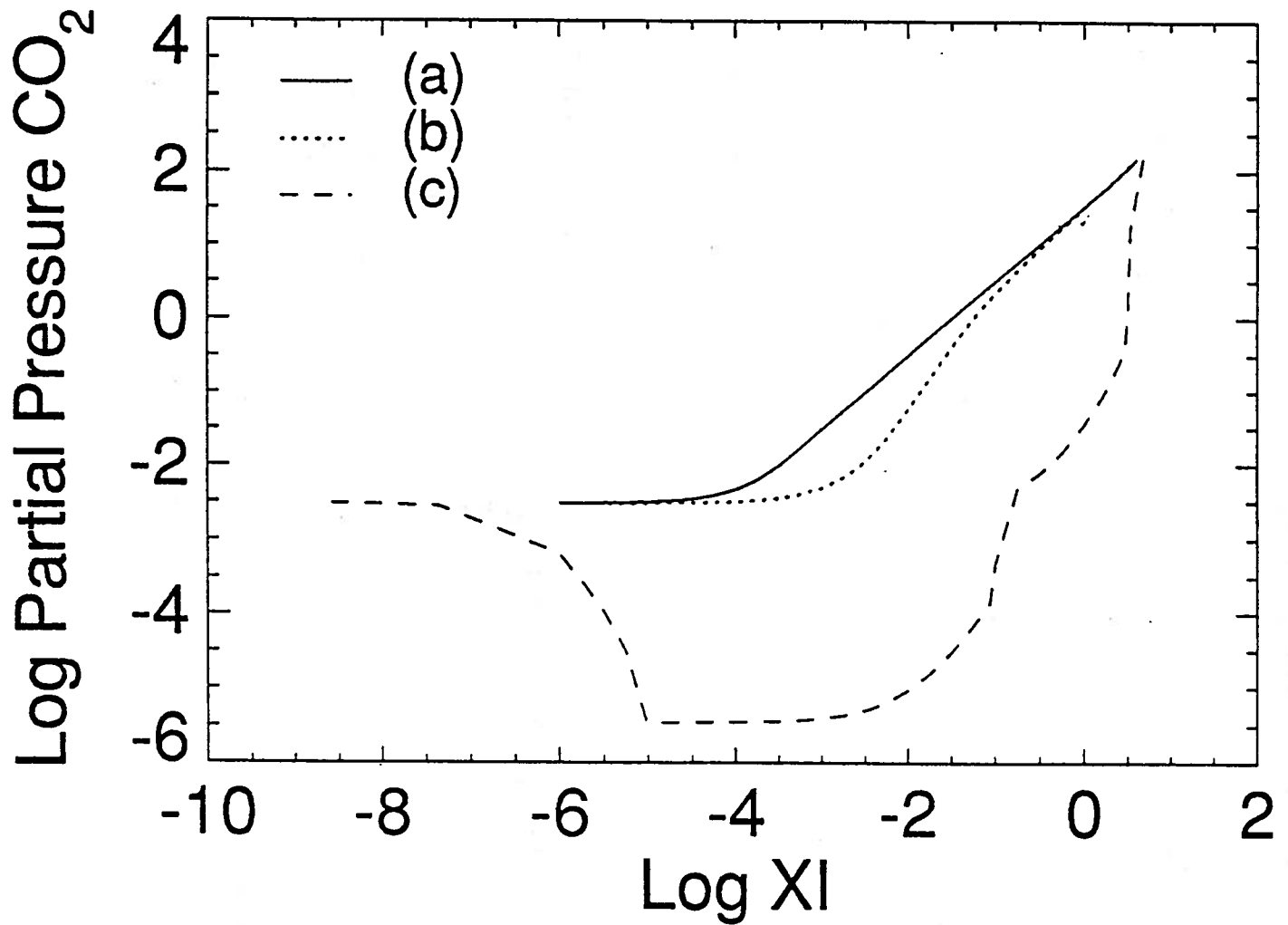


Fig. 5.1: Buildup of the partial pressure of CO<sub>2</sub> in bars as a function of time ('XI'): (a) in brackish formation water; (b) in brackish formation water in a calcite-dolomite aquifer with ion exchange; (c) in brackish formation water in an albitic (i.e. Na-rich) siliciclastic aquifer.

Figure 5.2

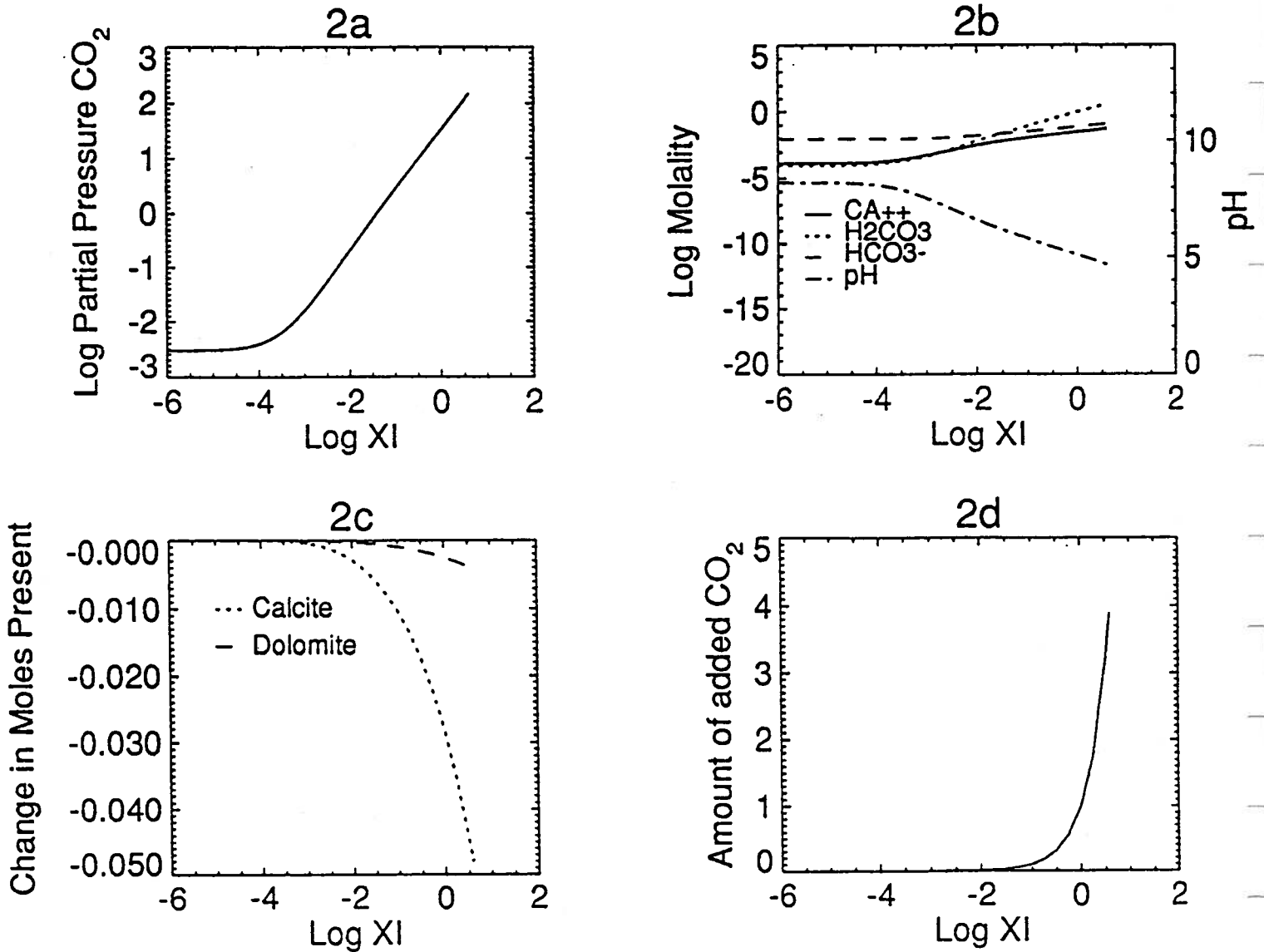


Fig. 5.2: Reaction of brackish formation water with a calcite-dolomite carbonate aquifer as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('XI'): (a) buildup of the partial pressure of CO<sub>2</sub> in bars; (b) change in the molality of the aqueous species; (c) change in the moles of mineral reactants; (d) molar amount of CO<sub>2</sub> injected into the aquifer.



thus decreasing the amount of calcium in the formation water. Consequently, the amount of carbon dioxide dissolved in the formation water due to carbonate mineral dissolution could be substantially increased because the calcium concentration is buffered through absorption onto exposed clay surfaces. This may occur as a marly section of the carbonate aquifer is broached and new formation fluids pass through it.

To quantify this effect, modelling of formation waters, equilibrated with a carbonate aquifer at 15 MPa CO<sub>2</sub> pressure, was completed as discussed above. The computer code, SOLMINEQ.88 (Kharaka et al., 1988), was used for the modelling. Initially, the composition of the clay exchanger was calculated based upon equilibrium with the formation waters before any CO<sub>2</sub> is added. Then the formation water was equilibrated with 15 MPa CO<sub>2</sub> in the absence of exchanger. Finally the formation water was re-equilibrated with clay exchanger at 15 MPa CO<sub>2</sub>. For the dilute formation water, the calcium concentration changed from 5 to 1772 mg/L as the CO<sub>2</sub> was added while maintaining calcite saturation. The calcium level dropped to 158 mg/L once the exchanger was equilibrated at the 15 MPa CO<sub>2</sub> pressure and calcite became undersaturated by an order of magnitude.

Figure 11.5.6 documents the reaction path for a similar case calculated using PATH.ubc. This calculation maintains equilibrium between exchange sites on the surface of the clay, calcite, dolomite and solution at all times during CO<sub>2</sub> addition. The increase of calcium and magnesium on the exchanger is clearly seen as the calcite and dolomite dissolve into the aqueous phase. When equilibrium between the exchanger, the carbonate minerals and formation water is satisfied at 15 MPa of CO<sub>2</sub> pressure, the amount of excess CO<sub>2</sub> dissolved in the formation water attributed to the combined effects of ion exchange and carbonate mineral dissolution is doubled. This is shown by the depression of the CO<sub>2</sub>-'XI' curve (curve b, Figure 5.1) For a calcium-rich brine, no increased dissolution of the carbonate minerals was observed (Figure 11.5.7) compared to the same reaction in the absence of

exchange sites on clay surface. Thus no excess capacity for CO<sub>2</sub> is generated by the presence of clay exchange sites in a calcium-rich brine.

## 5.6 CO<sub>2</sub> SOLUBILITY IN SILICICLASTIC AQUIFERS

Siliciclastic aquifers containing basic silicate minerals, can absorb more CO<sub>2</sub> (see Gunter and Bird, 1988, for an explanation) than other aquifers through a complex set of water-rock reactions. These reactions can be summarized in a general sense by the reaction of feldspar and clay silicate minerals with CO<sub>2</sub>:



The reactant clays comprise of both illites and smectites. The final ratio and the respective amounts of the calcite to dolomite depend on the initial formation mineralogy and formation water composition. The more feldspars and clays initially present, the more carbonate minerals produced as reaction products and the more carbon dioxide trapped in the formation.

Aquifers meeting these qualifications can be divided into two types: those in which the dominant basic silicate minerals are calcium and magnesium-rich and those in which they are sodium and potassium-rich. The first will absorb the most CO<sub>2</sub> because the silicate breakdown will release calcium and magnesium which combine with the injected CO<sub>2</sub> to form calcite and dolomite. The absorption of CO<sub>2</sub> for the second type is less. The breakdown of the basic silicates neutralizes the dissolving CO<sub>2</sub> and forms bicarbonate ions in the fluid. The potassium and sodium concentrations (released when the basic silicates breakdown) build up in solution, because the solubilities of potassium and sodium carbonates are much higher than those of calcite and dolomite. Consequently the ionic strength of the brine will build up until the partial pressure of CO<sub>2</sub> in the fluid is 15 MPa and the fluid is in equilibrium with the formation minerals that remain. It is appealing to

speculate that a set of conditions exist under which saturation with one of the alkali carbonates is reached, similar to the formation of the sodium carbonate-rich lakes at the earth's surface. These conditions have not been identified for CO<sub>2</sub> injection into Alberta aquifers.

The reaction paths followed by the formation fluid when CO<sub>2</sub> is injected into a siliciclastic reservoir can be followed on phase diagrams; diagrams which plot the relative stability fields of minerals as functions of the activities or activity ratios of various species in the formation fluid. Figures 11.5.8a, b, c, d represent the systems K<sup>+</sup>/H<sup>+</sup> versus H<sub>4</sub>SiO<sub>4</sub>, Na<sup>+</sup>/H<sup>+</sup> vs H<sub>4</sub>SiO<sub>4</sub>, Ca<sup>++</sup>/(H<sup>+</sup>)<sup>2</sup> vs H<sub>4</sub>SiO<sub>4</sub> and Mg<sup>++</sup>/(H<sup>+</sup>)<sup>2</sup> versus H<sub>4</sub>SiO<sub>4</sub>, respectively, and were calculated using the geochemical computer program, GeoCalc. The basic silicate mineral stability fields occupy the areas of these phase diagrams where the cation over hydrogen ion ratio is high. On the first three figures, this area is represented by a feldspar mineral (potassium feldspar, albite or anorthite) or zeolite (anorthite would occupy the laumontite field); on the fourth, this area is represented by the chlorite mineral, clinocllore. All of these diagrams were calculated assuming that all minerals were in equilibrium with water.

The diagrams do not take into account the effects of solid solution on the size of each of the mineral stability fields, even though the end-member feldspars, zeolites and clays generally do form solid solutions with the other end members in the same mineral group. The reason for this assumption is simplicity; the thermodynamic data for solid solution minerals is non-existent or poor, and the numerical methods for calculating dynamic equilibrium for solid solution minerals are intractable.

Generally, we have chosen to take a simple approach to modelling the effect of the four end member basic silicates on CO<sub>2</sub> uptake. We have represented the aquifer solids as a three phase mixture; excess quartz (representing the dominant phase in the aquifer solids)

and 1000 grams (i.e. 5 wt%) of each of the basic end member silicate and clay mineral illite (note that we used muscovite as a proxy for illite in the modelling).

To model the effects of CO<sub>2</sub> addition to a formation mineralogy rich in calcium, the three-phase assemblage, anorthite, muscovite and quartz, in dilute or brackish formation water was allowed to react with CO<sub>2</sub> (Table 5.2). The calculated reaction paths are complex with anorthite and quartz initially reacting to form laumontite (Figures 5.3c, d (or Figure 11.5.9b)). Illite is stable and little reaction occurs. Once all the anorthite has reacted, the laumontite then breaks down to form kaolinite, calcite and quartz. The reaction progress can be followed by monitoring the change in the aquifer water chemistry (Figure 5.3b) or the partial pressure of CO<sub>2</sub> in Figure 5.3a (or Figure 11.5.9a). The first part of the curve is similar to that for no water-rock reaction; flat. However instead of a steep rise, the CO<sub>2</sub> sharply drops to a flat minimum as first the pH is buffered to more basic conditions and then as calcite precipitates. Each plateau in the minimum of the CO<sub>2</sub> curve marks the loss or precipitation of a new phase. The CO<sub>2</sub> pressure starts to rise sharply to the final imposed pressure only after all the laumontite has reacted. There is no source of calcium left to form calcite, thus allowing the level of carbonate (dissolved CO<sub>2</sub>) in solution to increase rapidly. In addition, a small amount of calcite will dissolve as the CO<sub>2</sub> pressure builds up to 15 MPa (Figure 5.3d). Approximately four moles of CO<sub>2</sub> have precipitated as calcite. The amount of CO<sub>2</sub> locked up in the aquifer has doubled when compared to the non-reactive or to the carbonate aquifer cases. If the mass of available anorthite had been increased, more CO<sub>2</sub> could have been trapped by the continued precipitation of calcite.

The reactions between a formation brine, an anorthite-rich formation, and injected CO<sub>2</sub> are different from the brackish formation water case because of the more concentrated constituents of the brine. For this modelling run, only quartz and anorthite were used to represent the formation mineralogy as illite was essentially inert (Table 5.2). The initial pressure of CO<sub>2</sub> in the brine is much higher because of the different formation fluid composition but the shape of the pressure curve (Figure 11.5.10a) is similar; it has a deep

minimum followed by a vertical rise to the final CO<sub>2</sub> pressure of 15 Mpa. The observed reactions are different because of the higher sodium concentrations and buffering effects of the brine. Na-smectite is stabilized over laumontite. Prehnite forms as an intermediate calcium phase. Both the prehnite and Na-smectite break down to form calcite and kaolinite. The final equilibrium mineral assemblage (calcite, quartz and kaolinite) is similar to the dilute formation water case; only the intermediate steps of the reaction path are different. The total amount (approximately 4 moles) of calcite formed is similar to the brackish formation water case, but the total CO<sub>2</sub> consumed is less; only approximately 5 moles. This is largely due to the limited solubility of CO<sub>2</sub> in brines; the salting out effect.

The effect of temperature on CO<sub>2</sub> injection into a calcium-dominated basic formation mineralogy was investigated at 100°C. As shown by Figure 11.5.11, similar reactions occur. Anorthite is replaced by prehnite which in turn breaks down to kaolinite. Sodium smectite also appears briefly. Although the solubilities of these minerals change significantly with the higher temperature, the same reaction drive dominates; the conversion of basic aluminous silicate minerals to kaolinite by acidic CO<sub>2</sub>. The resulting reaction path is very similar to the 25°C case. Approximately 4 moles of calcite is precipitated. The total mass of CO<sub>2</sub> consumed is less than the 25°C case because the solubility of CO<sub>2</sub> in a brine is lower at higher temperatures.

If CO<sub>2</sub> reacting with a brine and a more complex calcium mineral assemblage involving intermediate and basic minerals is modeled at 25°C, the reaction path will be considerably more complex but the final results will be similar to the previous cases. For example, by adding 1000 grams of Ca-smectite to the anorthite-muscovite-quartz assemblage, the shape of the CO<sub>2</sub> pressure curve (Figure 11.5.12a) changes slightly. The first part of the curve is similar; flat. Then the pressure starts to rise and then drops as the silicate-water reactions start to dominate. Both anorthite and Ca-smectite break down to form sodium smectite, calcite and kaolinite. Trace amounts of dolomite and anhydrite are also made. Illite is essentially inert. In the final stages of the reaction, Na-smectite also breaks down to form

kaolinite. Four moles of calcite are formed, similar to the two cases above. Only 6 moles of CO<sub>2</sub> were consumed due to the salting out effect.

If the amounts of the accessory minerals are decreased by an order of magnitude (i.e. to 100 grams of anorthite and smectite), the shape of the CO<sub>2</sub> pressure curve is similar (Figure 11.5.13a) to the previous calculations. The minimum is not as deep nor as wide because there are fewer basic silicate minerals (anorthite) available for reactions. However, the observed reactions are very similar to the previous calculations. At equilibrium, 0.2 moles of calcite has been made; and the brine formation water, not the solids, has trapped the majority of the CO<sub>2</sub>. This emphasizes the earlier results **that the actual amount of CO<sub>2</sub> locked up by precipitation of carbonate minerals is limited only by the amount of basic calcium silicate mineral present in the aquifer solid assemblage.** Once again, the salting out effect has limited the solubility of CO<sub>2</sub> to two moles in the brine instead of the four dissolved in brackish water. We expect the major effect of the brine will be the same in all other cases. Therefore, the modelling of magnesium, sodium and potassium silicate systems will be continued only using the dilute formation water.

The magnesium-rich siliciclastic aquifers behave similarly to the calcium-rich ones. In Figure 11.5.14, the reaction path for 5 wt % clinocllore with excess quartz is shown. The pressure of CO<sub>2</sub> remains low until the end where it rises almost vertically. The initial magnesium formation mineral, clinocllore, reacts to form talc and kaolinite. Once clinocllore has reacted out, the talc in turn breaks down to form magnesite, the magnesium analogue to calcite. The final assemblage is quartz, magnesite and kaolinite. Over 9 moles of magnesite had formed, at which time the model became unstable. The final CO<sub>2</sub> pressure reached was only 5 MPa with only 1.4 moles of CO<sub>2</sub> dissolved in the water. The magnesium reactions appear more promising as a CO<sub>2</sub> sink than their calcium counterparts.

Figure 5-3

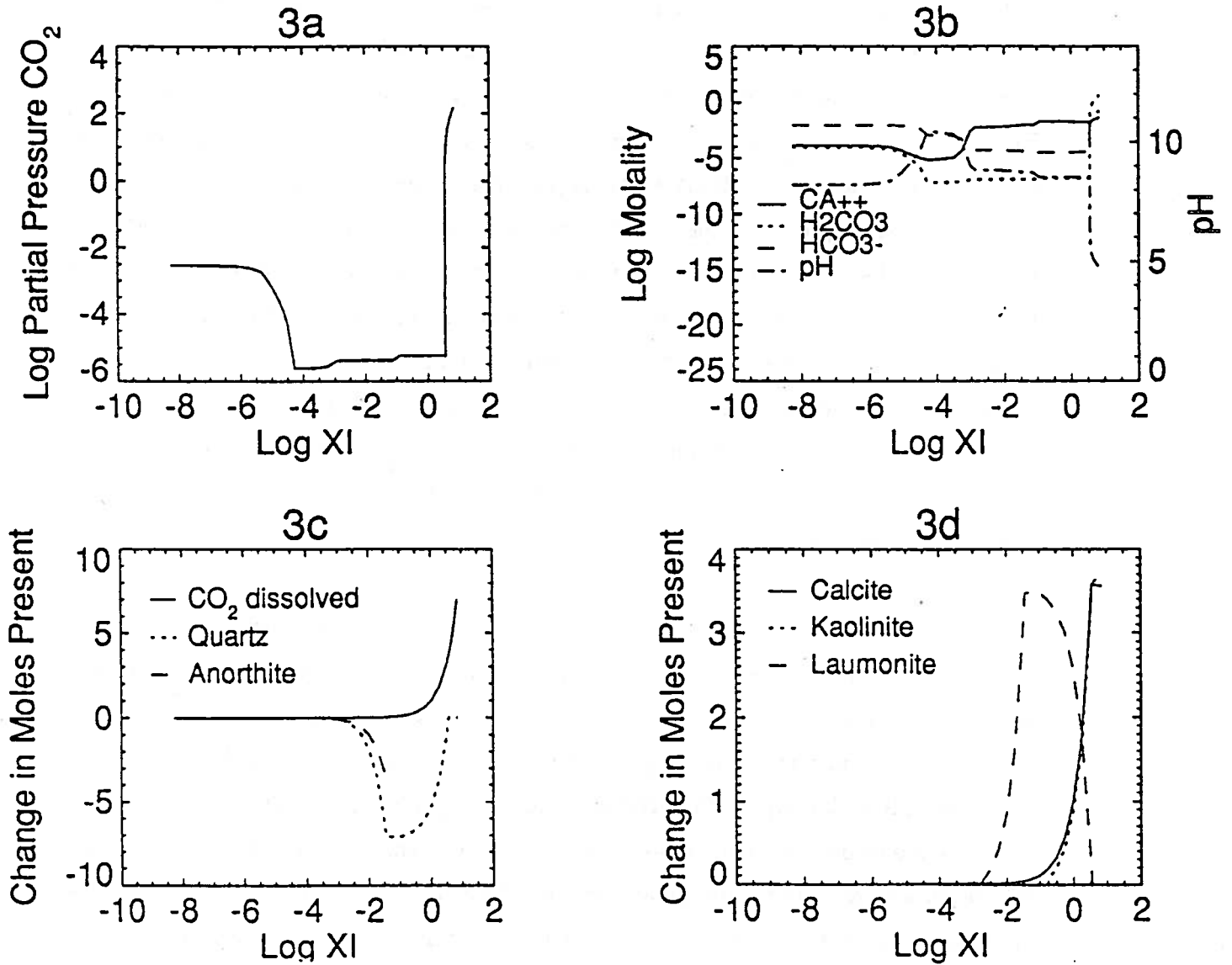


Fig. 5.3: Reaction of brackish formation water with an anorthite-muscovite-quartz siliciclastic aquifer as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('XI'): (a) buildup of the partial pressure of CO<sub>2</sub> in bars; (b) change in the molality of the aqueous species; (c) change in the moles of the initial formation mineralogy and the amount of CO<sub>2</sub> injected into the aquifer; (d) change in the moles of mineral products.

The sodium-rich siliciclastic aquifers were modelled as a mixture of 5 wt% of albite and illite in the presence of excess quartz. As was observed in previous simulations, the illite behaved inertly. The albite reacts to form jadeite which in turn breaks down to form sodium smectite. The final equilibrium assemblage is illite, quartz and sodium smectite. The kaolinite stability field was never reached because the large sodium build up in the formation fluid stabilized smectite. The CO<sub>2</sub> pressure curve (Figure 5.1, Curve "c" (or Figure 11.5.15a)) rises from the minimum much earlier than for the Ca- or Mg- cases (Figure 5.3a) because no carbonate phases precipitate. Final CO<sub>2</sub> take-up is 5 moles, of which 4.4 moles is present in the form of bicarbonate ion and 1.6 moles as dissolved CO<sub>2</sub>. Even though the initial formation water was a brackish formation water (Table 5.2), the build-up of the bicarbonate ion increases the ionic strength from 0.063 to 4.41. This results in a significant salting out effect for the dissolved CO<sub>2</sub>. The observed concentration of bicarbonate is more than an order of magnitude higher than calculated for the calcium- or magnesium-rich siliciclastic aquifers. As discussed earlier, the build-up of bicarbonate cannot occur for the calcium or magnesium cases because of early saturation with calcite, magnesite and/or dolomite.

The effects of CO<sub>2</sub> addition to a dilute formation water in a potassium-rich siliciclastic reservoir were modelled using a formation composed of 5 wt% of each potassium feldspar and illite, in the presence of excess quartz. Under these conditions, the potassium feldspar reacted to form muscovite and quartz, both of which remained in equilibrium with the fluid during the addition of CO<sub>2</sub>. The pressure of CO<sub>2</sub> climbed steadily (Figure 11.5.16a) similar to the carbonate aquifer case (Figure 5.1, curve b) and was not affected significantly by the mineral reactions. The potassium subsystem is by far the least reactive of all the siliciclastic systems considered under high CO<sub>2</sub> pressures; the final bicarbonate ion concentration reaches only 0.6 molal. Although this is considerably higher than its calcium and magnesium counterparts, it is only a fraction of the concentrations reached by the sodium analogue case. Consequently, siliciclastic aquifers dominated by potassium



accessory phases would not enhance the  $\text{CO}_2$  uptake significantly above the 4 moles dissolved in the inert (mineral absent) aquifer case.

## 6.0 VALIDATION OF GEOCHEMICAL MODELLING

### 6.1 EXPERIMENTAL DESIGN

Autoclave experiments were designed to confirm the results of these geochemical modelling predictions. A synthetic brackish formation water was prepared according to the following recipe: 0.05261 M sodium chloride, 0.000335 M potassium chloride, 0.000138 M calcium chloride, 0.0000116 M magnesium chloride, 0.009134 M sodium bicarbonate and 0.000139 M sodium carbonate. Drill core from a siliciclastic aquifer (6-18-50-3W5, 1555.65m) was ground to a fine powder. Relatively pure mineral specimens from Ward's Natural Science Ltd. were also ground to a fine powder. The powdered drill core and mineral powders were characterized by XRD and SEM. Mixtures of 10 grams of the powdered drill core with:

- a) 30 grams of powdered albite (Na-feldspar); experiment 411,
- b) 20 grams of powdered clinocllore (Mg-chlorite); experiment 414,
- c) 30 grams of powdered microcline (K-feldspar); experiment 410,
- d) 30 grams of powdered labradorite (Ca-feldspar); experiment 412, and
- e) a control, the siliciclastic aquifer by itself; experiment 437

are placed into 300 ml autoclaves and sealed. Each autoclave had two ports in the head at the top to facilitate aqueous sampling. One port was affixed with a dip tube which extended to within 1.5 cm of the bottom of the autoclave, and the other with a 2 cm diameter sintered stainless steel filter, with a nominal pore size of 0.5 microns. Approximately 1.2 moles (53 g) of carbon dioxide were transferred into each sealed autoclave quantitatively. Finally the autoclaves were filled with approximately 250 grams of the simulated brackish formation water. This was done by connecting them to a piston type hydraulic accumulator containing the water on one side of the piston, and nitrogen at approximately 88 bars on the other. The autoclaves were thereby pressurized

hydrostatically to about 88 bars. The pressure was monitored by means of a pressure transducer fixed on each autoclave. The autoclaves were weighed to ensure no loss of the contents. They were placed in an enclosure at room temperature (20°C). The contents of the autoclaves were constantly stirred by means of magnetic stir bars. Pressure in the autoclaves cycled with room temperature by plus or minus about 8 bars.

The autoclave contents were allowed to react for approximately four weeks. During this time, the pressures were constantly monitored. They were weighed at regular intervals to confirm no loss of the contents, and checked to ensure that stirring of the contents was maintained.

At the end of this time, the aqueous contents were sampled. A sample tube was pressurized to 88 bars (autoclave pressure) with nitrogen and connected at the top of the autoclave to the port with the filter element. At the outlet end of the sample tube, a back pressure regulator (BPR) was connected and set to maintain an 88 bar pressure. A heavy immiscible liquid (dichloro methane) was injected at 88 bars through the dip tube into the bottom of the autoclave, displacing the aqueous sample into the sample tube. At the same time, the nitrogen was displaced from the sample tube through the BPR to the atmosphere. After the contents of the sample tube were flushed about three times, the sample tube was isolated by closing valves at either end. Injection of the dichloro methane continued through a by-pass line, along side the sample tube, and through the BPR. This was done until all of the water and carbon dioxide were displaced from the autoclave. The replacement of the water, under pressure, ensured that no minerals precipitated as a result of the de-gassing that occurs as a result of depressurization at the end of the experiment.

The CO<sub>2</sub> was collected quantitatively from the sample tube by slowly depressurizing into a Brooks Gas Meter. The remaining aqueous sample was analyzed for cations by ICP, and alkalinity, chloride and sulphate by IC. The autoclave, with dichloro methane at 88 bars,

was depressurized and opened. The powder was removed, dried, and analyzed by XRD and SEM to determine the extent of reaction.

## 6.2 PRODUCT EXAMINATION

The X-Ray charts for each of the autoclave experiments are shown in appendix 11.6.2. Three charts are presented for each experiment, the first shows the entire X-Ray scan, while the second and third charts provide the 2-Theta measurement and D-spacings for each peak in the range of 2 to 34 degrees 2-Theta and 34 to 66 degrees 2-Theta, respectively.

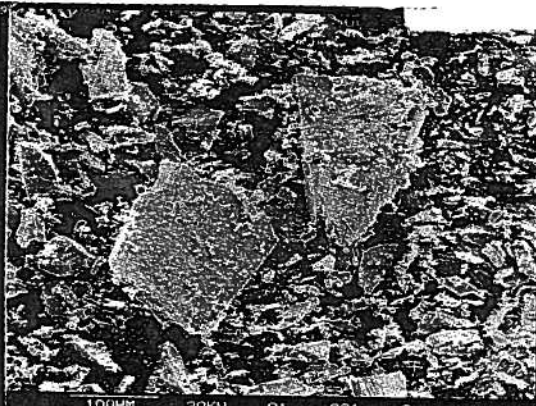
The observed changes to the mineralogy in the autoclaves, as determined by X-Ray diffraction, are small. The largest change was less than 5 weight percent of the sample. A new phase (peak at 4.91 angstroms) formed in Run 437 (the control) but could not be identified as only one x-ray peak was clear. Approximately 2-3% of illite was formed in Run 410 (microcline addition to the control). The presence of illite is consistent with the modelling, which used muscovite as a proxy for illite. Two new peaks have been observed in Run 411 (albite addition to the control), one tentatively can be identified as kaolinite while the other is probably an amphibole. An approximate total of 3 weight percent (of both) were formed. Two new peaks were observed in Run 412 (labradorite added to the control), one is kaolinite while the other could not be identified. The masses of the two total to approximately 3%. The formation of kaolinite is consistent with calcium siliciclastic modelling runs. No new peaks, hence no new phases, were observed in Run 414. The presence of new carbonate minerals could not be identified in any of the charts. As some carbonate phases were present in the siliciclastic control, thus in all on the experiments, small changes in the weight percent present would not be possible to observe.

Figures 6.1A and 6.1B contain SEM photographs of the pre- and post run solids from the autoclave experiments. The magnification of the photos is 120 times. Each photo is

identified by the fourth number at the base of the photo. Photos one through seven examine the pre-run samples (photos #1 & #2 are from Run 411; #3 is from Run 412; #4 is from Run 410; #5 from Run 414; #6 and #7 are from Run 437). Of interest is the calcite rhomb visible in photo 7. All of the mineral grains have sharp angular edges and cleavage is visible on some of the larger grains. Photos eight through thirteen examine the run products (photo #8 is from Run 411; #9 & #10 are from Run 414; #11 is from run 410; #12 is from Run 412; #13 is from Run 437). No new minerals could be identified in any of the photos, however, evidence of quartz overgrowths can be clearly seen in photos #8, #9, #10, #11 and #13. For example on photo 13, the largest grain in the lower left corner is quartz and can be seen to have clearly defined crystal terminations. Quartz overgrowths were also identified in the post-run products from autoclave run 412 but can not be seen in photo #12. In every geochemical modelling simulation where silicate minerals were present, quartz was formed as a product mineral, even when it initially dissolved. Thus the presence of quartz overgrowths is consistent with the geochemical modelling.

Table 6.1 contains the analytical results for the composition of the initial water and for each of the waters in the autoclaves at the end of the experiments.

pH decreased in all the experiments, but most significantly for the control. pH is expected to decrease with increasing amounts of dissolved carbon dioxide, however it will be buffered by reactions with the silicate mineralogy (see discussion in the modelling section). The greater reactivity of the "spiked" samples (autoclave runs #410, #411, #412 and #414) has resulted in increased amounts of silicate mineral buffering, thus the pH has not shifted as much.



100PM 20KV 01 001 S



100PM 20KV 01 002 S



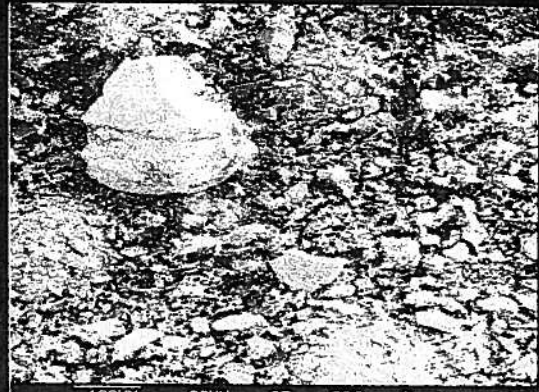
100PM 20KV 02 003 2



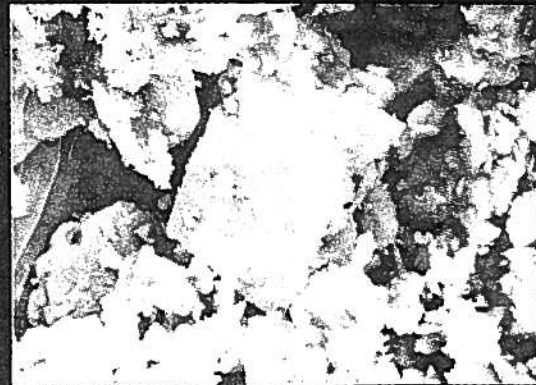
100PM 20KV 03 004 2



100PM 20KV 04 005 2



100PM 20KV 05 006 2

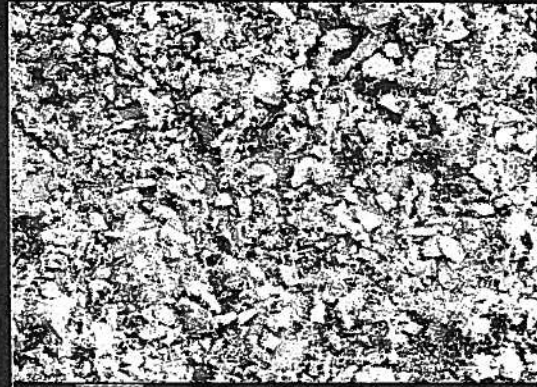
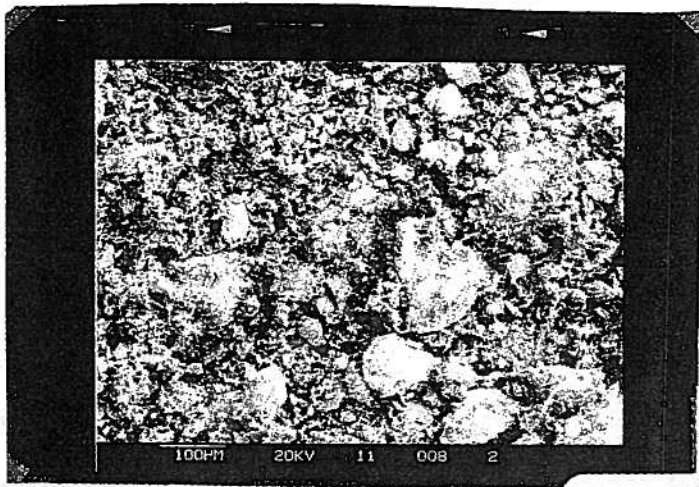


20PM 20KV 05 007 2

**Legend:**

- 001/002 - Run 411
- 003 - Run 412
- 004 - Run 410
- 005 - Run 414
- 006/007 - Run 437

PRE-RUN SAMPLES  
FIGURE 6-1A



**Legend:**

- 008 - Run 411
- 009/010 - Run 414
- 011 - Run 410
- 012 - Run 412
- 013 - Run 437

**POST-RUN PRODUCTS  
FIGURE 6-1B**

The alkalinity has increased for all of the runs, but most for the spiked runs because the silicate minerals buffered the pH. As discussed previously, this buffering allows the dissolution of slightly more carbon dioxide. The observed alkalinity values correspond to approximately 0.08 moles of total dissolved carbon dioxide, indicating that the experiments are still far from final equilibrium values.

The sodium levels vary around the initial pre-run value. Because of the relatively high concentration of sodium in the charge, these variations can not be assigned to a reaction and are probably the result of normal analytical error.

The calcium levels have increased in all of the runs. Only 0.3 grams of calcite would have to be present in the siliciclastic formation mineralogy and dissolve completely to raise the solution composition to the observed calcium levels of approximately 500 mg/l. Experiment #412 was spiked with Labradorite, a calcium-sodium feldspar, thus higher levels of calcium would be expected. This was not observed, thus precipitation of the calcium derived from the labradorite in another phase must have occurred. The X-ray charts contained evidence of a phase which could not be identified. Based upon the modelling and mass balances, it is probably that it was either a calcium zeolite or a calcium smectite.

Potassium levels increased slightly for all runs, except for the experiment spiked with Microcline (Run 410) which had its potassium levels increased by over 3 times compared to the other experiments. Microcline contains potassium, thus a larger increase would be expected unless the formation of illite buffers the potassium level. Illite was identified as a reaction product in both the modelling and the X-ray examinations. Its formation buffered the potassium levels to the observed levels.



Table 6-1

Aquifer Disposal of Carbon Dioxide Autoclave Experiments							
Analysis of Post Run Waters							
Concentration	Pre-Run	410	411	412	414	437	
mg/l							
Alkalinity (HCO <sub>3</sub> )	570	3360	3420	4180	3600	1520	
pH	7.25	6.49	6.48	6.56	6.49	6.16	
Chloride	1820	1480	1680	1790	1900	1805	
Sulfate	<2.5	6.9	8.2	8.3	7.9	8.8	
Phosphorus	0.68						
Sulfur	0.69	1.88	3.39	2.74	3.82	3.77	
Magnesium	0.74	5.84	10.72	7.13	150.8	2.54	
Silicon	0.35	40.42	54.53	56.39	43.16	6.06	
Sodium	1528	1458	1461	1471	1655	1505	
Aluminum	0	3.82	4.39	3.8	2.77	2.97	
Calcium	5.32	491.2	514.8	519.5	738	251	
Cadmium							
Cobalt	0	0.4	0.11	34.06	0.52	0.35	
Nickel	0.04	6.94	6.08	24.52	13.34	50.45	
Potassium	15.09	69.5	23.96	20.52	20.34	17.29	
Manganese	0.01	21.15	17.38	24.53	32.21	12.28	
Iron	0.05	586.7	580.4	950.5	219.2	61.62	
Chromium	0.01	4.64	3.1	2.02	1.12	3.89	

Magnesium concentrations increased slightly for all runs, except for the Clinocllore spiked experiment (Run #414) in which the shift was considerable. Clinocllore contains magnesium, thus the increase in magnesium is consistent with both the bulk mineralogy and the geochemical modelling.

Silicon concentrations increased for all autoclave runs. The concentrations in run #437, the control experiment, increased to a value which is in equilibrium with quartz. The concentrations in the other runs were significantly above quartz saturation values.

Aluminum concentrations increased in all samples due to dissolution of the silicate minerals.

The variation in chloride concentration is normal when IC (Ion chromatography) is used to measure higher chloride concentrations.

Sulphate and total sulphur concentrations are essentially the same for all samples and probably indicated that a small amount of gypsum (calcium sulphate) was present in the siliciclastic formation mineralogy. This gypsum dissolved and raised the amount of sulphur in the water.

The increase in iron, chromium, manganese, nickel and cobalt values are from the autoclave metal, and do not represent reactions between the fluid and the formation mineralogy or the minerals spikes.

The increase in all of the components clearly indicate that dissolution of the formation mineralogy and the mineral spike are taking place. Examination using SOLMINEQ.88 pc/shell, a geochemical program used to evaluate water compositions, indicates that all of the waters are slightly supersaturated with calcite, and all of the spiked runs are supersaturated with quartz. The calcite supersaturation is caused by the loss of a small

amount of carbon dioxide from the water before the water analysis is made. This shifts the pH to slightly more basic levels, resulting in an apparent calcite supersaturation. The supersaturation of quartz can only occur when the dissolution rate of the spiked phases (albite, clinocllore, labradorite and microcline) occurs more rapidly than the precipitation rate of quartz or other possible product minerals.

### 6.3 KINETICS

As expected, the rates of reaction at room temperature are slow. The rates at which Al-bearing silicates dissolve in the laboratory, under STP conditions, varies between  $1 \times 10^{-10}$  and  $1 \times 10^{-13}$  mol (Si)/m<sup>2</sup>/sec, depending upon the type of silicate (Kirkwood and Nesbitt, 1990, see Table 7). Of the minerals that consume acid upon dissolution, feldspars and biotites dissolve more rapidly than muscovitic micas and some chlorites. Dissolution rates of clay minerals such as smectites and illites generally have not been given the same detailed laboratory study as feldspars or micas, consequently, their laboratory dissolution rates generally are not well established. Field studies of weathering processes, however, indicate that the clay minerals generally are more reactive than feldspars or micas where contacted by waters undersaturated in the clay minerals. In fact, there is abundant evidence that the clay minerals control solution compositions in sedimentary basins such as the Illinois Basin (Nesbitt, 1980, 1985) and the Western Canada Basin (Hutcheon and Abercombie, 1992). These field studies suggest that reaction rates for dissolution of clay minerals are at the high end of the reaction rate spectrum (values quoted above for the other silicate minerals); consequently, reaction rates of the order of  $1 \times 10^{-9}$  to  $1 \times 10^{-10}$  mol(Si)/m<sup>2</sup>/sec for dissolution of the clay minerals such as smectites, vermiculites, septachlorites and illites are reasonable.

Field studies of catchments now being weathered indicates that bulk release rates of elements (from the catchments) are 1 to 3 orders of magnitude lower than predicted if dissolution alone were operative. (Cleaves *et al.*, 1985; Velbel, 1985; Kirkwood and

Nesbitt, 1990). These results have been interpreted to indicate that dissolution rates of silicate minerals are lower in nature than in the laboratory, the assumption being that the reactions taking place in the catchments are the same as occurred in the laboratory. The implication is that the laboratory dissolution rates are inapplicable to nature (Paces, 1983). An alternative, and equally or more likely explanation is that different reactions occur in the catchments than in the laboratory (Nesbitt and Young, 1984; Kirkwood and Nesbitt, 1990).

Clay minerals formation is common in catchments, thus element release is retarded by formation of secondary clay minerals at the expense of dissolution of feldspars and other silicate minerals. Furthermore, the effects of cation exchange reactions on release rates from the catchments generally have not been considered. Since the reactions controlling element release from catchments generally are not well studied, implied dissolution rates derived from catchment studies are suspect in the extreme. By contrast, laboratory dissolution rates are well documented and should be used in modelling. The reaction of acids with silicate minerals including feldspars, micas and clay minerals. If secondary minerals form during dissolution of these minerals, reaction rates of formation of secondary minerals should be included in the calculations, rather than using "quasi-reaction rates" derived from catchment studies.

It was thought that the high pressures of CO<sub>2</sub> used in our autoclave experiments (described above) might accelerate the reactions. On the contrary, the rates of reaction observed in this study are in line with those quoted above.

#### **6.4 VALIDATION**

The geochemical modelling predicted the changes which would occur as the system evolved towards and reached the final equilibrium between the minerals, carbon dioxide, water and the dissolved constituents. The experiments never reached final equilibrium; the

changes in solids were small and the total amount of dissolved carbon dioxide was small relative to the total amount. However, the few changes in mineralogy which occurred during the autoclave experiments are consistent with the geochemical modelling and the water chemistry. The quartz overgrowths observed by SEM, the formation of illite and kaolinite observed by X-ray and the changes in dissolved cation and anion concentrations observed are in agreement with the modelling. The X-ray data indicated that some new minerals were forming, but insufficient amounts were present to determine which phases they were.

Clearly the amount of time necessary for equilibrium to occur, or even sufficient reactions to occur, is greater than the elapsed experimental run time. However, the experiments did show conclusively that:

- The formation will react and dissolve into the formation water when excess carbon dioxide is introduced.
- The spiked experiments did dissolve more carbon dioxide than the formation did by itself. This agrees with the modelling which showed that reaction with complex silicate minerals controls the amount of carbon dioxide which can be dissolved.
- The autoclave experiments need much longer than four weeks to come to equilibrium. Similar or longer times would be expected during injection in the subsurface, thus little or no near well damage due to precipitation would occur.

The limited amount of reactions which did occur, agree with the initial portions of each of the geochemical modelling results which were presented earlier. Unfortunately the slow reaction kinetics at low temperatures preclude more detailed comparison.

## **7.0 CONCLUSIONS**

### **7.1 SYSTEM OVERVIEW**

Aquifer disposal of power plant CO<sub>2</sub> is dependent upon the nearby availability of suitable aquifers and the economics of CO<sub>2</sub> capture, compression and purification. Much optimizing is required to minimize capture and compression costs, but pipeline and well systems appear relatively straightforward with several environmental concerns, such as aquitard cementing, still to be addressed.

The costs of pipeline and well systems are but a small part of those of the overall CO<sub>2</sub> disposal system in this Alberta setting, and generally such systems will follow conventional oil and gas practices.

### **7.2 AQUIFER OVERVIEW**

Aquifer disposal of CO<sub>2</sub> in the region between the Genesee and Sundance power stations, west of Edmonton, Alberta, Canada, has been investigated by identifying potential aquifers. The depths of the selected disposal formations (Lower Mannville and Wabamun) are greater than 1400 metres and permit injection pressures of liquid CO<sub>2</sub> greater than 15 MPa. These aquifers are deep enough to be part of the regional flow systems, isolated from the surface by extensive regional aquitards, yet relatively shallow in order to minimize drilling costs.

### **7.3 NUMERICAL SIMULATION OF AQUIFER INJECTABILITY**

There is potential for subsurface disposal of liquid CO<sub>2</sub> both in the Wabamun carbonate aquifer and in the Lower Mannville siliciclastic aquifer in the Wabamun Lake area, Alberta. Our conclusions are based on the modelling of the Lower Mannville aquifer. By choosing a 4" radius injector and completing the entire thickness of the aquifer, an average CO<sub>2</sub>

injection rate of 180 t/day can be achieved over a period of 30 years. The CO<sub>2</sub> injection rate decreased as the completion interval of the injector decreased. There is very little effect on the CO<sub>2</sub> injection rate by choosing a 3" radius injector. Injecting CO<sub>2</sub> in the high-permeability region of the aquifer as the CO<sub>2</sub> injection rate increased 10 fold as the absolute permeability of the aquifer increased by an order of magnitude to over 1500 ton/day.

Injecting CO<sub>2</sub>-rich water is not a feasible alternative to injecting liquid CO<sub>2</sub>.

Although the Wabamun limestone was not modelled, a similar injectivity is expected.

#### **7.4 MODELLING OF CO<sub>2</sub> RESERVOIR REACTIONS**

Based upon formation water analyses from 754 wells within the area, two waters (a brine formation water and a brackish formation water) were selected to illustrate extremes for modelling purposes. Three general types of formation mineralogy were chosen; an inert or mineral-absent formation, a carbonate formation, and a siliciclastic formation. The mineralogy of the carbonate formation included the minerals calcite, dolomite and minor amounts of quartz, and represent a typical Devonian carbonate sequence (Wabamun Group) in the area of the Sundance and Genesee power plants. The modelling examined the effects of varying the amounts of these three minerals. The mineralogy of the siliciclastic formation was initially chosen to represent the Lower Mannville Group in the area, but was extended to allow examination of the effects of each of a calcium, magnesium, sodium and potassium aluminosilicate dominant formation mineralogy.

The modelling results indicate that brackish and dilute formation waters can take up more CO<sub>2</sub> than brine formation waters. Thus, brackish or dilute formation waters are favoured for CO<sub>2</sub> capture. The maximum solubility of CO<sub>2</sub> is limited in brines due to the salting-out effect at higher ionic strengths.

The reaction of the mineralogy and formation water for a carbonate aquifer with injected CO<sub>2</sub> does not significantly increase the CO<sub>2</sub> uptake. However, if the carbonate aquifer contains significant amounts of clays with a large cation exchange capacity, the CO<sub>2</sub> capture capacity will be significantly greater than a clay-absent carbonate aquifer.

**The maximum amount of CO<sub>2</sub> can be trapped in a siliciclastic aquifer containing a brackish formation water.** The amount of trapped CO<sub>2</sub> is dependent upon the amount of and type of basic minerals (feldspars and clays) present in the formation. Magnesium- and calcium-rich siliciclastic aquifers are favoured for neutralization and trapping of the injected CO<sub>2</sub> through the precipitation of calcite (calcium carbonate), dolomite (calcium magnesium carbonate) or magnesite (magnesium carbonate). The amount of captured CO<sub>2</sub> can be increased by neutralization and precipitation by more than a factor of two over solubility in a brackish formation water, depending upon the amount of available calcium and/or magnesium in the formation minerals and the pressure of CO<sub>2</sub>. Sodium-rich siliciclastic aquifers will absorb CO<sub>2</sub>, neutralizing it to form bicarbonate ions and thus converting the brackish chloride formation water to a bicarbonate brine. The increase in CO<sub>2</sub> solubility due to formation of bicarbonate is only partially balanced by the salting out effect due to the increased ionic strength. Thus a sodium-rich formation mineralogy may be favoured as a disposal site when the precipitation of carbonate minerals must be avoided. Potassium-rich siliciclastic aquifers equilibrate more rapidly than their sodium counterparts and only limited amounts of bicarbonate ion is formed. Thus CO<sub>2</sub> capture is not enhanced significantly for potassium-rich siliciclastic aquifers.

## 7.5 VALIDATION OF GEOCHEMICAL MODELLING

The geochemical modelling predicted the changes which would occur as the system evolved towards and reached the final equilibrium between the minerals, carbon dioxide, water and the dissolved constituents. The autoclave experiments never reached final equilibrium; the changes in solids were small and the total amount of dissolved carbon



dioxide was small relative to the total possible amount. However, the few changes in mineralogy which occurred during the autoclave experiments are consistent with the geochemical modelling and the water chemistry. The quartz overgrowths observed by SEM, the formation of illite and kaolinite observed by X-ray and the changes in dissolved cation and anion concentrations observed are in agreement with the modelling. The X-ray data indicated that some new minerals were forming, but insufficient amounts were present to determine which phases they were.

Clearly the amount of time necessary for equilibrium to occur, or even sufficient reactions to occur, is greater than the length of the experiments. Thus modelling is essential in order to predict long term effects of injection fluid, formation fluid and formation mineral reactions.

The implications of the experiments on subsurface injection is positive. Slow reaction rates imply that only a very limited amount of reaction will occur in the near well region, and that the dominate reaction type in this region will be dissolution. Thus, porosity and permeability will be enhanced in the near well region and injectivity will improve. Over a longer time period, the anticipated complex trapping reactions will occur at some distance from the well. This will form a partial zone of reduced permeability limiting the ultimate migration of carbon dioxide.

## 8.0 RECOMMENDATIONS

The petrophysics, formation water chemistry and mineralogy of the aquifers in the vicinity of Sundance and Genesee should be more accurately characterized. Only single well injection of liquid CO<sub>2</sub> has been considered. Injection rates of up to 1000 metric tons daily are sustainable over the life cycle of a power plant. Rates that are an order of magnitude larger, are needed to dispose of all the CO<sub>2</sub> produced by a single power plant. This would require 10 wells injecting at the same rates. Multi-well injection patterns should be optimized through more detailed numerical modelling of aquifers in the Sundance and Genesee areas. The effect of injection on the basin flow should also be considered.

One concern which has not been addressed is that the most efficient capture mechanisms are those in which carbonate minerals precipitate, which may reduce the permeability of the reservoir. The detailed examination of permeability changes is beyond the scope of this paper, as these changes depend upon the permeability and the porosity of the aquifer, the amount and surface area of the reactive minerals available, the kinetics of the reactions and on attachment mechanisms of the newly formed minerals, especially the carbonate minerals. This is not the case in carbonate aquifers because only dissolution occurs. The porosity and permeability must increase in these reservoirs as CO<sub>2</sub> is injected. The net change in porosity can be calculated for siliciclastic aquifers but the permeability can not. However, in the early stage of reaction in the siliciclastic reservoirs, dissolution is the predominant mechanism. From this, we can conclude that in the near well region of a CO<sub>2</sub> injection well, permeability and porosity should increase.

Resolution of the permeability changes in a siliciclastic reservoir can only be addressed by physical simulation using core plugs under the actual conditions of aquifer disposal; where CO<sub>2</sub>-charged water would be flowed through an aquifer core at different rates and the permeability changes monitored as a function of time. Planning of the experiments can

be guided by the existing kinetic data. Then, dissolution of clay minerals and other silicates of the Western Canada Basin in the presence of abundant CO<sub>2</sub> can be modelled using laboratory reaction rates calibrated in the autoclave experiments. Only in this manner can absolute reaction time be assessed.

The reactions considered in this 1992/93 study have been numerically simulated using a closed system reaction type of geochemical model in which the calculation is normalized to one litre of water. These calculations are limited because they assume a closed reaction environment. In reality, CO<sub>2</sub> disposal should be modelled in the context of the hydrodynamics of a sedimentary basin. In a sedimentary basin, deep groundwater moves on the order of one centimetre to one metre a year. The basins are hundreds of kilometres across, so basinal water movement is measured in thousands of years. During that time, the CO<sub>2</sub>-charged formation waters will be exposed to a much larger mass of solids than assumed for the modelling carried out here. Consequently, over periods of thousands of years, the reaction between the *basic* minerals in the aquifers will be responsible for capture of more CO<sub>2</sub> than predicted by our model calculations. This will limit the mobility of the CO<sub>2</sub> to a smaller radius than would otherwise be expected and could replace stratigraphic traps. These effects of an open system should be evaluated and included as part of any aquifer model used for assessing the long-term effects of CO<sub>2</sub> aquifer disposal.

Aquifer disposal of CO<sub>2</sub> should only be considered in a system context. In addition to the above, further geological and geochemical work is required to pinpoint disposal and monitoring well locations. Also, overall system concepts and costs should be developed starting from one or more power plants for a specific disposal scheme. In effect, a feasibility level study is needed of all system elements from environmental and permitting through to reservoir characteristics over time, in order to properly define the potential economics of aquifer disposal of CO<sub>2</sub> in a Lake Wabamun area context.

## BIBLIOGRAPHY

Bachu, S. and J.R. Underschultz, 1993: Hydrogeology of formation waters, northeastern Alberta basin. American Association of Petroleum Geologists Bulletin, in press.

Bachu, S. and R.A. Burwash 1993: Geothermal regime in the Western Canada Sedimentary Basin. In Geological Atlas of the Western Canada Sedimentary Basin (G.D. Mossop and I. Shetsen, comp.), Calgary. Canadian Society of Petroleum Geologists and Alberta Research Council, in press.

Bachu, S., and R.A. Burwash, 1991: Regional-scale analysis of the geothermal regime in the Western Canada Sedimentary Basin. Geothermics, 20, no. 5/6, pp. 387-407.

Bachu, S. 1993: Basement heat flow in the Western Canada Sedimentary Basin. Tectonophysics, in press.

Bachu, S. and J.R. Underschultz, 1992: Regional-scale porosity and permeability variations, Peace River Arch area, Alberta, Canada. American Association of Petroleum Geologists Bulletin, in press.

Brown, T.H., R.G. Berman and E.H. Perkins, 1989: PTA-SYSTEM: A GeoCalc software package for the calculation and display of activity-temperature-pressure phase diagrams. Amer. Min., 74, 485-487.

Clark, S.P., "Handbook of Physical Constants". The Geological Society of America, Inc., New York, P. 382-383, 1966.

Cleaves, E.T., A.E. Godfrey, and O.P. Bricker, 1970: Geochemical balance of a small watershed and its geomorphic implications. Geol. Soc. Amer. Bull., 81, p.3015.

Cushman, J.H., 1984: On unifying the concepts of scale, instrumentation, and stochastics in the development of multiphase transport theory. Water Resources Research, 20, pp. 1668-1676.

Dunsmore, H.E., 1992: A geological perspective on global warming and the possibility of carbon dioxide removal as calcium carbonate mineral. Energy Convers. Mgmt., 33, 565-572.

Gunter, W.D. and G.W. Bird, 1988: CO<sub>2</sub> production in tar sands reservoirs under in situ steam temperatures: reactive calcite dissolution. *Chemical Geology*, 70, 301-311.

Hitchon, B., S. Bachu, A. Sauveplane, A.T., Ing, A.T. Lytviak and J.R. Underschultz, 1989: Hydrogeological and geothermal regimes in the Phanerozoic succession, Cold Lake area, Alberta and Saskatchewan. Alberta Research Council Bulletin No. 59, 84 p.

Hitchon, B., 1991: Hydrochemistry of Phanerozoic strata, northeast Alberta; report to Alberta Research Council. Alberta Geological Survey, Open File Report 1991-20, 30 p.

Hitchon, B., S. Bachu, and J.R. Underschultz, 1990: Regional subsurface hydrogeology, Peace River Arch area, Alberta and British Columbia. Canadian Society of Petroleum Geologists, 38A, pp. 196-217.

Hitchon, B., S. Bachu, C.M. Sauveplane, and A.T. Lytviak, 1987: Dynamic Basin Analysis: an integrated approach with large data bases. In J.C. Goff and B.P.J. Williams, eds., *Fluid Flow in Sedimentary Basins and Aquifers*. Geological Society Special Publication No. 34, pp. 31-44.

Hitchon, B., 1984: Graphical and statistical treatment of standard formation water analysis. In B. Hitchon and E.I. Wallick, eds., *First Canadian/American Conference on Hydrogeology: Practical applications of ground water geochemistry*. National Water Well Association, Dublin, Ohio, pp. 225-236.

Hutcheon and Abercrombie, 1992: Upsetting the Geochemical Balance by Amalgamating Abercrombie with Fitch at West Edmonton Mall. AAPG Memoir 49, p.161.

Katz, B.G., O.P. Bricker, and M.M. Kennedy, 1985: Geochemical mass balance relationships for selected ions in precipitation and stream water. *Amer. Jour. sci.*, 285, p.931.

Kharaka, Y.K., W.D. Gunter, P.K. Agarwal, E.H. Perkins and J.D. DeBraal. SOLMINEQ.88: A computer program for geochemical modelling of water-rock reactions. U.S. Geol. Surv. Water-Resources Investigations Report 88-4227, Menlo Park.

Kirkwood, D.E. and H.W. Nesbitt, 1990: "Formation and evolution of soils from an acidified watershed: Plastic Lake, Ontario, Canada". *Geochim. Cosmochim. Acta*, 55, p.1295.

Koide, H., Y. Tazaki, Y. Noguchi, S. Nakayama, M. Iijima, K. Ito and Y. Shindo, 1992: Subterranean containment and long-term storage of carbon dioxide in unused aquifers and in depleted natural gas reservoirs. *Energy Convers. Mgmt.*, 33, 619-626.

McHugh, M.A. and V.J. Krukonis, 1986: *Supercritical Fluid Extraction, Principles and Practice*. Butterworths, Boston, P. 10.

Nesbitt, H.W. and G.M. Young, Prediction of some weathering trends of plutonic and volcanic rocks based on thermodynamic and kinetic considerations. *Geochim. Cosmochim. Acta*, 48, P.1523.

Nesbitt, H.W., 1980: Characterization of mineral-formation water interactions in Carboniferous sandstones and shales of the Illinois Sedimentary Basin: *Amer.Jour.Sci.*, 280, p.607.

Nesbitt, H.W., 1985. A chemical equilibrium model for the Illinois Basin formation waters. *Amer.Jour.Sci.*, 285, P.436.

Paces, T., 1983. Rate constants of dissolution derived from the measurements of mass balance in hydrological catchments. *Geochim. Cosmochim. Acta*, 47, p.1855.

Perkins, E.H., Y.K. Kharaka, W.D. Gunter and J.D. DeBraul, 1990: Geochemical modelling of water-rock interactions using SOLMINEQ.88. In: *Chemical Modelling of Aqueous Systems II* (eds. D.C. Melchior and R.L. Bassett), Chap. 9, pp. 117-127, ACS symposium series 416, Washington, D.C.

Perkins, E.H., 1980: A reinvestigation of the theoretical basis for the calculation of mass transfer in geochemical processes involving aqueous solutions. MSc Thesis, University of British Columbia, Vancouver.

Porter, J.E., R.A. Price, and R.G. McGrossan, 1982: The Western Canada Sedimentary Basin. *Philosophical Transactions of the Royal Society of London, Series A*, 305, pp. 169-192.

Stanley Industrial Consultants Ltd./Alberta Research Council/Mahoney Exploration. Aquifer Disposal of CO<sub>2</sub>. International Energy Agency, in preparation.

STARS Technical Manual, Version 4.0" (1990): Computer Modelling Group.

·van der Meer, L.G.H., 1992: Investigations regarding the storage of Carbon Dioxide in Aquifers in the Netherlands. Energy Convers. Mgmt., 33, 611-618.

Velbel, M.A., 1985: Geochemical mass balances and weathering rates in forested watersheds of the southern Blue Ridge. Amer.Jour.Sci., 285, p.904.

**Open File Report 1994 - 16B**

**Appendices to  
Aquifer Disposal of  
CO<sub>2</sub> - Rich Gases  
Phase 1**



# APPENDICES TO AQUIFER DISPOSAL OF CO<sub>2</sub>-RICH GASES

## Phase I

### IN THE VICINITY OF THE SUNDANCE AND GENESEE POWER PLANTS

Injectivity, Chemical Reactions and Proof of Concept

by

W.D. Gunter  
E.H. Perkins  
S. Bachu  
D. Law  
B. Wiwchar  
Z. Zhou

Alberta Research Council

and

T.J. McCann

Stanely Industrial Consultants Ltd.

C-1993-5

March 1993

#### DISCLAIMER

This report was prepared as an accounting of work conducted by the Alberta Research Council (ARC). Every possible effort was made to ensure that the work conforms to accepted scientific practice. However, neither ARC, nor any of its employees, makes and warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any of the information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process or services by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favouring by the ARC. The views and opinions of authors expressed herein do not necessarily state or reflect those of the ARC.

## TABLE OF CONTENTS

### APPENDICES

11.3.1	CORED INTERVALS FOR AQUIFERS OF INTEREST
11.3.2	FORMATION WATER ANALYSES FOR AQUIFERS OF INTEREST
11.3.3	X-RAY DIFFRACTOGRAMS OF AQUIFER MINERALOGY
11.4.1	THERMAL AQUIFER MODEL
11.5.1	GRAPHS GENERATED FROM PATH.UBC OUTPUT
11.5.2	PAPER PRESENTED AT IEA CONFERENCE "CARBON DIOXIDE DISPOSAL"
11.6.1	X-RAY DIFFRACTOGRAMS OF MINERAL REACTANTS
11.6.2	X-RAY DIFFRACTOGRAMS OF REACTION PRODUCTS

## **APPENDIX 11.3.1**

### **Cored Intervals for Aquifers of Interest**



82310	00/16-18-052-05W5/0	19560511	8	2609.700	2628.000	
82310	00/16-18-052-05W5/0	19560518	9	2699.000	2708.100	
82310	00/16-18-052-05W5/0	19560520	10	2742.300	2769.100	
82314	00/05-21-052-05W5/0	19731201	1	1595.600	1608.400	12.500
82314	00/05-21-052-05W5/0	19731202	2	1608.400	1626.700	17.700

**APPENDIX 11.3.2**

**Formation Water Analyses for Aquifers of Interest**

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 73444 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): -954107

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E79-16954-2

Well identifier Well name KB elev. Gr. elev  
 0495031111000 NATOMAS GAO PEMBINA 11-11-49-3 770.50 766.20

Interval Sampled from: 1605.00 to: 1630.00 meters KB

Formation Sampled: BNFF

Sample produced by: DST # 2 Sampling point: BOTTOM

DST Recovery 27.00 M OIL-CUT MUD  
 Date: Sampled: 1979/11/14 Received: 1979/11/16 Analyzed: 1979/12/17

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	1344.	3.441	58.5	Cl	26250.	43.576	740.4
K	28900.	43.498	739.1	HCO3	183.	0.177	3.0
Ca	691.	2.029	34.5	SO4	5123.	6.278	106.7
Mg	207.	1.002	17.0				

Specific gravity 1.0340 @ 25. C Refractive Index 1.34180 @ 25. C  
 PH 5.20 @ 21. C Resistivity ohm/m 0.13700 @ 25. C

Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 18360. Calculated TDS: 50721.  
 TDS by Evapor. @ 110 C: 64980. TDS at Ignition: 57380.

Sample appearance:

THE ANALYSIS WAS DETERMINED ON WATER EXTRACTED FROM SLIGHTLY OIL FLECKED MUD AND IS CHARACTERISTIC OF A KCL MUD FILTRATE WATER.

Remarks:

Fe PRESENT [E79-16954-1]:SAMPLED FROM TOP OF FLUID|RESISTIVITY OF THE FILTRATE :0.135 OHM/METERS @25 C|MUD.

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 73444 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): -954108

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E79-16955-2

Well identifier Well name KB elev. Gr. elev  
 0495031111000 NATOMAS GAO PEMBINA 11-11-49-3 770.50 766.20

Interval Sampled from: 1575.00 to: 1600.00 meters KB

Formation Sampled: BNFF

Sample produced by: DST # 3 Sampling point: BOTTOM (DUPL.)

DST Recovery 25.00 M MUD  
 Date: Sampled: 1979/11/14 Received: 1979/11/16 Analyzed: 1979/12/07

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	2460.	6.726	107.0	Cl	24350.	43.175	686.8
K	25200.	40.512	644.5	HCO3	317.	0.327	5.2
Ca	741.	2.324	37.0	SO4	4987.	6.527	103.8
Mg	79.	0.409	6.5				

Specific gravity 1.0350 @ 25. C Refractive Index 1.34160 @ 25. C  
 PH 7.80 @ 22. C Resistivity ohm/m 0.12600 @ 25. C

Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 17298. Calculated TDS: 47611.  
 TDS by Evapor. @ 110 C: 59380. TDS at Ignition: 53220.

Sample appearance:

THE ANALYSIS WAS DETERMINED ON WATER EXTRACTED FROM MUD AND IS CHARACTERISTIC OF A KCL MUD FILTRATE.

Remarks:

Fe NIL [E79-16955-1]:SAMPLED FROM TOP OF FLUID (DUPL.)|RESISTIVITY OF FILTRATE |0.135 OHM/METERS @ 25 C|MUD SAMPLE.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73454 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1128207

CHEMICAL & GEOLOGICAL LAB LTD

Lab. Sample ID. C81-7800-3

Well identifier Well name KB elev. Gr. elev  
 0495032116000 PCP PEMBINA 16-21-49-3 788.10 783.40

Interval Sampled from: 1608.00 to: 1628.00 meters KB

Formation Sampled: BL

Sample produced by: DST # 1 Sampling point: TOP OF TOOL

DST Recovery

169.00 M OIL-CUT MUD

Date: Sampled: 1981/03/19 Received: 1981/03/23 Analyzed: 1981/04/10

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	2160.	48.795	94.0
K	31.	0.412	0.8
Ca	24.	0.622	1.2
Mg	12.	0.513	1.0

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	1860.	27.247	52.5
HCO3	1586.	13.499	26.0
SO4	440.	4.758	9.2
CO3	240.	4.154	8.0

Specific gravity 1.0020 @ 25. C

PH 9.00 @ 25. C

Hydrogen Sulfide Description:

Organics Description:

Calculated sodium: 2148.

TDS by Evapor. @ 110 C: 6045.

Refractive Index 1.33360 @ 25. C

Resistivity ohm/m 1.23000 @ 25. C

Calculated TDS: 5504.

TDS at Ignition: 4500.

Sample appearance:

CLEAR, COLORLESS FILTRATE RECOVERED FROM WATERY MUD. ORGANICS: PRESENT.

Remarks:

Fe TRACE

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73460 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1078207

CHEMICAL & GEOLOGICAL LAB LTD

Lab. Sample ID. E80-11529-1

Well identifier Well name KB elev. Gr. elev  
 0495032810000 COLGAS DOME PEMBINA 10-28-49-3 788.10 784.40

Interval Sampled from: 1576.00 to: 1584.00 meters KB

Formation Sampled: GLC SS

Sample produced by: DST # 1 Sampling point: DOWNHOLE SAMPLER

DST Recovery

495.00 M CLEAN OIL  
 405.00 M SALT WATER-CUT OIL  
 70.00 M OIL-CUT MUD

Date: Sampled: 1980/10/09 Received: 1980/10/15 Analyzed: 1980/11/25

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	27127.	45.786	1180.0
K	255.	0.253	6.5
Ca	1554.	3.009	77.5
Mg	296.	0.945	24.4

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	45400.	49.690	1280.6
HCO3	305.	0.194	5.0
SO4	152.	0.123	3.2

Specific gravity 1.0490 @ 25. C

PH 6.60 @ 22. C

Hydrogen Sulfide Description:

Organics Description:

Calculated sodium: 27287.

TDS by Evapor. @ 110 C: 81560.

Refractive Index 1.34550 @ 25. C

Resistivity ohm/m 0.10600 @ 25. C

Calculated TDS: 74839.

TDS at Ignition: 70780.

Sample appearance:

ORGANICS: NIL. A LYNES UNITED DOWNHOLE SAMPLER #75 WAS RECOVERED @ 5000 KPA. IT CONTAINED 20.3 L OF GAS, 587 ML OF OIL & 2.1 L OF WATER.

Remarks:

Fe MUCH



AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73460 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): -1078208

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E80-11530-4

Well identifier Well name KB elev. Gr. elev  
 0495032810000 COLGAS DOME PEMBINA 10-28-49-3 788.10 784.40

Interval Sampled from: 1604.00 to: 1608.00 meters KB

Formation Sampled: BNFF

Sample produced by: DST # 2 Sampling point: BOTTOM

DST Recovery  
 100.00 M MUD- AND SALT WATER-CUT OIL  
 700.00 M OIL-CUT SALT WATER

Date: Sampled: 1980/10/10 Received: 1980/10/15 Analyzed: 1980/11/05

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	33383.	44.889	1452.1	Cl	56500.	49.265	1593.7
K	595.	0.470	15.2	HCO3	809.	0.410	13.3
Ca	2002.	3.088	99.9	SO4	514.	0.331	10.7
Mg	608.	1.547	50.0				

Specific gravity 1.0620 @ 25. C Refractive Index 1.34900 @ 25. C  
 PH 6.70 @ 22. C Resistivity ohm/m 0.08800 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 33745. Calculated TDS : 93767.  
 TDS by Evapor. @ 110 C: 95720. TDS at Ignition : 88720.

Sample appearance:

ORGANICS: NIL. THE SAMPLE CONSISTED OF SLIGHTLY MURKY SALT WATER.

Remarks:

Fe TRACE

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73466 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -904202

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E79-10548-3

Well identifier Well name KB elev. Gr. elev  
 0495032907000 COLGAS ET AL PEMBINA 7-29-49-3 800.80 796.70

Interval Sampled from: 1628.00 to: 1638.00 meters KB

Formation Sampled: BNFF

Sample produced by: DST # 1 Sampling point: BOTTOM

DST Recovery  
 5.30 M3 SALT WATER

Date: Sampled: 1979/06/08 Received: 1979/06/12 Analyzed: 1979/06/27

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	34094.	44.909	1483.0	Cl	57700.	49.285	1627.5
Ca	2367.	3.577	118.1	HCO3	698.	0.346	11.4
Mg	605.	1.508	49.8	SO4	595.	0.375	12.4

Specific gravity 1.0660 @ 25. C Refractive Index 1.34900 @ 25. C  
 PH 7.00 @ 24. C Resistivity ohm/m 0.08500 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 34107. Calculated TDS : 95717.  
 TDS by Evapor. @ 110 C: 98700. TDS at Ignition : 92200.

Sample appearance:

NA-NA+K. THE SAMPLE CONSISTED OF MURKY SALT WATER.

Remarks:

Fe TRACE

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73470 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1305512

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C83-0151-2

Well identifier Well name KB elev. Gr. elev  
 0495032914000 COLGAS DOME PEMBINA 14-29-49-3 811.50 806.90

Interval Sampled from: 1637.00 to: 1642.50 meters KB

Formation Sampled: BNFF

Sample produced by: DST # 1 Sampling point: BOTTOM

DST Recovery 20.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1983/03/16 Received: 1983/03/23 Analyzed: 1983/04/04

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	4435.	47.160	192.9	Cl	6450.	44.476	181.9
K	55.	0.344	1.4	HCO3	732.	2.933	12.0
Ca	90.	1.098	4.5	SO4	423.	2.153	8.8
Mg	67.	1.348	5.5	CO3	60.	0.489	2.0

Specific gravity 1.0080 @ 25. C Refractive Index 1.33540 @ 25. C  
 PH 8.60 @ 25. C Resistivity ohm/m 0.42700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 4477. Calculated TDS : 11927.  
 TDS by Evapor. @ 110 C: 14360. TDS at Ignition : 11270.

Sample appearance:

ORGANICS : MUCH. PALE YELLOW COLORED FILTRATE RECOVERED FROM THE WATER PORTION OF THE SAMPLE.

Remarks:

Fe TRACE [C83-0151-1] DOWN HOLE SAMPLER 187 RESISTIVITY: 1.43 OHM M @ 25 C  
 PALE YELLOW COLORED FILTRATE RECOVERED FROM MUD CONTAINING A TRACE OF HYDROCARBONS.  
 THE DOWN HOLE SAMPLER WAS RECEIVED WITH AN OPENING PRESSURE OF 400 KPA @ 23 C  
 IT CONTAINED 1300 ML MUD ONLY INSUFFICIENT RECOVERABLE GAS FOR ANALYSIS.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73470 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): -1306102

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C83-0152-6

Well identifier Well name KB elev. Gr. elev  
 0495032914000 COLGAS DOME PEMBINA 14-29-49-3 811.50 806.90

Interval Sampled from: 1613.00 to: 1619.00 meters KB

Formation Sampled: OST

Sample produced by: DST # 2 Sampling point: DOWN HOLE SAMPLE

DST Recovery 137.00 M OIL-CUT MUD  
 Date: Sampled: 1983/03/17 Received: 1983/03/23 Analyzed: 1983/04/04

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	4505.	48.068	196.0	Cl	6450.	44.628	181.9
K	47.	0.295	1.2	HCO3	946.	3.803	15.5
Ca	70.	0.857	3.5	SO4	290.	1.481	6.0
Mg	43.	0.868	3.5				

Specific gravity 1.0060 @ 25. C Refractive Index 1.33500 @ 25. C  
 PH 8.30 @ 25. C Resistivity ohm/m 0.53500 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 4516. Calculated TDS : 11835.  
 TDS by Evapor. @ 110 C: 13460. TDS at Ignition : 9850.

Sample appearance:

PALE YELLOW COLORED FILTRATE RECOVERED FROM THE WATER PORTION OF THE SAMPLE. THE DOWN HOLE SAMPLER WAS RECEIVED WITH AN OPENING PRESSURE OF 0 KPA @ 23 C IT CONTAINED 575 ML MUD AND 625 ML OIL.

Remarks:

Fe TRACE [C83-0152-3] MIDDLE 1 RESISTIVITY: 0.728 OHM M @ 25 C PALE YELLOW COLORED FILTRATE RECOVERED FROM THE WATER PORTION OF THE SAMPLE. [C83-0152-5] BOTTOM RESISTIVITY: 2.53 OHM M @ 25 C PALE YELLOW COLORED FILTRATE RECOVERED FROM OIL FILTRATED MUD.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73475 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1031506

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C81-7210-5

Well identifier Well name KB elev. Gr. elev  
 0495033103000 PCP PEMBINA 3-31-49-3 814.30 809.60

Interval Sampled from: 1660.00 to: 1669.00 meters KB

Formation Sampled: BNFF

Sample produced by: DST # 1 Sampling point: DOWN HOLE SAMPLE

DST Recovery 75.00 M MUD  
 Date: Sampled: 1981/02/24 Received: 1981/02/24 Analyzed: 1981/03/12

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	10900.	46.885	474.1	Cl	16630.	46.386	469.1
K	415.	1.050	10.6	HCO3	708.	1.147	11.6
Ca	480.	2.369	24.0	SO4	379.	0.780	7.9
Mg	170.	1.383	14.0				

Specific gravity 1.0200 @ 25. C Refractive Index 1.33800 @ 25. C  
 PH 7.60 @ 24. C Resistivity ohm/m 0.23900 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 10361. Calculated TDS: 28368.  
 TDS by Evapor. @ 110 C: 29740. TDS at Ignition: 27780.

Sample appearance:

ORGANICS: PRESENT. PALE YELLOW FILTRATE RECOVERED FROM THE WATER PORTION OF THE SAMPLE.

Remarks:

Fe TRACE

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73475 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): -1031507

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C81-7248-3

Well identifier Well name KB elev. Gr. elev  
 0495033103000 PCP PEMBINA 3-31-49-3 814.30 809.60

Interval Sampled from: 1641.00 to: 1647.00 meters KB

Formation Sampled: ELRS

Sample produced by: DST # 2 Sampling point: BOTTOM

DST Recovery 170.00 M MUD  
 Date: Sampled: 1981/02/25 Received: 1981/02/26 Analyzed: 1981/03/12

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	3250.	49.095	141.4	Cl	4320.	42.317	121.9
K	95.	0.844	2.4	HCO3	610.	3.472	10.0
Ca	47.	0.814	2.3	SO4	407.	2.943	8.5
Mg	18.	0.514	1.5				

Specific gravity 1.0040 @ 25. C Refractive Index 1.33400 @ 25. C  
 PH 8.50 @ 23. C Resistivity ohm/m 0.76700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 3138. Calculated TDS: 8230.  
 TDS by Evapor. @ 110 C: 8415. TDS at Ignition: 7865.

Sample appearance:

ORGANICS: PRESENT CLEAR, COLORLESS FILTRATE RECOVERED FROM MUD CONTAINING A TRACE OF HYDROCARBONS.

Remarks:

Fe PRESENT

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73475 Chemistry number: 4  
 AGSWDB Hard copy number (HRDCPNO): -1092406

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E81-3129

Well identifier Well name KB elev. Gr. elev  
 0495033103000 PCP PEMBINA 3-31-49-3 814.30 809.60

Interval Sampled from: 1643.00 to: 1646.00 meters KB

Formation Sampled: ELRS

Sample produced by: Sampling point: RECOVERY  
 Date: Sampled: 1981/06/25 Received: 1981/06/26 Analyzed: 1981/06/29

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	24114.	45.532	1048.9	Cl	40500.	49.589	1142.4
K	269.	0.299	6.9	HCO3	571.	0.406	9.4
Ca	1361.	2.948	67.9	SO4	12.	0.011	0.2
Mg	340.	1.215	28.0				

Specific gravity 1.0420 @ 25. C Refractive Index 1.34420 @ 25. C  
 PH 6.80 @ 26. C Resistivity ohm/m 0.13500 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 24281. Calculated TDS : 66775.  
 TDS by Evapor. @ 110 C: 71200. TDS at Ignition : 65560.

Sample appearance:

ORGANICS : NIL.

Remarks:

Fe TRACE

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73484 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1209301

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E81-9364-4

Well identifier Well name KB elev. Gr. elev  
 0495033308000 AMOCO PEMBINA 8-33-49-3 807.40 803.10

Interval Sampled from: 1615.00 to: 1621.00 meters KB

Formation Sampled: OST

Sample produced by: DST # 1 Sampling point: DOWNHOLE SAMPLER  
 DST Recovery

18.00 M OIL-CUT MUD  
 Date: Sampled: 1981/11/20 Received: 1981/11/23 Analyzed: 1981/12/08

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	21463.	45.021	933.6	Cl	36100.	49.103	1018.2
K	400.	0.493	10.2	HCO3	566.	0.447	9.3
Ca	1401.	3.371	69.9	SO4	455.	0.457	9.5
Mg	279.	1.107	23.0				

Specific gravity 1.0420 @ 25. C Refractive Index 1.34400 @ 25. C  
 PH 7.50 @ 21. C Resistivity ohm/m 0.12200 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 21707. Calculated TDS : 60221.  
 TDS by Evapor. @ 110 C: 61940. TDS at Ignition : 57680.

Sample appearance:

A LYNES UNITED DOWNHOLE SAMPLER 180 WAS RECEIVED AT 255 KPA. IT CONTAINED GAS A ND 1.8 L. OF VERY MUDDY SALT WATER. ORGNAICS: NIL.

Remarks:

Fe NIL [E81-9364-1]: [SAMPLED FROM 9.5M ABOVE TOOL. |MUD, NO ANALYSIS ATTEMPTED. |  
 [E81-9364-2]: [SAMPLED FROM TOP OF TOOL. |MUD, NO ANALYSIS ATTEMPTED. |

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73486 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1183211

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C81-10724-2

Well identifier Well name KB elev. Gr. elev  
 0495033406000 COLGAS DOME PEMBINA 6-34-49-3 800.50 796.80

Interval Sampled from: 1602.00 to: 1614.00 meters KB

Formation Sampled: BNFF

Sample produced by: DST # 1 Sampling point: TOP  
 DST Recovery

1.00 M CLEAN CONDENSATE  
 1.00 M SALT WATER

Date: Sampled: 1981/09/25 Received: 1981/09/29 Analyzed: 1981/10/29

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	32400.	43.481	1409.3	Cl	57450.	49.996	1620.5
K	563.	0.444	14.4	HCO3	500.	0.253	8.2
Ca	2302.	3.544	114.9	SO4	430.	0.276	9.0
Mg	790.	2.006	65.0				

Specific gravity 1.0600 @ 25. C Refractive Index 1.34800 @ 25. C  
 PH 7.30 @ 25. C Resistivity ohm/m 0.08900 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 33516. Calculated TDS: 94734.  
 TDS by Evapor. @ 110 C: 99000. TDS at Ignition: 89110.

Sample appearance:

CLEAR, COLORLESS FILTRATE RECOVERED FROM A SAMPLE CONTAINING A TRACE SEDIMENT.  
 ORGANICS: TRACE.

Remarks:

Fe PRESENT

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73505 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -458104

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E74-2232-2

Well identifier Well name KB elev. Gr. elev  
 0495040410000 CS KEY PEM 10-4-49-4 851.00 847.30

Interval Sampled from: 1565.15 to: 1588.62 meters KB

Formation Sampled: BR

Sample produced by: DST # 6 Sampling point:  
 DST Recovery

77.40 M MUD  
 109.70 M GAS-CUT MUD  
 382.80 M WATER  
 31.70 M MUD-CUT WATER

Date: Sampled: 1974/07/01 Received: 1974/07/04 Analyzed: 1974/07/17

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	10977.	48.139	477.5	Cl	17000.	48.344	479.5
Ca	240.	1.207	12.0	HCO3	960.	1.586	15.7
Mg	78.	0.647	6.4	SO4	36.	0.076	0.7

Specific gravity 1.0230 @ 16. C Refractive Index 1.33820 @ 25. C  
 PH 7.50 @ 27. C Resistivity ohm/m 0.24000 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 10981. Calculated TDS: 28807.  
 TDS by Evapor. @ 110 C: 30140. TDS at Ignition: 26150.

Sample appearance:

ANALYSIS DETERMINED ON COLORLESS WATER SAMPLE RECOVERED FROM MUDDY WATER SAMPL  
 E.

Remarks:

Fe PRESENT [E74-2232-1]:TOP|RES:2.57 OHM/M @ 25 C.|COLORLESS WTR RECOVERED FRO  
 M MUD|[E74-2232-3]:BOTTOM|RES: 0.240 OHM/M @ 25 C.|COLORLESS WATER RECOVERED F  
 ROM MUDDY WATER. |[E74-2232-4]:L.U.S. BOTTOM HOLE SAMPLE R. |RECEIVED UNDER A PR  
 ESSURE OF 130 PSIG. CONTAINED IN THE SAMPLER WAS GAS AND 2100 MLS OF MUD. RES:0.  
 931 OHM/M @25 C. |COLORLESS WATER RECOVERED FROM MUD SAMPLE.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73549 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1545211

CORE LABORATORIES CANADA LT. Lab. Sample ID. E84-4915-6

Well identifier Well name KB elev. Gr. elev  
 0495041406020 WESTAR ET AL PEMBINA 6-14-49-4 821.50 818.20

Interval Sampled from: 1689.00 to: 1693.50 meters KB

Formation Sampled: MISS SYS

Sample produced by: DST # 1 Sampling point: DOWNHOLE SAMPLER  
 DST Recovery

54.00 M CLEAN OIL  
 65.00 M OIL-CUT MUD  
 36.00 M SALT WATER

Date: Sampled: 1984/05/31 Received: 1984/06/01 Analyzed: 1984/06/06

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	29090.	45.474	1265.3	Cl	47500.	48.150	1339.8
K	386.	0.355	9.9	HCO3	961.	0.566	15.7
Ca	2098.	3.762	104.7	SO4	591.	0.442	12.3
Mg	423.	1.251	34.8				

Specific gravity 1.0490 @ 25. C Refractive Index 1.34640 @ 25. C  
 PH 7.80 @ 25. C Resistivity ohm/m 0.08900 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 28242. Calculated TDS : 79327.  
 TDS by Evapor. @ 110 C: 93800. TDS at Ignition : 77800.

Sample appearance:

NORTHSTAR TESTERS DOWNHOLE SAMPLER RECEIVED UNDER ATMOSPHERIC PRESSURE AND CONTAINED 4.3 L OF OIL STAINED SALT WATER. (5% OIL).

Remarks:

Fe MUCH [E84-4915-1]:SAMPLED FROM 155 M ABOVE TOOL. |RESISTIVITY:0.526 OHM METERS @25C. |OIL FLECKED MUD. | [E84-4915-4]:SAMPLED FROM 36 M ABOVE TOOL. |RESISTIVITY:0.100 OHM METERS @25C. |MURKY WATER. SLIGHT TRACE OF OIL. | [E84-4915-5]:SAMPLED FROM ABOVE TOOL. |RESISTIVITY:0.094 OHM METERS @25C. |MURKY WATER. SLIGHT TRACE OF OIL.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73549 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): -1545302

CHEMEX LABS (ALBERTA) LTD.

Lab. Sample ID. WFST1101

Well identifier Well name KB elev. Gr. elev  
 0495041406020 WESTAR ET AL PEMBINA 6-14-49-4 821.50 818.20

Interval Sampled from: 1688.00 to: 1690.00 meters KB

Formation Sampled: MISS SYS

Sample produced by: Sampling point:  
 Date: Sampled: 1984/06/21 Received: 1984/07/16 Analyzed: 1984/07/17

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	27700.	46.576	1204.9	Cl	42600.	46.448	1201.6
K	590.	0.583	15.1	HCO3	337.	0.213	5.5
Ca	1920.	3.704	95.8	SO4	323.	0.260	6.7
Mg	695.	2.211	57.2				
Fe	4.	0.005	0.1				

Specific gravity 1.0570 @ 0. C Refractive Index 1.34800 @ 0. C  
 PH 6.70 @ 25. C Resistivity ohm/m 0.09800 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 24391. Calculated TDS : 70095.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73549 Chemistry number: 4  
 AGSWDB Hard copy number (HRDCPNO): -1545303

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7021-84-711

Well identifier Well name KB elev. Gr. elev  
 0495041406020 WESTAR ET AL PEMBINA 6-14-49-4 821.50 818.20

Interval Sampled from: 1688.00 to: 1690.00 meters KB

Formation Sampled: MISS SYS

Sample produced by:  
 CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	29500.	44.924	1283.2
K	466.	0.417	11.9
Ca	1708.	2.984	85.2
Mg	562.	1.619	46.2

Sampling point: WATER SAMPLE  
 ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	50263.	49.635	1417.7
HCO3	446.	0.256	7.3
SO4	225.	0.164	4.7

Specific gravity 1.0590 @ 15. C  
 PH 6.60 @ 0. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 29850.

Refractive Index 1.34560 @ 22. C  
 Resistivity ohm/m 0.08500 @ 25. C  
 Calculated TDS : 82827.

Sample appearance:

NALC EQUIV. 83208.

Remarks:

Fe N.D.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73570 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1574112

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7012-84-1762

Well identifier Well name KB elev. Gr. elev  
 0495041816020 GEI ET AL PEMBINA 16-18-49-4 852.90 848.20

Interval Sampled from: 1771.00 to: 1781.00 meters KB

Formation Sampled: GLC SS

Sample produced by: DST # 2

Sampling point: BOTTOM

DST Recovery  
 30.00 M GAS-CUT OIL  
 65.00 M GAS-CUT MUD

Date: Sampled: 1984/09/30 Received: 1984/10/03 Analyzed: 1984/10/09

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	9000.	44.594	391.5
K	143.	0.417	3.7
Ca	472.	2.683	23.6
Mg	239.	2.240	19.7

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	15039.	48.321	424.2
HCO3	679.	1.268	11.1
SO4	201.	0.477	4.2

Specific gravity 1.0180 @ 15. C  
 PH 7.30 @ 0. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 9112.

Refractive Index 1.33560 @ 22. C  
 Resistivity ohm/m 0.26000 @ 25. C  
 Calculated TDS : 25396.

Sample appearance:

NALC EQUIV. 25393.

Remarks:

Fe N D

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73570 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): -1574201

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7012-84-1762

Well identifier Well name KB elev. Gr. elev  
 0495041816020 GEI ET AL PEMBINA 16-18-49-4 852.90 848.20

Interval Sampled from: 1725.00 to: 1729.00 meters KB

Formation Sampled: GLC SS

Sample produced by: DST # 3 Sampling point: BOTTOM

DST Recovery  
 22.00 M FRESH WATER  
 90.00 M MUD- AND GAS-CUT WATER

Date: Sampled: 1984/10/01 Received: 1984/10/03 Analyzed: 1984/10/09

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	2350.	48.473	102.2	Cl	3089.	41.317	87.1
K	26.	0.315	0.7	HCO3	1015.	7.888	16.6
Ca	24.	0.568	1.2	SO4	118.	1.165	2.5
Mg	7.	0.273	0.6				

Specific gravity 1.0055 @ 15. C Refractive Index 1.33300 @ 22. C  
 PH 8.30 @ 0. C Resistivity ohm/m 0.97000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 2401. Calculated TDS : 6138.

Sample appearance:

NACL EQUIV. 5836.

Remarks:

Fe N D

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73591 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1376311

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7023-83-27

Well identifier Well name KB elev. Gr. elev  
 0495042514000 PCP PEMBINA 14-25-49-4 817.40 812.70

Interval Sampled from: 1661.00 to: 1664.00 meters KB

Formation Sampled: OST

Sample produced by: DST # 1 Sampling point: BOTTOMHOLE SAMPL

DST Recovery  
 59.00 M GAS-CUT MUD  
 20.00 M OIL-CUT MUD  
 95.80 M WATER

Date: Sampled: 1983/01/17 Received: 1983/01/19 Analyzed: 1983/01/25

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	13200.	45.263	574.2	Cl	21690.	48.229	611.8
K	200.	0.403	5.1	HCO3	882.	1.140	14.5
Ca	656.	2.581	32.7	SO4	477.	0.783	9.9
Mg	247.	1.602	20.3				

Specific gravity 1.0268 @ 25. C Refractive Index 1.33920 @ 25. C  
 PH 7.20 @ 25. C Resistivity ohm/m 0.18000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 13407. Calculated TDS : 36911.

Sample appearance:

NACL EQUIVALENT = 36685. INSUFFICIENT SAMPLE FOR ROUTINE OIL ANALYSIS.

Remarks:

Fe PRESENT



-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73594 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1488304

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E84-00089-4

Well identifier Well name KB elev. Gr. elev  
 0495042806020 ANDEX ET AL PEMBINA 6-28-49-4 813.00 808.90

Interval Sampled from: 1689.00 to: 1726.00 meters KB

Formation Sampled: NORD

Sample produced by: DST # 1 Sampling point: DOWNHOLE SAMPLER  
 DST Recovery

10.00 M MUD-CUT OIL  
 90.00 M GAS-CUT MUD

Date: Sampled: 1984/01/02 Received: 1984/01/05 Analyzed: 1984/01/24

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	11990.	46.263	521.5	Cl	18700.	46.789	527.5
K	167.	0.379	4.3	HCO3	778.	1.131	12.8
Ca	529.	2.342	26.4	SO4	831.	1.535	17.3
Mg	214.	1.562	17.6				

Specific gravity 1.0220 @ 25. C Refractive Index 1.33860 @ 25. C  
 PH 8.00 @ 22. C Resistivity ohm/m 0.19100 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 11806. Calculated TDS : 32463.  
 TDS by Evapor. @ 110 C: 32960. TDS at Ignition : 31070.

Sample appearance:

ORGANICS: TRACE. LYNES UNITED DOWNHOLE SAMPLER 51 RECEIVED UNDER 2410 KPA PRES SURE. RECOVERED FROM THE CHAMBER WAS GAS AND 50 ML. OF OIL CUT MUDDY WATER. (17 % OIL)

Remarks:

Fe NIL [E84-00089-1]: SAMPLED FROM TOP | RESISTIVITY: 1.28 OHM/METERS @ 25 C. | M UD. | [E84-00089-2]: SAMPLED FROM MIDDLE: RESISTIVITY: 0.240 OHM/METERS @ 25 C. | OIL CUT MUDDY WATER (20% OIL).  
 -----

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73598 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -835108

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7022-857

Well identifier Well name KB elev. Gr. elev  
 0495042911000 FOCUS ZEPHYR PEMBINA 11-29-49-4 828.00 823.60

Interval Sampled from: 1727.00 to: 1730.00 meters KB

Formation Sampled: OST

Sample produced by: Sampling point: SWABBING  
 Data: Sampled: 1978/11/16 Received: 1978/11/20 Analyzed: 1978/12/01

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	16800.	44.013	730.8	Cl	29202.	49.610	823.7
K	400.	0.616	10.2	HCO3	327.	0.323	5.4
Ca	1756.	5.278	87.6	SO4	53.	0.066	1.1
Mg	19.	0.094	1.6				

Specific gravity 1.0348 @ 15. C Refractive Index 1.34050 @ 25. C  
 PH 6.60 @ 0. C Resistivity ohm/m 0.13000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 17036. Calculated TDS : 48227.

Sample appearance:

APPEARANCE: MUD SETTLED ON BOTTOM. NACL EQUIV 48223

Remarks:

Fe TRACE  
 -----

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73606 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1144306

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E81-2096-1

Well identifier Well name KB elev. Gr. elev  
 0495043611000 COLGAS DOME PEMBINA 11-36-49-4 814.40 810.70

Interval Sampled from: 1616.00 to: 1623.00 meters KB

Formation Sampled: OST

Sample produced by: DST # 1 Sampling point: TOP OF TOOL

DST Recovery 18.00 M MUD-CUT WATER  
 Date: Sampled: 1981/05/25 Received: 1981/06/01 Analyzed: 1981/06/12

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	1867.	48.481	81.2	Cl	1780.	29.973	50.2
K	24.	0.366	0.6	HCO3	1281.	12.533	21.0
Ca	29.	0.864	1.4	SO4	247.	3.070	5.1
Mg	6.	0.295	0.5	CO3	222.	4.417	7.4

Specific gravity 1.0030 @ 25. C Refractive Index 1.33370 @ 25. C  
 PH 8.90 @ 23. C Resistivity ohm/m 1.30000 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 1881. Calculated TDS : 4795.  
 TDS by Evapor. @ 110 C: 5105. TDS at Ignition : 4595.

Sample appearance:

ORGANICS: PRESENT. THE SAMPLE CONSISTED OF VERY MUDDY WATER WITH A TRACE OF HYDROCARBON.

Remarks:

Fe TRACE [E81-2096-3]: DOWN HOLE SAMPLER | A LYNES DOWN HOLE SAMPLER WAS RECEIVED AT ATMOSPHERIC PRESSURE | IT CONTAINED 30 ML. OF MUD ONLY, INSUFFICIENT FOR ANALYSIS.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73666 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1545304

CORE LABORATORIES CANADA LT. Lab. Sample ID. C84-5196-4

Well identifier Well name KB elev. Gr. elev  
 0495051416020 PROPHET ET AL PEMBINA 16-14-49-5 799.60 795.60

Interval Sampled from: 1739.00 to: 1746.00 meters KB

Formation Sampled: MISS SYS

Sample produced by: DST # 1 Sampling point: DOWN HOLE SAMPLE

DST Recovery 58.00 M CLEAN OIL  
 258.00 M OIL- AND GAS-CUT SALT WATER  
 Date: Sampled: 1984/06/08 Received: 1984/06/18 Analyzed: 1984/06/21

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	33900.	41.029	1474.6	Cl	63000.	49.444	1777.0
K	813.	0.579	20.8	HCO3	944.	0.430	15.5
Ca	4084.	5.670	203.8	SO4	689.	0.399	14.3
Mg	1069.	2.448	88.0				

Specific gravity 1.0680 @ 25. C Refractive Index 1.34950 @ 25. C  
 PH 7.20 @ 25. C Resistivity ohm/m 0.07900 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 34835. Calculated TDS : 104141.  
 TDS by Evapor. @ 110 C: 116200. TDS at Ignition : 101700.

Sample appearance:

A LYNES UNITED DOWNHOLE SAMPLER 214 WAS REC'D UNDER 689 KPA PRESSURE. RECOVERED FROM THE CHAMBER WAS GAS AND 1.9 L OF OIL STAINED MUDDY SALT WATER.

Remarks:

Fe PRESENT

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73666 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): -1545306

CORE LABORATORIES CANADA LT. Lab. Sample ID. E84-5197-5

Well identifier Well name KB elev. Gr. elev  
 0495051416020 PROPHET ET AL PEMBINA 16-14-49-5 799.60 795.60

Interval Sampled from: 1731.00 to: 1738.00 meters KB

Formation Sampled: NORD

Sample produced by: DST # 3 Sampling point: DOWN HOLE SAMPLE

DST Recovery  
 138.00 M CLEAN OIL  
 380.00 M OIL-CUT SALT WATER

Date: Sampled: 1984/06/09 Received: 1984/06/10 Analyzed: 1984/06/25

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	32450.	42.484	1411.5	Cl	58000.	49.240	1636.0
K	640.	0.493	16.4	HCO3	1010.	0.498	16.6
Ca	3275.	4.919	163.4	SO4	835.	0.523	17.4
Mg	744.	1.843	61.2				

Specific gravity 1.0600 @ 25. C Refractive Index 1.34940 @ 25. C  
 PH 6.90 @ 26. C Resistivity ohm/m 0.08400 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 33230. Calculated TDS: 96580.  
 TDS by Evapor. @ 110 C: 106400. TDS at Ignition: 94480.

Sample appearance:

LYNES UNITED SERVICES LTD. DOWNHOLE SAMPLER 56 RECEIVED UNDER 3792 KPA. RECOVERED FROM THE CHAMBER WAS GAS AND 2.5 L. OF OIL AND WATER. (13% OIL.).

Remarks:

Fe MUCH

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73666 Chemistry number: 5  
 AGSWDB Hard copy number (HRDCPNO): -1545308

CORE LABORATORIES CANADA LT. Lab. Sample ID. E84-5198-1

Well identifier Well name KB elev. Gr. elev  
 0495051416020 PROPHET ET AL PEMBINA 16-14-49-5 799.60 795.60

Interval Sampled from: 1705.00 to: 1712.00 meters KB

Formation Sampled: MISS SYS

Sample produced by: DST # 5 Sampling point: TOP

DST Recovery  
 143.00 M MUD  
 199.00 M GAS-CUT SALT WATER

Date: Sampled: 1984/06/10 Received: 1984/06/10 Analyzed: 1984/06/15

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	42090.	37.752	1830.8	Cl	86000.	50.019	2425.7
K	724.	0.382	18.5	HCO3	549.	0.186	9.0
Ca	7988.	8.219	398.6	SO4	335.	0.144	7.0
Mg	1944.	3.299	160.0				

Specific gravity 1.0860 @ 25. C Refractive Index 1.35670 @ 25. C  
 PH 7.20 @ 26. C Resistivity ohm/m 0.06700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 43299. Calculated TDS: 139836.  
 TDS by Evapor. @ 110 C: 161600. TDS at Ignition: 133700.

Sample appearance:

THE SAMPLE CONSISTED OF SLIGHTLY MUDDY SALT WATER.

Remarks:

Fe PRESENT [E84-05198-2]: SAMPLED FROM MIDDLE. [RESISTIVITY: 0.071 OHM/METERS @ 25 C.] [SLIGHTLY MUDDY WATER.] [H2S. PRESENT. [E84-05198-3]: SAMPLED FROM BOTTOM [RESISTIVITY: 0.070 OHM/METERS @ 25C.] [SLIGHTLY MUDDY WATER.] [H2S. PRESENT. [E84-05198-4]: SAMPLED FROM DOWNHOLE SAMPLER. [RES.: 0.126 OHM/METERS @ 25C.] [LYNES UNITED SERVICES LTD.] [DOWNHOLE SAMPLER 65 RECEIVED UNDER ATMOSPHERIC PRESSURE AND CONTAINED 600 ML OF MUD ONLY.]

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 73715 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -293409

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. 9758

Well identifier Well name KB elev. Gr. elev  
 0495053108000 WHITE ROSE-SUPERTEST W. ALSIKE 8-31 780.30 776.60

Interval Sampled from: 1940.66 to: 1948.59 meters KB

Formation Sampled: WAB

Sample produced by: DST # 3 Sampling point:  
 Date: Sampled: 1957/04/30 Analyzed: 1957/05/02

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	45344.	35.409	1972.4	Cl	98016.	49.633	2764.7
Ca	12958.	11.608	646.6	HCO3	680.	0.200	11.1
Mg	2016.	2.978	165.9	SO4	461.	0.172	9.6

Specific gravity 1.1100 @ 0. C  
 PH 7.20 @ 0. C  
 Calculated sodium: 45364.  
 TDS by Evapor. @ 110 C: 161200.

Resistivity ohm/m 0.07200 @ 20. C  
 Calculated TDS : 159149.  
 TDS at Ignition : 147100.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78124 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39591

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C81-7501-2

Well identifier Well name KB elev. Gr. elev  
 0505030210000 COLGAS GENESEE 10-2-50-3 799.80 796.10

Interval Sampled from: 1564.00 to: 1571.00 meters KB

Formation Sampled: OSTRACOD

Sample produced by: DST # 3 Sampling point: BOTTOM  
 DST Recovery

9.00 M MUD  
 Date: Sampled: 1981/03/08 Received: 1981/03/12 Analyzed: 1981/03/24

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	1425.	53.566	62.0	Cl	675.	16.453	19.0
K	16.	0.354	0.4	HCO3	1440.	20.395	23.6
Ca	24.	1.035	1.2	SO4	150.	2.699	3.1
Mg	19.	1.351	1.6	CO3	144.	4.147	4.8

Specific gravity 1.0020 @ 25. C  
 PH 9.00 @ 23. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 1099.  
 TDS by Evapor. @ 110 C: 5336.

Refractive Index 1.33340 @ 25. C  
 Resistivity ohm/m 1.98000 @ 25. C  
 Calculated TDS : 2819.  
 TDS at Ignition : 3204.

Sample appearance:

CLEAR, COLORLESS FILTRATE REC'D FROM MUD.

Remarks:

FE MUCH. C81-7501-3 DHS #81 DHS HAD AN OPENING PRESSURE OF 0 KPA @ 20 C. IT CO  
 NTAINED NO FLUID.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78124 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): 39592

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C81-7502-3

Well identifier Well name KB elev. Gr. elev  
 0505030210000 COLGAS GENESEE 10-2-50-3 799.80 796.10

Interval Sampled from: 1548.00 to: 1558.00 meters KB

Formation Sampled: GLAUCONITIC

Sample produced by: DST # 4 Sampling point: BOTTOM

DST Recovery  
 38.00 M OIL-CUT MUD  
 Date: Sampled: 1981/03/09 Received: 1981/03/12 Analyzed: 1981/03/30

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	1195.	54.747	52.0	Cl	650.	19.310	18.3
K	4.	0.108	0.1	HCO3	1141.	19.695	18.7
Ca	16.	0.841	0.8	SO4	49.	1.075	1.0
Mg	5.	0.433	0.4	CO3	108.	3.791	3.6

Specific gravity 1.0000 @ 25. C Refractive Index 1.33320 @ 25. C  
 PH 9.00 @ 24. C Resistivity ohm/m 2.16000 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 930. Calculated TDS : 2319.  
 TDS by Evapor. @ 110 C: 4220. TDS at Ignition : 2376.

Sample appearance:

PALE YELLOW FILTRATE RECOVERED FROM OIL FLECKED WATERY MUD.

Remarks:

FE PRESENT. C81-7502-1 TOP RES: 2.36 OHM/M @25C PALE YELLOW FILTRATE RECOVERED FROM OIL FLECKED MUD. -2 MIDDLE RES: 2.34 OHM/M @25C PALE YELLOW FILTRATE RECOVERED FROM MUD WITH TRACE HYDROCARBONS. 4 DHS #176 NO ANALYSIS.  
 ~~~~~

-----  
 | AGSWDB WATER ANALYSIS REPORT |  
 -----

AGSWDB Well site identifier (SITID): 78129 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39596

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C81-8438-4

Well identifier Well name KB elev. Gr. elev  
 0505030601000 COLGAS DOME GENESEE 1-6-50-3 787.30 783.60

Interval Sampled from: 1607.00 to: 1616.00 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 2 Sampling point: BOTTOM

DST Recovery  
 25.00 M MUD  
 70.00 M GAS- AND OIL-CUT MUD  
 55.00 M OIL-CUT SALT WATER  
 Date: Sampled: 1981/05/08 Received: 1981/05/12 Analyzed: 1981/05/29

| CATIONS |        |        |        | ANIONS |        |        |        |
|---------|--------|--------|--------|--------|--------|--------|--------|
| ION     | mg/l   | %MEQ   | MEQ/L  | ION    | mg/l   | %MEQ   | MEQ/L  |
| Na      | 25090. | 40.346 | 1091.4 | Cl     | 50300. | 52.451 | 1418.8 |
| K       | 516.   | 0.488  | 13.2   | HCO3   | 720.   | 0.436  | 11.8   |
| Ca      | 1942.  | 3.583  | 96.9   | SO4    | 551.   | 0.424  | 11.5   |
| Mg      | 747.   | 2.272  | 61.5   |        |        |        |        |

Specific gravity 1.0560 @ 25. C Refractive Index 1.34740 @ 25. C  
 PH 7.40 @ 23. C Resistivity ohm/m 0.08600 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 29515. Calculated TDS : 83409.  
 TDS by Evapor. @ 110 C: 113900. TDS at Ignition : 83620.

Sample appearance:

CLEAR COLORLESS FILTRATE WITH APP. 30% SEDIMENT AND TRACE HYDROCARBONS.

Remarks:

FE MUCH. C81-8438-2 TOP RES: .289 OHM/M @25C CLEAR COLORLESS FILTRATE RECOVERED FROM MUD. -3 MIDDLE RES: .102 OHM/M @25C CLEAR COLORLESS FILTRATE RECOVERED FROM WATER. -4 DHS RES: .089 OHM/M @25C CLEAR COLORLESS FILTRATE RECOVERED FROM OIL FLECKED WATERY MUD.  
 ~~~~~

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78134 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39600  
 CHEMEX LABS (ALBERTA) LTD. Lab. Sample ID. 82-42-2-5X-3832  
 Well identifier Well name KB elev. Gr. elev  
 0505030706000 PCP GENESEE 6-7-50-3 766.80 763.00  
 Interval Sampled from: 1584.50 to: 1588.00 meters KB  
 Formation Sampled: OST 3120

Sample produced by: Sampling point: SEPARATOR  
 Date: Sampled: 1983/03/14 Received: 1983/03/16 Analyzed: 1983/03/17

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	28800.	31.435	1252.7	Cl	72700.	51.456	2050.6
K	500.	0.321	12.8	HCO3	771.	0.317	12.6
Ca	8000.	10.017	399.2	SO4	393.	0.205	8.2
Mg	3000.	6.195	246.9				
Fe	60.	0.054	2.1				

Specific gravity 1.0900 @ 15. C Refractive Index 1.35100 @ 25. C  
 PH 7.35 @ 25. C Resistivity ohm/m 0.09400 @ 25. C  
 Calculated sodium: 32775. Calculated TDS : 117247.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78139 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39611  
 CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E83-10726-4  
 Well identifier Well name KB elev. Gr. elev  
 0505031806000 COLGAS DOME GENESEE 6-18-50-3 738.50 734.80  
 Interval Sampled from: 1559.50 to: 1564.00 meters KB  
 Formation Sampled: ELLERSLIE

Sample produced by: DST # 3 Sampling point: TOP OF TOOL  
 DST Recovery  
 163.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1983/02/28 Received: 1983/03/02 Analyzed: 1983/03/10

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	4810.	48.827	209.2	Cl	6400.	42.128	180.5
K	74.	0.442	1.9	HCO3	1275.	4.876	20.9
Ca	80.	0.932	4.0	SO4	387.	1.880	8.1
Mg	46.	0.883	3.8	CO3	4.	0.031	0.1

Specific gravity 1.0090 @ 25. C Refractive Index 1.33510 @ 25. C  
 PH 8.70 @ 23. C Resistivity ohm/m 0.47200 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 4640. Calculated TDS : 12184.  
 TDS by Evapor. @ 110 C: 13280. TDS at Ignition : 10500.

Sample appearance:

SLIGHTLY SALTY WATER EXTRACTED FROM OIL FLECKED MUD.

Remarks:

FE PRESENT. E83-10726-1 152M ABOVE TOOL RES OF FILT: 1.80 OHM/M @25C MUD. -2 7  
 6M ABOVE TOOL RES OF FILT: 1.48 OHM/M @25C MUD. -3 19M ABOVE TOOL RES OF FILT:  
 .594 OHM/M @25C OIL FLECKED MUD. -5 DHS RES OF FILT: .502 OHM/M @25C QUINN DH  
 S REC'D @ATM PRESSURE, 1.4L OF OIL FLECKED MUD.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78247 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39773

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E85-13930

Well identifier Well name KB elev. Gr. elev  
 0505053608000 ANDEX ET AL HIGHVALE 8-36-50-5 760.60 755.80

Interval Sampled from: 1602.00 to: 1606.00 meters KB

Formation Sampled: NORDEGG

Sample produced by: Sampling point: TEST SEPARATOR  
 Date: Sampled: 1985/04/01 Received: 1985/04/04 Analyzed: 1985/04/19

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	33570.	39.389	1460.2	Cl	66100.	50.292	1864.4
K	795.	0.548	20.3	HCO3	466.	0.206	7.6
Ca	4653.	6.263	232.2	SO4	539.	0.303	11.2
Mg	1351.	2.999	111.2				

Other Determinations

Parameter	mg/l
boron	19.
strontium	354.

Specific gravity 1.0700 @ 25. C Refractive Index 1.35150 @ 25. C  
 PH 7.00 @ 21. C Resistivity ohm/m 0.07700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 35407. Calculated TDS: 108280.  
 TDS by Evapor. @ 110 C: 121400. TDS at Ignition: 106400.

Remarks:

FE PRESENT.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78247 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39774

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E85-13872-4

Well identifier Well name KB elev. Gr. elev  
 0505053608000 ANDEX ET AL HIGHVALE 8-36-50-5 760.60 755.80

Interval Sampled from: 1607.00 to: 1625.00 meters KB

Formation Sampled: BF

Sample produced by: DST # 1 Sampling point: DHS  
 DST Recovery

9.00 M OIL-CUT MUD  
 129.00 M GAS- AND OIL-CUT MUD

Date: Sampled: 1985/03/19 Received: 1985/03/21 Analyzed: 1985/04/09

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	7100.	45.236	308.8	Cl	11090.	45.819	312.8
K	98.	0.367	2.5	HCO3	686.	1.647	11.2
Ca	238.	1.740	11.9	SO4	1062.	3.239	22.1
Mg	162.	1.953	13.3				

Specific gravity 1.0100 @ 25. C Refractive Index 1.33600 @ 25. C  
 PH 8.00 @ 23. C Resistivity ohm/m 0.28300 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 7379. Calculated TDS: 20269.  
 TDS by Evapor. @ 110 C: 20160. TDS at Ignition: 18400.

Sample appearance:

LYNES DHS REC'D @ATM PRESSURE, 400MLS SLIGHTLY SALTY OIL CUT MUDDY WATER (8% OIL).

Remarks:

FE TRACE. E85-13872-1 TOP RES: 1.03 OHM/M @25C MUD, TRACE HYDROCARBON. -2 MIDD  
 LE RES: .341 OHM/M @25C OIL CUT MUDDY WATER (16% OIL). -3 BOTTOM RES: .312 OHM  
 /M @25C OIL CUT MUDDY WATER (10% OIL).

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 78240 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39764

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E81-17778-3

Well identifier Well name KB elev. Gr. elev  
 0505052403000 ANDEX ET AL HIGHVALE 3-24-50-5 695.80 691.70

Interval Sampled from: 1573.00 to: 1580.00 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 1 Sampling point: DHS

DST Recovery 38.00 M OIL-CUT MUD  
 Date: Sampled: 1981/02/26 Received: 1981/03/04 Analyzed: 1981/03/17

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	3826.	46.954	166.4
K	40.	0.289	1.0
Ca	108.	1.521	5.4
Mg	53.	1.230	4.4

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	5520.	43.929	155.7
HCO3	791.	3.658	13.0
SO4	412.	2.420	8.6

Specific gravity 1.0040 @ 25. C Refractive Index 1.33500 @ 25. C  
 PH 7.50 @ 22. C Resistivity ohm/m 0.58900 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 3851. Calculated TDS : 10333.  
 TDS by Evapor. @ 110 C: 10720. TDS at Ignition : 9040.

Sample appearance:

QUINN DHS REC'D @620 KPA. GAS AND 3.4L OF OIL CUT MUD.

Remarks:

FE NIL. E81-17778-1 OM RES: 1.50 OHM/M @25C OIL FLECKED MUD.

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 78243 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39769

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E85-15363-3

Well identifier Well name KB elev. Gr. elev  
 0505052516000 ANDEX ET AL HIGHVALE 16-25-50-5 780.50 775.70

Interval Sampled from: 1624.00 to: 1645.00 meters KB

Formation Sampled: NORDEGG

Sample produced by: DST # 1 Sampling point: BOTTOM

DST Recovery 361.00 M CLEAN OIL  
 10.00 M OIL-CUT MUD  
 Date: Sampled: 1985/05/15 Received: 1985/05/17 Analyzed: 1985/05/24

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	4360.	47.150	189.6
K	48.	0.305	1.2
Ca	80.	0.992	4.0
Mg	39.	0.798	3.2

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	5810.	40.743	163.9
HCO3	1527.	6.222	25.0
SO4	732.	3.789	15.2

Specific gravity 1.0080 @ 25. C Refractive Index 1.33470 @ 25. C  
 PH 7.90 @ 26. C Resistivity ohm/m 0.50400 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 4528. Calculated TDS : 11940.  
 TDS by Evapor. @ 110 C: 11870. TDS at Ignition : 9960.

Sample appearance:

CLEAR COLORLESS SLIGHTLY SALTY WATER RECOVERED FROM OIL CUT MUD (36% OIL).

Remarks:

FE TRACE.



AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78152 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39628

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C82-13309

Well identifier Well name KB elev. Gr. elev  
 0505040208000 COLGAS ET AL PEMBINA 8-2-50-4 803.60 799.90

Interval Sampled from: 1636.00 to: 1646.00 meters KB

Formation Sampled: BF

Sample produced by: Sampling point: STOCK TANK  
 Date: 1982/01/25 Received: 1982/01/25 Analyzed: 1982/02/15

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	26790.	44.122	1165.3	Cl	46900.	50.089	1322.9
K	704.	0.682	18.0	HCO3	986.	0.612	16.2
Ca	1413.	2.670	70.5	SO4	700.	0.552	14.6
Mg	409.	1.274	33.7				

Specific gravity 1.0530 @ 25. C Refractive Index 1.34590 @ 25. C  
 PH 7.90 @ 24. C Resistivity ohm/m 0.10100 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 28727. Calculated TDS : 78634.  
 TDS by Evapor. @ 110 C: 80060. TDS at Ignition : 74930.

Sample appearance:

CLEAR COLORLESS FILTRATE WITH TRACE SEDIMENT.

Remarks:

FE TRACE.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78152 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39629

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E81-7919-2

Well identifier Well name KB elev. Gr. elev  
 0505040208000 COLGAS ET AL PEMBINA 8-2-50-4 803.60 799.90

Interval Sampled from: 1633.00 to: 1647.00 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 2 Sampling point: MIDDLE

DST Recovery  
 35.00 M CLEAN OIL  
 40.00 M GAS- AND OIL-CUT MUD  
 Date: 1981/10/11 Received: 1981/10/13 Analyzed: 1981/11/02

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	4486.	47.134	195.1	Cl	6570.	44.764	185.3
K	125.	0.772	3.2	HCO3	622.	2.462	10.2
Ca	148.	1.784	7.4	SO4	477.	2.399	9.9
Mg	15.	0.298	1.2	CO3	48.	0.386	1.6

Specific gravity 1.0080 @ 25. C Refractive Index 1.33490 @ 25. C  
 PH 8.50 @ 22. C Resistivity ohm/m 0.47700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 4562. Calculated TDS : 12126.  
 TDS by Evapor. @ 110 C: 12180. TDS at Ignition : 11020.

Sample appearance:

SLIGHTLY SALTY WATER EXTRACTED FROM SLIGHTLY OIL CUT MUD.

Remarks:

FE PRESENT. E81-7919-1 TOP RES OF FILT: .476 OHM/M @25C SLIGHTLY OIL CUT MUD.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78147 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39625

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E82-13342-3

Well identifier Well name KB elev. Gr. elev  
 0505040106000 PCP PEMBINA 6-1-50-4 790.40 785.70

Interval Sampled from: 1614.50 to: 1647.00 meters KB

Formation Sampled: GLC

Sample produced by: DST # 1 Sampling point: 28M ABOVE TOOL

DST Recovery  
 28.00 M CLEAN OIL  
 140.00 M GAS- AND OIL-CUT MUD

Date: Sampled: 1982/03/02 Received: 1982/03/05 Analyzed: 1982/03/12

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	1369.	31.111	59.5
K	64.	0.855	1.6
Ca	537.	14.000	26.8
Mg	94.	4.041	7.7

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	1350.	19.894	38.1
HCO3	3228.	27.640	52.9
SO4	226.	2.458	4.7

Specific gravity	1.0040 @ 25. C	Refractive Index	1.33700 @ 25. C
PH	8.00 @ 23. C	Resistivity ohm/m	2.08000 @ 25. C
Hydrogen Sulfide Description:			
Organics Description :			
Calculated sodium:	1406.	Calculated TDS :	5200.
TDS by Evapor. @ 110 C:	11470.	TDS at Ignition :	3080.

Sample appearance:

INHIBITOR CONTAMINATED MUDDY WATER.

Remarks:

FE PRESENT. E82-13342-1 168M RES: 2.76 OHM/M @25C (SAME AS ABOVE). E82-13342-2  
 98M RES: 2.66 OHM/M @25C (SAME AS ABOVE).

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78149 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39626

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C82-11979-4

Well identifier Well name KB elev. Gr. elev  
 0505040108020 PCP PEMBINA A8-1-50-4 789.60 784.90

Interval Sampled from: 1610.00 to: 1620.00 meters KB

Formation Sampled: BF

Sample produced by: DST # 4 Sampling point: DHS #78

DST Recovery  
 111.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1981/11/22 Received: 1981/11/24 Analyzed: 1982/01/12

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	2090.	47.344	90.9
K	20.	0.266	0.5
Ca	20.	0.520	1.0
Mg	18.	0.771	1.5

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	2050.	30.113	57.8
HCO3	1525.	13.016	25.0
SO4	543.	5.888	11.3
CO3	120.	2.083	4.0

Specific gravity	1.0040 @ 25. C	Refractive Index	1.33360 @ 25. C
PH	8.90 @ 25. C	Resistivity ohm/m	1.45000 @ 25. C
Hydrogen Sulfide Description:			
Organics Description :			
Calculated sodium:	2199.	Calculated TDS :	5700.
TDS by Evapor. @ 110 C:	6527.	TDS at Ignition :	4367.

Sample appearance:

PALE YELLOW FILTRATE RECOVERED FROM MUD WITH TRACE HYDROCARBONS. DHS REC'D @  
 KPA @23C, 1100MLS FLECKED OIL.

Remarks:

FE PRESENT. C82-11979-1 TOP RES: 2.24 OHMM @25C PALE YELLOW FILTRATE RECOVERED  
 FROM MUD. -2 MIDDLE RES: 1.90 OHM/M @25C PALE YELLOW FILTRATE RECOVERED FROM  
 MUD WITH TRACE HYDROCARBONS. -3 BOTTOM RES: 1.46 OHM/M @25C (SAME AS 2).

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78157 Chemistry number: 6  
 AGSWDB Hard copy number (HRDCPNO): 39644

CHEMICAL & GEOLOGICAL LAB LTD

Lab. Sample ID. E81-8729-3

Well identifier Well name KB elev. Gr. elev  
 0505040316000 ESSO PCP PEMBINA 16-3-50-4 781.30 777.30

Interval Sampled from: 1585.00 to: 1595.00 meters KB

Formation Sampled: GLAUCONITE

Sample produced by: DST # 6 Sampling point: COLUMN #3

DST Recovery 350.00 M MUD-CUT WATER  
 Date: Sampled: 1981/11/01 Received: 1981/11/05 Analyzed: 1981/11/24

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	18904.	46.955	822.3	Cl	30600.	49.287	863.1
K	220.	0.321	5.6	HCO3	602.	0.563	9.9
Ca	721.	2.054	36.0	SO4	132.	0.157	2.7
Mg	141.	0.663	11.6				

Specific gravity 1.0330 @ 25. C Refractive Index 1.34150 @ 25. C  
 PH 7.90 @ 22. C Resistivity ohm/m 0.14300 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 19041. Calculated TDS: 50931.  
 TDS by Evapor. @ 110 C: 55340. TDS at Ignition: 46180.

Sample appearance:

MUDDY SALT WATER.

Remarks:

FE NIL. E81-8729-1 COLUMN #1 RES: .187 OHM/M @25C MUD. -2 COLUMN #2 RES: .309 OHM/M @25C MUD.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78160 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39652

CHEMICAL & GEOLOGICAL LAB LTD

Lab. Sample ID. E79-17445

Well identifier Well name KB elev. Gr. elev  
 0505040816000 ANDEX ET PEMBINA 16-8-50-4 755.20 751.10

Interval Sampled from: 1598.00 to: 1620.00 meters KB

Formation Sampled: GLS SS.

Sample produced by: DST # 1 Sampling point: DSH

DST Recovery 22.00 M MUD  
 38.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1979/11/18 Received: 1979/11/28 Analyzed: 1979/12/18

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	4030.	47.685	175.3	Cl	5380.	41.280	151.8
K	58.	0.403	1.5	HCO3	898.	4.003	14.7
Ca	65.	0.882	3.2	SO4	687.	3.891	14.3
Mg	46.	1.030	3.8	CO3	91.	0.825	3.0

Specific gravity 1.0080 @ 25. C Refractive Index 1.33460 @ 25. C  
 PH 8.40 @ 20. C Resistivity ohm/m 0.56600 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 4064. Calculated TDS: 10775.  
 TDS by Evapor. @ 110 C: 12380. TDS at Ignition: 10550.

Sample appearance:

THE ANALYSIS DETERMINED ON SL. SALTY WATER EXTRACTED FROM OIL-FLECKED MUD.

Remarks:

FE NIL.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78156 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39637

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C82-14598-3

Well identifier Well name KB elev. Gr. elev  
 0505040216000 COLGAS ET AL PEMBINA 16-2-50-4 794.80 791.10

Interval Sampled from: 1623.00 to: 1630.00 meters KB

Formation Sampled: OSTRACOD

Sample produced by: DST # 1 Sampling point: BOTTOM

DST Recovery  
 95.00 M MUD  
 760.00 M SALT WATER  
 Date: Sampled: 1982/03/30 Received: 1982/03/31 Analyzed: 1982/04/27

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	21620.	42.602	940.4
K	188.	0.218	4.8
Ca	953.	2.154	47.6
Mg	345.	1.286	28.4

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	41400.	52.900	1167.7
HCO3	342.	0.254	5.6
SO4	16.	0.015	0.3
CO3	378.	0.571	12.6

Specific gravity 1.0480 @ 25. C Refractive Index 1.34270 @ 25. C  
 PH 8.50 @ 23. C Resistivity ohm/m 0.11500 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 25529. Calculated TDS : 68789.  
 TDS by Evapor. @ 110 C: 65150. TDS at Ignition : 61460.

Sample appearance:

CLEAR COLORLESS FILTRATE RECOVERED FROM MUDDY WATER.

Remarks:

FE PRESENT. C82-14598-1 TOP RES: 1.29 OHM/M @25C (SAME AS ABOVE). -2 MIDDLE RE  
 S: .118 OHM/M @25C (SAME AS ABOVE). -4 DHS #197 RES: .118 OHM/M @25C CLEAR COL  
 ORLESS FILTRATE WITH TRACE SEDIMENT.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78157 Chemistry number: 5  
 AGSWDB Hard copy number (HRDCPNO): 39643

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E81-8617

Well identifier Well name KB elev. Gr. elev  
 0505040316000 ESSO PCP PEMBINA 16-3-50-4 781.30 777.30

Interval Sampled from: 1585.00 to: 1595.00 meters KB

Formation Sampled: GLAUCONITE

Sample produced by: DST # 6 Sampling point:

DST Recovery  
 350.00 M MUD-CUT WATER  
 Date: Sampled: 1981/11/01 Received: 1981/11/04 Analyzed: 1981/11/20

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	15000.	46.367	652.5
K	213.	0.387	5.4
Ca	521.	1.848	26.0
Mg	238.	1.392	19.6

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	24600.	49.311	693.9
HCO3	427.	0.497	7.0
SO4	134.	0.198	2.8

Specific gravity 1.0280 @ 25. C Refractive Index 1.34030 @ 25. C  
 PH 8.00 @ 21. C Resistivity ohm/m 0.15800 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 15131. Calculated TDS : 40834.  
 TDS by Evapor. @ 110 C: 41060. TDS at Ignition : 37900.

Sample appearance:

MUDY SALT WATER RECOVERED FROM JOHNSTON DHS.

Remarks:

FE PRESENT.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78162 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): 39657

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. F75-1207-5

Well identifier Well name KB elev. Gr. elev  
 0505040907000 SKELLY ET AL A1 LINDALE 7-9-50-4 773.30 769.30

Interval Sampled from: 1594.10 to: 1600.20 meters KB

Formation Sampled: MANNVILLE

Sample produced by: DST # 3 Sampling point: TOOL

DST Recovery  
 30.50 M MUD  
 182.90 M SALT WATER

Date: Sampled: 1975/08/17 Received: 1975/08/21 Analyzed: 1975/08/22

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	18703.	47.374	813.5	Cl	29900.	49.112	843.4
Ca	681.	1.979	34.0	HCO3	781.	0.745	12.8
Mg	134.	0.642	11.0	SO4	122.	0.148	2.5

Specific gravity 1.0360 @ 16. C Refractive Index 1.34180 @ 25. C  
 PH 7.80 @ 23. C Resistivity ohm/m 0.13400 @ 25. C

Hydrogen Sulfide Description:

Organics Description :

Calculated sodium: 18708.

TDS by Evapor. @ 110 C: 52360.

Calculated TDS : 49929.  
 TDS at Ignition : 49310.

Sample appearance:

PALE YELLOW WATER WITH TRACE SEDIMENT.

Remarks:

FE PRESENT. F75-1207-1 TOP OF FLUID RES: .426 OHM/M @25C DARK RED WATER WITH 3  
 0% SEDIMENT. -2 270' ABOVE TOOL RES: .149 OHM/M @25C PALE YELLOW WATER WITH TR  
 ACE SEDIMENT. -3 90' ABOVE TOOL RES: .135 OHM/M @25C (SAME AS 2). -4 TOP OF TO  
 OL RES: .135 OHM/M @25C (SAME AS 2).

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78164 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39660

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E83-17271-2

Well identifier Well name KB elev. Gr. elev  
 0505041108000 ANDEX ET AL PEMBINA 8-11-50-4 778.30 773.60

Interval Sampled from: 1562.00 to: 1567.00 meters KB

Formation Sampled: GLAUCONITE

Sample produced by: DST # 3 Sampling point: DHS

DST Recovery  
 19.00 M MUD

Date: Sampled: 1983/09/28 Received: 1983/09/30 Analyzed: 1983/10/04

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	3770.	49.999	164.0	Cl	4790.	41.195	135.1
K	25.	0.195	0.6	HCO3	617.	3.083	10.1
Ca	35.	0.533	1.7	SO4	691.	4.387	14.4
Mg	2.	0.050	0.2	CO3	55.	0.559	1.8

Specific gravity 1.0060 @ 25. C Refractive Index 1.33450 @ 25. C  
 PH 8.60 @ 21. C Resistivity ohm/m 0.51600 @ 25. C

Hydrogen Sulfide Description:

Organics Description :

Calculated sodium: 3668.

TDS by Evapor. @ 110 C: 10340.

Calculated TDS : 9544.  
 TDS at Ignition : 8790.

Sample appearance:

LYNES DHS REC'D @ATM PRESSURE, 2L OF MUD. SLIGHTLY SALTY WATER EXTRACTED FROM M  
 UD.

Remarks:

FE TRACE. E83-17271-1 TOP OF TOOL RES: .775 OHM/M @25C MUD.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78160 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39653

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E79-17100-3

Well identifier Well name KB elev. Gr. elev  
 0505040816000 ANDEX ET PEMBINA 16-8-50-4 755.20 751.10

Interval Sampled from: 1598.00 to: 1620.00 meters KB

Formation Sampled: GLC

Sample produced by: DST # 1 Sampling point: TOP OF TOOL

DST Recovery  
 22.00 M MUD  
 38.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1979/11/18 Received: 1979/11/22 Analyzed: 1979/12/10

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	3982.	48.294	173.2	Cl	5174.	40.691	145.9
K	57.	0.406	1.5	HCO3	1042.	4.761	17.1
Ca	75.	1.043	3.7	SO4	523.	3.036	10.9
Mg	11.	0.252	0.9	CO3	163.	1.515	5.4

Specific gravity 1.0050 @ 25. C Refractive Index 1.33460 @ 25. C  
 PH 8.60 @ 22. C Resistivity ohm/m 0.59600 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 4016. Calculated TDS: 10475.  
 TDS by Evapor. @ 110 C: 11780. TDS at Ignition: 8840.

Sample appearance:

SLIGHTLY SALTY WATER EXTRACTED FROM OIL FLECKED MUD.

Remarks:

FE PRESENT. E79-17100-1 TOP OF FLUID RES OF FILT: 2.28 OHM/M @25C MUD. -2 MIDDLE RES OF FILT: 1.64 OHM/M @25C OIL FLECKED MUD.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78162 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39656

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. F75-1189-5

Well identifier Well name KB elev. Gr. elev  
 0505040907000 SKELLY ET AL A1 LINDALE 7-9-50-4 773.30 769.30

Interval Sampled from: 1585.57 to: 1605.08 meters KB

Formation Sampled: MANNVILLE

Sample produced by: DST # 2 Sampling point: TOP OF TOOL

DST Recovery  
 457.20 M SALT WATER  
 Date: Sampled: 1975/08/14 Received: 1975/08/19 Analyzed: 1975/08/20

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	21721.	47.388	944.8	Cl	34900.	49.373	984.4
Ca	841.	2.105	42.0	HCO3	659.	0.542	10.8
Mg	121.	0.499	10.0	SO4	89.	0.093	1.9

Specific gravity 1.0400 @ 16. C Refractive Index 1.34250 @ 25. C  
 PH 7.70 @ 21. C Resistivity ohm/m 0.12100 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 21730. Calculated TDS: 58005.  
 TDS by Evapor. @ 110 C: 59910. TDS at Ignition: 56290.

Sample appearance:

COLORLESS WATER WITH TRACE SEDIMENT.

Remarks:

FE MUCH. F75-1189-1 1600' ABOVE TOOL RES: .517 OHM/M @25C DARK RED WATER EXTRA CTED FROM MUD. -2 1250' ABOVE TOOL RES: .154 OHM/M @25C DARK RED WATER RECOVER ED FROM MUDDY WATER. -3 600' ABOVE TOOL RES: .121 OHM/M @25C COLORLESS WATER WITH TRACE SEDIMENT. -4 180' ABOVE TOOL RES: .121 OHM/M @25C (SAME AS 3).

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78174 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39666  
 CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E84-3104-4  
 Well identifier Well name KB elev. Gr. elev  
 0505041506000 PCP HIGHVALE 6-15-50-4 746.80 743.50  
 Interval Sampled from: 1578.00 to: 1600.00 meters KB  
 Formation Sampled: GLC

Sample produced by: DST # 1 Sampling point: DHS  
 DST Recovery  
 16.00 M GAS- AND OIL-CUT MUD  
 80.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1984/03/27 Received: 1984/03/30 Analyzed: 1984/05/01

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	12970.	45.773	564.2	Cl	21080.	48.242	594.6
K	204.	0.423	5.2	HCO3	969.	1.288	15.9
Ca	569.	2.304	28.4	SO4	494.	0.835	10.3
Mg	170.	1.135	14.0				

Specific gravity 1.0250 @ 25. C Refractive Index 1.33900 @ 25. C  
 PH 7.00 @ 22. C Resistivity ohm/m 0.19200 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 13298. Calculated TDS : 36087.  
 TDS by Evapor. @ 110 C: 36940. TDS at Ignition : 34240.

Sample appearance:  
 LYNES DHS REC'D @ATM PRESSURE, 2.3L OIL STAINED MUDDY WATER (2% OIL).

Remarks:  
 FE MUCH. E84-3104-1 TOP RES: 1.94 OHM/M @25C WATERY MUD. -2 19M RES: .448 OHM/M @25C SLIGHTLY OIL STAINED MUD. -3 TOP OF TOOL RES: .242 OHM/M @25C OIL STAIN ED MUDDY WATER (2% OIL).

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78174 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39667  
 CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E84-3105-4  
 Well identifier Well name KB elev. Gr. elev  
 0505041506000 PCP HIGHVALE 6-15-50-4 746.80 743.50  
 Interval Sampled from: 1572.00 to: 1577.00 meters KB  
 Formation Sampled: MANNVILLE

Sample produced by: DST # 2 Sampling point: DHS  
 DST Recovery  
 36.00 M GAS-CUT MUD  
 16.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1984/03/28 Received: 1984/03/30 Analyzed: 1984/04/27

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	6060.	43.244	263.6	Cl	9400.	43.497	265.1
K	82.	0.344	2.1	HCO3	1313.	3.530	21.5
Ca	521.	4.265	26.0	SO4	650.	2.220	13.5
Mg	214.	2.889	17.6	CO3	2.	0.011	0.1

Specific gravity 1.0130 @ 25. C Refractive Index 1.33600 @ 25. C  
 PH 8.40 @ 24. C Resistivity ohm/m 0.36700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 5901. Calculated TDS : 17334.  
 TDS by Evapor. @ 110 C: 18310. TDS at Ignition : 16810.

Sample appearance:  
 LYNES DHS REC'D @ATM PRESSURE, 1.6L OF OIL CUT MUDDY WATER (12% OIL).

Remarks:  
 FE PRESENT. E84-3105-1 TOP RES: 1.50 OHM/M @25C MUDDY WATER. -2 MIDDLE RES: 1.30 OHM/M @25C MUDDY WATER. -3 BOTTOM RES: .413 OHM/M @25C OIL CUT MUDDY WATER.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78170 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39662

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E88-9863-3

Well identifier Well name KB elev. Gr. elev  
 0505041214000 COLGAS DOME GENESEE 14-12-50-4 753.80 750.10

Interval Sampled from: 1560.00 to: 1562.00 meters KB  
 Interval Sampled from: 1563.00 to: 1564.00 meters KB

Sample produced by: Sampling point: METER RUN  
 Date: Sampled: 1988/06/08 Received: 1988/06/08 Analyzed: 1988/06/15

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	20165.	44.923	877.1	Cl	34050.	49.189	960.4
K	1199.	1.570	30.7	HCO3	1227.	1.030	20.1
Ca	801.	2.047	40.0	SO4	88.	0.094	1.8
Mg	272.	1.146	22.4				

Specific gravity 1.0370 @ 25. C Refractive Index 1.34220 @ 25. C  
 PH 8.00 @ 22. C Resistivity ohm/m 0.12700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 21153. Calculated TDS: 56967.  
 TDS by Evapor. @ 110 C: 59760. TDS at Ignition: 55660.

Sample appearance:

SAMPLE CONSISTED OF 73.95% OIL AND 46.05% SALT WATER.

Remarks:

FE PRES.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78173 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39665

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E84-6732

Well identifier Well name KB elev. Gr. elev  
 0505041408000 ANDEX ET AL PEMBINA 8-14-50-4 749.20 744.40

Interval Sampled from: 1563.00 to: 1567.30 meters KB

Formation Sampled: ELLERSLIE

Sample produced by: Flowing Sampling point: FLOWLINE  
 Date: Sampled: 1984/08/06 Received: 1984/08/10 Analyzed: 1984/08/16

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	22560.	37.020	981.3	Cl	47000.	50.012	1325.7
K	399.	0.385	10.2	HCO3	505.	0.312	8.3
Ca	5526.	10.403	275.7	SO4	344.	0.270	7.2
Mg	515.	1.599	42.4				

Specific gravity 1.0500 @ 25. C Refractive Index 1.34700 @ 25. C  
 PH 6.90 @ 24. C Resistivity ohm/m 0.09700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 23522. Calculated TDS: 77155.  
 TDS by Evapor. @ 110 C: 93460. TDS at Ignition: 75740.

Sample appearance:

SALT WATER WITH TRACE OIL (1% OIL).

Remarks:

FE TRACE.



-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78175 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): 39670

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7011-84-107

Well identifier Well name KB elev. Gr. elev  
 0505041516000 PCP HIGHVALE 16-15-50-4 738.00 733.30

Interval Sampled from: 1553.50 to: 1557.50 meters KB

Formation Sampled: GLC

Sample produced by: DST # 1 Sampling point: 30M

DST Recovery  
 10.00 M CLEAN OIL

Date: Sampled: 1984/02/11 Received: 1984/02/13 Analyzed: 1984/02/13

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	2800.	11.052	121.8	Cl	18136.	46.422	511.6
K	16850.	39.105	430.9	HCO3	1096.	1.630	18.0
Ca	160.	0.725	8.0	SO4	149.	0.282	3.1
Mg	105.	0.784	8.6				

Specific gravity 1.0250 @ 15. C Refractive Index 1.33730 @ 25. C  
 PH 8.00 @ 0. C Resistivity ohm/m 0.17000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 11863. Calculated TDS : 30952.

Remarks:

FE PRESENT. NACL EQUIV 38520.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78175 Chemistry number: 4  
 AGSWDB Hard copy number (HRDCPNO): 39671

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7011-84-107

Well identifier Well name KB elev. Gr. elev  
 0505041516000 PCP HIGHVALE 16-15-50-4 738.00 733.30

Interval Sampled from: 1553.50 to: 1557.50 meters KB

Formation Sampled: GLC

Sample produced by: DST # 1 Sampling point: 10M

DST Recovery  
 10.00 M CLEAN OIL

Date: Sampled: 1984/02/11 Received: 1984/02/13 Analyzed: 1984/02/13

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	2850.	11.379	124.0	Cl	18117.	46.905	511.0
K	16400.	38.497	419.4	HCO3	1065.	1.602	17.5
Ca	166.	0.760	8.3	SO4	160.	0.306	3.3
Mg	73.	0.551	6.0				

Specific gravity 1.0249 @ 15. C Refractive Index 1.33780 @ 25. C  
 PH 8.00 @ 0. C Resistivity ohm/m 0.17000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 11898. Calculated TDS : 30938.

Remarks:

FE TRACE. NACL EQUIV 38040.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78175 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39668

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7024-84-044

Well identifier Well name KB elev. Gr. elev  
 0505041516000 PCP HIGHVALE 16-15-50-4 738.00 733.30

Interval Sampled from: 1553.50 to: 1557.50 meters KB

Formation Sampled: ELESLIE

Sample produced by: Swabbing Sampling point:  
 Date: Sampled: 1984/02/24 Received: 1984/03/01 Analyzed: 1984/03/01

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	18700.	43.494	813.4	Cl	33512.	50.544	945.3
K	1850.	2.530	47.3	HCO3	925.	0.811	15.2
Ca	652.	1.740	32.5	SO4	45.	0.050	0.9
Mg	189.	0.832	15.6				

Specific gravity 1.0415 @ 15. C Refractive Index 1.34300 @ 25. C  
 PH 7.60 @ 0. C Resistivity ohm/m 0.13000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 20997. Calculated TDS : 55850.

Remarks:

FE PRESENT. NACL EQUIV 55335.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78175 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39669

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7011-84-107

Well identifier Well name KB elev. Gr. elev  
 0505041516000 PCP HIGHVALE 16-15-50-4 738.00 733.30

Interval Sampled from: 1553.50 to: 1557.50 meters KB

Formation Sampled: GLC

Sample produced by: DST # 1 Sampling point: BHS  
 DST Recovery  
 10.00 M CLEAN OIL

Date: Sampled: 1984/02/10 Received: 1984/02/13 Analyzed: 1984/02/13

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	5400.	19.435	234.9	Cl	20171.	47.075	569.0
K	13850.	29.307	354.2	HCO3	1840.	2.495	30.2
Ca	183.	0.756	9.1	SO4	221.	0.381	4.6
Mg	81.	0.551	6.7				

Specific gravity 1.0278 @ 15. C Refractive Index 1.33870 @ 25. C  
 PH 8.10 @ 0. C Resistivity ohm/m 0.16500 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 13517. Calculated TDS : 35078.

Remarks:

FE TRACE, NACL EQUIV 40368.

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 78186 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): 39683

AGAT ENGINEERING LTD Lab. Sample ID. 5479

Well identifier Well name KB elev. Gr. elev  
 0505042416000 COLGAS DOME HIGHVALE 16-24-50-4 732.80 729.10

Interval Sampled from: 1633.00 to: 1649.00 meters KB

Formation Sampled: ELLERSLIE

Sample produced by: DST # 1 Sampling point: TOP OF RECOVERY

DST Recovery  
 120.00 M MUD  
 20.00 M OIL-CUT MUD

Date: Sampled: 1983/06/23 Received: 1983/06/27 Analyzed: 1983/07/04

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	1770.	49.927	77.0	Cl	1920.	35.119	54.2
K	21.	0.340	0.5	HCO3	762.	8.098	12.5
Ca	10.	0.320	0.5	SO4	395.	5.333	8.2
Mg	4.	0.213	0.3	CO3	30.	0.648	1.0

Specific gravity 1.0030 @ 25. C  
 PH 9.26 @ 25. C Resistivity ohm/m 1.51000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 1725. Calculated TDS : 4459.  
 TDS by Evapor. @ 110 C: 4570. TDS at Ignition : 4170.  
 TDS by evaporation @ 180. C : 4540. mg/l

Sample appearance:

"30 MIN." API FILTRATE LOSS IS 11.65ML. WATER EXTRACTED FROM MUD.

Remarks:

THE SAMPLE CONTAINED IONS (INHIBITORS?) WHICH INTERFERED WITH THE ALKALINITY TEST. FE TRACE+

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 78186 Chemistry number: 4  
 AGSWDB Hard copy number (HRDCPNO): 39684

AGAT ENGINEERING LTD Lab. Sample ID. #5479

Well identifier Well name KB elev. Gr. elev  
 0505042416000 COLGAS DOME HIGHVALE 16-24-50-4 732.80 729.10

Interval Sampled from: 1633.00 to: 1649.00 meters KB

Formation Sampled: ELLERSLIE

Sample produced by: DST # 1 Sampling point: 10M ABOVE TOOL

DST Recovery  
 120.00 M MUD  
 20.00 M OIL-CUT MUD

Date: Sampled: 1983/06/23 Received: 1983/06/27 Analyzed: 1983/07/04

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	8720.	46.855	379.3	Cl	13800.	48.084	389.2
K	156.	0.493	4.0	HCO3	224.	0.453	3.7
Ca	359.	2.213	17.9	SO4	293.	0.754	6.1
Mg	113.	1.149	9.3				
Fe	0.10000	0.000	0.0				

Specific gravity 1.0170 @ 25. C  
 PH 8.08 @ 25. C Resistivity ohm/m 0.31000 @ 25. C  
 Calculated sodium: 8549. Calculated TDS : 23224.  
 TDS by Evapor. @ 110 C: 23400. TDS at Ignition : 22400.  
 TDS by evaporation @ 180. C : 23400. mg/l

Remarks:

SAMPLE CONTAINS IONS (INHIBITORS?) WHICH INTERFERED WITH THE ALKALINITY TEST.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78186 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39681

AGAT ENGINEERING LTD Lab. Sample ID. 5625

Well identifier Well name KB elev. Gr. elev  
 0505042416000 COLGAS DOME HIGHVALE 16-24-50-4 732.80 729.10

Interval Sampled from: 1555.00 to: 1557.50 meters KB

Formation Sampled: BF

Sample produced by: Sampling point: WELLHEAD  
 Date: Sampled: 1983/08/30 Received: 1983/08/31 Analyzed: 1983/04/07

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	23800.	44.732	1035.2	Cl	40500.	49.360	1142.4
K	963.	1.064	24.6	HCO3	607.	0.430	9.9
Ca	1460.	3.148	72.9	SO4	37.	0.033	0.8
Mg	317.	1.127	26.1				
Fe	68.	0.105	2.4				

Specific gravity 1.0470 @ 25. C  
 PH 6.87 @ 25. C Resistivity ohm/m 0.14000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 24237. Calculated TDS : 66849.  
 TDS by Evapor. @ 110 C: 68900. TDS at Ignition : 65200.  
 TDS by evaporation @ 180. C : 67700. mg/l

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78186 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39682

AGAT ENGINEERING LTD Lab. Sample ID. E4013

Well identifier Well name KB elev. Gr. elev  
 0505042416000 COLGAS DOME HIGHVALE 16-24-50-4 732.80 729.10

Interval Sampled from: 1565.00 to: 1566.00 meters KB

Formation Sampled: ELLERSLIE

Sample produced by: Sampling point: RIG TANK  
 Date: Sampled: 1983/08/04 Received: 1983/08/09 Analyzed: 1983/08/12

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	20200.	41.102	878.7	Cl	39100.	51.591	1102.9
K	1200.	1.436	30.7	HCO3	453.	0.347	7.4
Ca	1860.	4.342	92.8	SO4	201.	0.196	4.2
Mg	254.	0.978	20.9				
Fe	5.	0.009	0.2				

Specific gravity 1.0410 @ 25. C  
 PH 7.53 @ 25. C Resistivity ohm/m 0.11000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 23009. Calculated TDS : 64647.  
 TDS by Evapor. @ 110 C: 63500. TDS at Ignition : 59700.  
 TDS by evaporation @ 180. C : 62400. mg/l

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78197 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39703

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E82-11446

Well identifier Well name KB elev. Gr. elev  
 0505042914000 ANDEX ET AL HIGHVALE 14-29-50-4 758.50 754.40

Interval Sampled from: 1595.00 to: 1598.00 meters KB

Formation Sampled: BF

Sample produced by:  
 CATIONS

Sampling point:  
 ANIONS

ION	mg/l	%MEQ	MEQ/L
Na	24987.	43.454	1086.9
K	456.	0.466	11.7
Ca	1834.	3.659	91.5
Mg	734.	2.415	60.4

ION	mg/l	%MEQ	MEQ/L
Cl	44000.	49.620	1241.1
HCO3	500.	0.328	8.2
SO4	70.	0.058	1.5

Specific gravity 1.0500 @ 25. C  
 PH 5.70 @ 22. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 25264.  
 TDS by Evapor. @ 110 C: 73260.

Refractive Index 1.34510 @ 25. C  
 Resistivity ohm/m 0.11000 @ 25. C  
 Calculated TDS : 72148.  
 TDS at Ignition : 69160.

Sample appearance:

SALT WATER.

Remarks:

FE MUCH.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78197 Chemistry number: 4  
 AGSWDB Hard copy number (HRDCPNO): 39705

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID.,E82-741

Well identifier Well name KB elev. Gr. elev  
 0505042914000 ANDEX ET AL HIGHVALE 14-29-50-4 758.50 754.40

Interval Sampled from: 1595.00 to: 1598.00 meters KB

Formation Sampled: LOWER MANNVILLE

Sample produced by: Sampling point:  
 Date: Sampled: 1982/05/24 Received: 1982/05/25 Analyzed: 1982/05/28

CATIONS			
ION	mg/l	%MEQ	MEQ/L
Na	25950.	46.588	1128.8
K	186.	0.196	4.8
Ca	1682.	3.464	83.9
Mg	121.	0.411	10.0

ANIONS			
ION	mg/l	%MEQ	MEQ/L
Cl	42000.	48.895	1184.7
HCO3	583.	0.394	9.6
SO4	60.	0.052	1.2

Specific gravity 1.0470 @ 25. C  
 PH 7.40 @ 22. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 25327.  
 TDS by Evapor. @ 110 C: 80160.

Refractive Index 1.34450 @ 25. C  
 Resistivity ohm/m 0.10400 @ 25. C  
 Calculated TDS : 69477.  
 TDS at Ignition : 61660.

Remarks:

FE TRACE.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78194 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39696

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7011-7728

Well identifier Well name KB elev. Gr. elev  
 0505042810000 ANDEX ET AL HIGHVALE 10-28-50-4 758.60 754.70

Interval Sampled from: 1568.20 to: 1570.94 meters KB

Formation Sampled: LOWER MANNVILLE

Sample produced by: Sampling point: WELLHEAD  
 Date: Sampled: 1977/11/03 Received: 1977/11/07 Analyzed: 1977/11/28

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	25200.	47.017	1096.1	Cl	40843.	49.415	1152.0
K	177.	0.194	4.5	HCO3	810.	0.569	13.3
Ca	923.	1.976	46.1	SO4	7.	0.006	0.1
Mg	233.	0.822	19.2				

Specific gravity 1.0469 @ 16. C Refractive Index 1.34300 @ 24. C  
 PH 7.10 @ 0. C Resistivity ohm/m 0.09600 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 25296. Calculated TDS : 67700.

Remarks:  
 FE TRACE. NACL EQUIV 67786.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78197 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39702

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. #82-1653

Well identifier Well name KB elev. Gr. elev  
 0505042914000 ANDEX ET AL HIGHVALE 14-29-50-4 758.50 754.40

Interval Sampled from: 1595.00 to: 1598.00 meters KB

Formation Sampled: LOWER MANNVILLE

Sample produced by: Sampling point:  
 Date: Sampled: 1982/06/14 Received: 1982/06/16 Analyzed: 1982/06/25

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	25800.	47.259	1122.2	Cl	41500.	49.294	1170.6
K	441.	0.475	11.3	HCO3	695.	0.480	11.4
Ca	1001.	2.103	50.0	SO4	60.	0.053	1.2
Mg	97.	0.336	8.0				

Specific gravity 1.0390 @ 25. C Refractive Index 1.34500 @ 25. C  
 PH 7.80 @ 23. C Resistivity ohm/m 0.11000 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 25872. Calculated TDS : 68872.  
 TDS by Evapor. @ 110 C: 71040. TDS at Ignition : 65540.

Remarks:  
 FE PRESENT.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78201 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39711  
 CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E81-6151-3  
 Well identifier Well name KB elev. Gr. elev  
 0505043009000 ANDEX HIGHVALE 9-30-50-4 773.40 769.30

Interval Sampled from: 1620.00 to: 1626.00 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 1 Sampling point: BOTTOM

DST Recovery  
 1.90 M3 CLEAN OIL  
 0.20 M3 MUD-CUT OIL  
 0.10 M3 OIL-CUT SALT WATER

Date: Sampled: 1981/09/04 Received: 1981/09/09 Analyzed: 1981/09/22

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	27640.	44.490	1202.3	Cl	47400.	49.475	1337.0
K	658.	0.623	16.8	HCO3	539.	0.327	8.8
Ca	1634.	3.017	81.5	SO4	265.	0.204	5.5
Mg	612.	1.864	50.4				

Specific gravity 1.0520 @ 25. C Refractive Index 1.34600 @ 25. C  
 PH 7.20 @ 23. C Resistivity ohm/m 0.10400 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 28037. Calculated TDS: 78213.  
 TDS by Evapor. @ 110 C: 79380. TDS at Ignition: 74600.

Sample appearance:

MURKY SALT WATER WITH TRACE OF OIL.

Remarks:

FE NIL. E81-6151-1 TOP RES: .112 OHM/M @25C MUD, TRACE OF OIL.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78206 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39720  
 CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E84-1609-3  
 Well identifier Well name KB elev. Gr. elev  
 0505043116000 ANDEX ET AL HIGHVALE 16-31-50-4 762.00 757.90

Interval Sampled from: 1597.00 to: 1608.00 meters KB

Formation Sampled: BF

Sample produced by: DST # 1 Sampling point: BOTTOM

DST Recovery  
 20.00 M CLEAN OIL  
 84.00 M GAS- AND OIL-CUT MUD

Date: Sampled: 1984/02/15 Received: 1984/02/21 Analyzed: 1984/03/16

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	8690.	42.988	378.0	Cl	15210.	48.791	429.0
K	167.	0.486	4.3	HCO3	634.	1.182	10.4
Ca	440.	2.497	22.0	SO4	848.	2.008	17.7
Mg	219.	2.049	18.0				

Specific gravity 1.0160 @ 25. C Refractive Index 1.33750 @ 25. C  
 PH 7.90 @ 21. C Resistivity ohm/m 0.26800 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 9590. Calculated TDS: 26618.  
 TDS by Evapor. @ 110 C: 27070. TDS at Ignition: 24980.

Sample appearance:

70% OIL, 30% MUDDY SALTY WATER.

Remarks:

FE TRACE. E84-1609-1 TOP RES: .891 OHM/M @25C SLIGHTLY OIL STAINED MUD. -2 MID  
 DLE RES: .818 OHM/M @25C SLIGHTLY OIL STAINED MUD.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78197 Chemistry number: 5  
 AGSWDB Hard copy number (HRDCPNO): 39706

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E82-0706

Well identifier Well name KB elev. Gr. elev  
 0505042914000 ANDEX ET AL HIGHVALE 14-29-50-4 758.50 754.40

Interval Sampled from: 1595.00 to: 1598.00 meters KB

Formation Sampled: LOWER MANNVILLE

Sample produced by: Sampling point: PRODUCTION TANK  
 Date: Sampled: 1982/05/12 Received: 1982/05/13 Analyzed: 1982/05/18

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	26490.	46.302	1152.3
K	756.	0.777	19.3
Ca	1305.	2.617	65.1
Mg	253.	0.837	20.8

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	43100.	48.852	1215.7
HCO3	844.	0.556	13.8
SO4	72.	0.060	1.5

Specific gravity 1.0440 @ 25. C Refractive Index 1.34490 @ 25. C  
 PH 7.40 @ 23. C Resistivity ohm/m 0.10300 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 26328. Calculated TDS : 71473.  
 TDS by Evapor. @ 110 C: 72580. TDS at Ignition : 64980.

Remarks:

FE PRESENT.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78197 Chemistry number: 6  
 AGSWDB Hard copy number (HRDCPNO): 39707

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E81-9892-4

Well identifier Well name KB elev. Gr. elev  
 0505042914000 ANDEX ET AL HIGHVALE 14-29-50-4 758.50 754.40

Interval Sampled from: 1594.00 to: 1599.00 meters KB

Formation Sampled: LOWER MANNVILLE

Sample produced by: DST # 1 Sampling point: DHS  
 DST Recovery

2.00 M MUD  
 98.00 M OIL-CUT SALT WATER

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	23168.	46.867	1007.8
K	322.	0.383	8.2
Ca	773.	1.794	38.6
Mg	248.	0.949	20.4

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	37400.	49.061	1054.9
HCO3	1032.	0.787	16.9
SO4	165.	0.160	3.4

Specific gravity 1.0430 @ 25. C Refractive Index 1.34400 @ 25. C  
 PH 6.90 @ 21. C Resistivity ohm/m 0.11800 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 23366. Calculated TDS : 62460.  
 TDS by Evapor. @ 110 C: 63920. TDS at Ignition : 58500.

Sample appearance:

MURKY SALT WATER WITH TRACE OIL. QUINN DHS REC'D @700 KPA, GAS AND 1.2L MURKY SALT WATER WITH TRACE OF OIL.

Remarks:

FE PRESENT. E81-9892-2 56M RES: .288 OHM/M @25C MUDDY WATER OIL SCUM. -3 1M RE S: .121 OHM/M @25C MUDDY WATER TRACE OIL.



AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78222 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): 39746

CHEMEX LABS (ALBERTA) LTD. Lab. Sample ID. 85-0201-0908

Well identifier Well name KB elev. Gr. elev  
 0505050314000 CDNOXY ET AL PEMBINA 14-3-50-5 755.10 750.80

Interval Sampled from: 1666.50 to: 1668.50 meters KB  
 Interval Sampled from: 1669.50 to: 1671.50 meters KB

Formation Sampled: BF6440

Sample produced by: Sampling point: RIG TANK  
 CATIONS ANIONS

ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	24380.	45.753	1060.5	Cl	40000.	48.678	1128.3
K	1134.	1.251	29.0	HCO3	1160.	0.820	19.0
Ca	1110.	2.390	55.4	SO4	30.	0.027	0.6
Mg	300.	1.065	24.7				
Fe	10.	0.016	0.4				

Specific gravity 1.0510 @ 5. C Refractive Index 1.34510 @ 25. C  
 PH 7.30 @ 5. C Resistivity ohm/m 1.05000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 24551. Calculated TDS : 66562.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78230 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39750

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E74-2130-2

Well identifier Well name KB elev. Gr. elev  
 0505051107000 NORTERRA ET AL LINDALE 7-11-50-5 760.20 757.10

Interval Sampled from: 1602.64 to: 1619.71 meters KB

Formation Sampled: GLAUC

Sample produced by: DST # 1 Sampling point: MIDDLE

DST Recovery  
 18.30 M MUD  
 378.00 M GAS-CUT WATER  
 Date: Sampled: 1974/06/20 Received: 1974/06/27

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	26473.	47.306	1151.5	Cl	42850.	49.653	1208.6
Ca	991.	2.032	49.5	HCO3	476.	0.320	7.8
Mg	194.	0.656	16.0	SO4	39.	0.033	0.8

Specific gravity 1.0500 @ 16. C Refractive Index 1.34470 @ 25. C  
 PH 7.40 @ 26. C Resistivity ohm/m 0.15000 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 26483. Calculated TDS : 70791.  
 TDS by Evapor. @ 110 C: 76320. TDS at Ignition : 66340.

Sample appearance:

COLORLESS WATER RECOVERED FROM MUDDY WATER.

Remarks:

FE PRESENT. E74-2130-1 TOP RES: .239 OHM/M @25C YELLOW WATER RECOVERED FROM MUDDY WATER. -3 BOTTOM RES: .232 OHM/M @25C SAME AS 1.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78207 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39724

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E87-3775

Well identifier Well name KB elev. Gr. elev  
 0505043202000 ANDEX COLGAS HIGHVALE 2-32-50-4 773.20 769.10

Interval Sampled from: 1604.00 to: 1616.00 meters KB

Formation Sampled: BF 6440

Sample produced by: Sampling point:WELLHEAD  
 Date: Sampled: 1987/02/23 Received: 1987/02/24 Analyzed: 1987/03/04

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	27900.	44.889	1213.6	Cl	47800.	49.870	1348.3
K	379.	0.359	9.7	I	12.	0.004	0.1
Ca	1281.	2.364	63.9	HCO3	1237.	0.750	20.3
Mg	525.	1.598	43.2	SO4	216.	0.166	4.5
Fe	0.14000	0.000	0.0				

Other Determinations

Parameter	mg/l
barium	2.
boron	7.
strontium	146.

Specific gravity 1.0500 @ 25. C Refractive Index 1.34550 @ 25. C  
 PH 7.40 @ 21. C Resistivity ohm/m 0.10400 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 29108. Calculated TDS : 79550.

Sample appearance:

SAMPLE CONSISTED OF EMULSIFIED OIL AND SALT WATER.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78213 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39727

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID, E77-7628-3

Well identifier Well name KB elev. Gr. elev  
 0505043310000 ANDEX ET AL HIGHVALE 10-33-50-4 764.70 760.80

Interval Sampled from: 1575.82 to: 1583.44 meters KB

Formation Sampled: NORDEGG

Sample produced by: DST # 1 Sampling point:BOTTOM  
 DST Recovery

36.60 M CLEAN OIL  
 18.30 M OIL-CUT MUD  
 61.30 M GAS- AND OIL-CUT MUD

Date: Sampled: 1977/06/28 Received: 1977/07/05 Analyzed: 1977/08/09

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	7514.	45.537	326.8	Cl	12200.	47.944	344.1
Ca	377.	2.621	18.8	HCO3	603.	1.377	9.9
Mg	160.	1.834	13.2	SO4	237.	0.687	4.9

Specific gravity 1.0140 @ 16. C Refractive Index 1.33550 @ 25. C  
 PH 8.00 @ 25. C Resistivity ohm/m 0.41100 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 7517. Calculated TDS : 20788.  
 TDS by Evapor. @ 110 C: 22500. TDS at Ignition : 20345.

Sample appearance:

COLORLESS WATER RECOVERED FROM OIL CUT MUDDY WATER.

Remarks:

FE PRESENT. E77-7628-2 MIDDLE OIL CUT MUD, NO ANALYSIS.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78231 Chemistry number: 4  
 AGSWDB Hard copy number (HRDCPNO): 39754

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E79-14396-3

Well identifier Well name KB elev. Gr. elev  
 0505051205000 ANDEX ET AL HIGHVALE 5-12-50-5 772.80 768.70

Interval Sampled from: 1646.00 to: 1652.00 meters KB

Formation Sampled: OSTRACOD

Sample produced by: DST # 3 Sampling point: BHS #1513

DST Recovery  
 8.00 M MUD  
 14.00 M GAS-CUT MUD

Date: Sampled: 1979/09/13 Received: 1979/09/17 Analyzed: 1979/10/02

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	2477.	48.807	107.7	Cl	3115.	39.802	87.9
K	21.	0.243	0.5	HCO3	602.	4.469	9.9
Ca	27.	0.610	1.3	SO4	595.	5.612	12.4
Mg	9.	0.335	0.7	CO3	8.	0.121	0.3

Specific gravity 1.0040 @ 25. C Refractive Index 1.33320 @ 25. C  
 PH 8.40 @ 24. C Resistivity ohm/m 0.91900 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 2490. Calculated TDS : 6540.  
 TDS by Evapor. @ 110 C: 6915. TDS at Ignition : 6260.

Sample appearance:

QUINN DHS REC'D @ATM PRESSURE, 2100MLS SALTY MUDDY WATER.

Remarks:

FE TRACE. E79-14396-1 22M ABOVE TOOL RES OF FILT: 1.51 OHM/M @25C MUD. -2 1.52  
 4M ABOVE TOOL RES OF FILT: 1.27 OHM/M @25C MUD.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 78236 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39762

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E79-10739-5

Well identifier Well name KB elev. Gr. elev  
 0505052310000 ANDEX ET AL HIGHVALE 10-23-50-5 757.80 753.70

Interval Sampled from: 1631.50 to: 1642.00 meters KB

Formation Sampled: BF

Sample produced by: DST # 1 Sampling point: TOOL

DST Recovery  
 150.00 M CLEAN OIL  
 Date: Sampled: 1979/06/13 Received: 1979/06/18 Analyzed: 1979/06/29

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na+K	16968.			Cl	26750.	92.261	754.5
Ca	469.	2.862	23.4	HCO3	671.	1.345	11.0
Mg	199.	2.002	16.4	SO4	601.	1.530	12.5

Specific gravity 1.0300 @ 25. C Refractive Index 1.34050 @ 25. C  
 PH 7.80 @ 25. C Resistivity ohm/m 0.15100 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 16974. Calculated TDS : 45323.  
 TDS by Evapor. @ 110 C: 46200. TDS at Ignition : 43500.

Remarks:

FE NIL.

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 78231 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39751

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E79-15184-1

Well identifier Well name KB elev. Gr. elev  
 0505051205000 ANDEX ET AL HIGHVALE 5-12-50-5 772.80 768.70

Interval Sampled from: 1646.00 to: 1652.00 meters KB

Formation Sampled: OST

Sample produced by: Sampling point:#1  
 Date: Sampled: 1979/10/11 Received: 1979/10/12 Analyzed: 1979/10/16

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	25678.	45.573	1116.9	Cl	43000.	49.487	1212.9
K	361.	0.377	9.2	HCO3	705.	0.471	11.6
Ca	1490.	3.034	74.4	SO4	56.	0.048	1.2
Mg	301.	1.011	24.8				

Specific gravity 1.0480 @ 25. C Refractive Index 1.34500 @ 25. C  
 PH 6.90 @ 24. C Resistivity ohm/m 0.11900 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 25900. Calculated TDS : 71093.  
 TDS by Evapor. @ 110 C: 73620. TDS at Ignition : 67980.

Remarks:  
 FE PRESENT.

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 78231 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 39752

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E79-15184-2

Well identifier Well name KB elev. Gr. elev  
 0505051205000 ANDEX ET AL HIGHVALE 5-12-50-5 772.80 768.70

Interval Sampled from: 1646.00 to: 1652.00 meters KB

Formation Sampled: OST

Sample produced by: Sampling point:#2  
 Date: Sampled: 1979/10/11 Received: 1979/10/12 Analyzed: 1979/10/16

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	26282.	45.531	1143.2	Cl	44200.	49.654	1246.7
K	362.	0.369	9.3	HCO3	498.	0.325	8.2
Ca	1537.	3.055	76.7	SO4	33.	0.027	0.7
Mg	317.	1.039	26.1				

Specific gravity 1.0500 @ 25. C Refractive Index 1.34550 @ 25. C  
 PH 6.90 @ 24. C Resistivity ohm/m 0.11100 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 26505. Calculated TDS : 72837.  
 TDS by Evapor. @ 110 C: 75680. TDS at Ignition : 70580.

Remarks:  
 FE PRESENT.

B  
B  
C

-----  
AGSWDB WATER ANALYSIS REPORT  
-----

AGSWDB Well site identifier (SITID): 80735 Chemistry number: 1  
AGSWDB Hard copy number (HRDCPNO): 44545

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E80-13493-3

Well identifier Well name KB elev. Gr. elev  
0515040313000 ANDEX ET AL HIGHVALE 13-3-51-4 764.30 760.20

Interval Sampled from: 1578.00 to: 1586.00 meters KB

Formation Sampled: OSTRACODE

Sample produced by: DST # 1 Sampling point: 0 M ABO TOOL

DST Recovery  
948.00 M CLEAN OIL  
2.00 M SALT WATER

Date: Sampled: 1980/11/16 Received: 1980/11/25 Analyzed: 1980/12/16

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	1715.	48.734	74.6	Cl	1717.	31.639	48.4
K	18.	0.301	0.5	HCO3	1434.	15.353	23.5
Ca	21.	0.685	1.0	SO4	222.	3.020	4.6
Mg	5.	0.269	0.4				

Specific gravity	1.0030 @ 25. C	Refractive Index	1.33360 @ 25. C
PH	8.40 @ 21. C	Resistivity ohm/m	1.36000 @ 25. C
Hydrogen Sulfide Description:		Calculated TDS :	4397.
Organics Description :		TDS at Ignition :	4125.
Calculated sodium:	1726.		
TDS by Evapor. @ 110 C:	4530.		

Remarks:

FE NIL.

-----  
AGSWDB WATER ANALYSIS REPORT  
-----

AGSWDB Well site identifier (SITID): 80735 Chemistry number: 2  
AGSWDB Hard copy number (HRDCPNO): 44546

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E79-7331-3

Well identifier Well name KB elev. Gr. elev  
0515040313000 ANDEX ET AL HIGHVALE 13-3-51-4 764.30 760.20

Interval Sampled from: 1578.50 to: 1586.50 meters KB

Formation Sampled: OST, ELRSL

Sample produced by: DST # 1 Sampling point: TOP OF TOOL

DST Recovery  
948.00 M CLEAN OIL  
2.00 M SALT WATER

Date: Sampled: 1979/03/01 Received: 1979/03/05 Analyzed: 1979/03/16

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na+K	22699.			Cl	37200.	91.026	1049.3
Ca	1214.	5.255	60.6	HCO3	1139.	1.619	18.7
Mg	267.	1.906	22.0	SO4	107.	0.193	2.2

Specific gravity	1.0400 @ 25. C	Refractive Index	1.34360 @ 25. C
PH	7.70 @ 20. C	Resistivity ohm/m	0.11300 @ 25. C
Hydrogen Sulfide Description:		Calculated TDS :	62055.
Organics Description :		TDS at Ignition :	60400.
Calculated sodium:	22707.		
TDS by Evapor. @ 110 C:	64820.		

Sample appearance:

SAMPLE CONSISTED OF MUDDY WATER WITH A TRACE OF OIL.

Remarks:

FE PRES.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80744 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44549

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E83-14182-2

Well identifier Well name KB elev. Gr. elev  
 0515040506000 ANDEX ET AL HIGHVALE 6-5-51-4 761.50 757.40

Interval Sampled from: 1601.50 to: 1612.00 meters KB

Formation Sampled: BF 6440

Sample produced by: DST # 1 Sampling point: BOTTOM

DST Recovery  
 15.00 M MUD  
 10.00 M OIL-CUT MUD

Date: Sampled: 1983/06/20 Received: 1983/06/23 Analyzed: 1983/06/30

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	12210.	45.700	531.1	Cl	19640.	47.668	554.0
K	171.	0.376	4.4	HCO3	727.	1.025	11.9
Ca	701.	3.010	35.0	SO4	473.	0.847	9.8
Mg	194.	1.374	16.0				

Specific gravity 1.0230 @ 25. C Refractive Index 1.33860 @ 25. C  
 PH 8.00 @ 25. C Resistivity ohm/m 0.19800 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 12066. Calculated TDS : 33431.  
 TDS by Evapor. @ 110 C: 34250. TDS at Ignition : 31360.

Sample appearance:

THE ANALYSIS DETERMINED ON SALTY WATER EXTRACTED FROM OIL FLECKED WATERY MUD.

Remarks:

FE PRES. E83-14182-1: TOP RESIS: 1.23, MUD. -3; DHS RESIS: .200, LYNES UNITED  
 DHS #101 REC'D UNDER ATM. PRESSURE. RECOVERED FROM THE CHAMBER WAS 700 ML OIL  
 STAINED WATERY MUD. SUFFICIENT OIL COULD NOT BE REC'D FOR ANY ANALYSIS. BOTH R  
 ESIS OHM/M @ 25 C.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80748 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44552

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. C78-3515-3

Well identifier Well name KB elev. Gr. elev  
 0515040805000 ANDEX ET AL HIGHVALE 5-8-51-4 757.30 753.20

Interval Sampled from: 1927.56 to: 1935.18 meters KB

Formation Sampled: WINT.

Sample produced by: DST # 1 Sampling point: BOTTOM

DST Recovery  
 94.50 M MUD  
 72.90 M WATER  
 91.40 M SULPHUROUS SALT WATER

Date: Sampled: 1978/06/16 Received: 1978/08/14 Analyzed: 1978/08/23

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na+K	44176.			Cl	87400.	79.905	2465.2
Ca	8909.	14.409	444.6	HCO3	616.	0.327	10.1
Mg	1665.	4.441	137.0	SO4	1360.	0.918	28.3

Specific gravity 1.1010 @ 16. C Refractive Index 1.35740 @ 25. C  
 PH 8.00 @ 22. C Resistivity ohm/m 0.06900 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 44194. Calculated TDS : 143831.  
 TDS by Evapor. @ 110 C: 165500. TDS at Ignition : 137400.

Sample appearance:

PALE YELLOW FILTRATE REC'D FROM A SAMPLE CONTAINING APPROX. 10% SED. AND H2S.

Remarks:

FE TRACE.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138171 Chemistry number: 5  
 AGSWDB Hard copy number (HRDCPNO): -1730512

AGAT ENGINEERING LTD Lab. Sample ID. W2583

Well identifier Well name KB elev. Gr. elev  
 0495052614000 AMOCO PEMBINA 14-26-49-5 792.10 788.30

Interval Sampled from: 1738.00 to: 1743.00 meters KB

Formation Sampled: NORD

Sample produced by: Sampling point:SEPARATOR  
 Date: Sampled: 1985/12/24 Received: 1985/12/30 Analyzed: 1986/01/06

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	22200.	44.333	965.6	Cl	39300.	50.892	1108.5
K	343.	0.403	8.8	HCO3	1020.	0.767	16.7
Ca	1090.	2.497	54.4	SO4	135.	0.129	2.8
Mg	207.	0.782	17.0				
Fe	120.	0.197	4.3				

Specific gravity 1.0460 @ 0. C  
 PH 6.70 @ 25. C Resistivity ohm/m 0.12000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 24293. Calculated TDS : 65527.

Sample appearance:

REFRACTIVE INDEX, BR, BA, SR AND I=N.A. N.A.=NOT ANALYZED. NIL=0.0. TRC+ = LESS THAN 0.1. TRC\* = LESS THAN 0.001. SALINITY = 6.78%. N.D. = NOT DETECTED.  
 -----

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138171 Chemistry number: 6  
 AGSWDB Hard copy number (HRDCPNO): -1731101

AGAT ENGINEERING LTD Lab. Sample ID. W2608

Well identifier Well name KB elev. Gr. elev  
 0495052614000 AMOCO PEMBINA 14-26-49-5 792.10 788.30

Interval Sampled from: 1738.00 to: 1743.00 meters KB

Formation Sampled: NORD

Sample produced by: Sampling point:DOME BATTERY 16-  
 Date: Sampled: 1985/12/30 Received: 1986/01/06 Analyzed: 1986/01/07

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	3880.	46.910	168.8	Cl	5540.	43.434	156.3
K	27.	0.194	0.7	HCO3	1670.	7.607	27.4
Ca	61.	0.849	3.1	SO4	3.	0.016	0.1
Mg	30.	0.686	2.5	CO3	32.	0.292	1.0
Fe	1.	0.012	0.0				

Specific gravity 1.0080 @ 0. C  
 PH 8.20 @ 25. C Resistivity ohm/m 0.54000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 4120. Calculated TDS : 10607.

Sample appearance:

REFRACTIVE INDEX, BR, BA, SR AND I=N.A. N.A.=NOT ANALYZED. NIL=0.0. TRC+ = LESS THAN 0.1. TRC\* = LESS THAN 0.001. SALINITY = 0.99%. N.D. = NOT DETECTED.  
 -----

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138182 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1856306

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E86-1961-3

Well identifier Well name KB elev. Gr. elev  
 0495053514000 ENRON ET AL PEMBINA 14-35-49-5 763.10 758.30

Interval Sampled from: 1706.00 to: 1715.50 meters KB

Formation Sampled: JUR SYS

Sample produced by: DST # 1 Sampling point: TOP OF TOOL

DST Recovery  
 54.00 M GAS-CUT OIL  
 6.00 M WATER

Date: Sampled: 1986/12/04 Received: 1986/12/08 Analyzed: 1986/12/17

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	18200.	45.464	791.7
K	236.	0.347	6.0
Ca	685.	1.963	34.2
Mg	347.	1.640	28.6

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	30250.	49.001	853.2
HCO3	1076.	1.013	17.6
SO4	479.	0.573	10.0

Specific gravity 1.0310 @ 25. C Refractive Index 1.34100 @ 25. C  
 PH 7.40 @ 21. C Resistivity ohm/m 0.14200 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 18810. Calculated TDS: 51100.  
 TDS by Evapor. @ 110 C: 49940. TDS at Ignition: 47600.

Sample appearance:

ORGANICS: TRACE. SAMPLE CONSISTED OF VERY SLIGHTLY MUDDY SALT WATER.

Remarks:

Fe TRACE

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138182 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): -1856308

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E86-1962-2

Well identifier Well name KB elev. Gr. elev  
 0495053514000 ENRON ET AL PEMBINA 14-35-49-5 763.10 758.30

Interval Sampled from: 1698.00 to: 1705.00 meters KB

Formation Sampled: ELRS

Sample produced by: DST # 2 Sampling point: DOWNHOLE SAMPLER

DST Recovery  
 6.00 M GAS- AND OIL-CUT MUD

Date: Sampled: 1986/12/04 Received: 1986/12/08 Analyzed: 1986/12/17

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	24090.	45.743	1047.9
K	305.	0.341	7.8
Ca	969.	2.111	48.4
Mg	452.	1.624	37.2

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	40000.	49.252	1128.3
HCO3	996.	0.713	16.3
SO4	239.	0.217	5.0

Specific gravity 1.0440 @ 25. C Refractive Index 1.34360 @ 25. C  
 PH 7.10 @ 21. C Resistivity ohm/m 0.11300 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 24464. Calculated TDS: 66613.  
 TDS by Evapor. @ 110 C: 65380. TDS at Ignition: 62960.

Sample appearance:

ORGANICS: NIL. SAMPLE CONSISTED OF SALT WATER WITH A SLIGHT OIL SCUM.

Remarks:

Fe MUCH



AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138171 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1730508

AGAT ENGINEERING LTD Lab. Sample ID. WE6082A

Well identifier Well name KB elev. Gr. elev  
 0495052614000 AMOCO PEMBINA 14-26-49-5 792.10 788.30

Interval Sampled from: 1747.00 to: 1752.00 meters KB

Formation Sampled: BNFF

Sample produced by: DST # 1 Sampling point: BHS 197  
 DST Recovery

2.00 M MUD  
 Date: Sampled: 1985/11/02 Received: 1985/11/07 Analyzed: 1985/11/11

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	818.	51.309	35.6	Cl	362.	14.724	10.2
K	11.	0.406	0.3	HCO3	924.	21.837	15.1
Ca	5.	0.381	0.3	SO4	238.	7.146	5.0
Mg	1.	0.154	0.1	CO3	84.	4.037	2.8
Fe	0.10000	0.005	0.0				

Specific gravity 1.0020 @ 0. C  
 PH 9.90 @ 25. C Resistivity ohm/m 2.88000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 753. Calculated TDS : 1898.

Sample appearance:

BR, SR, BR, I & RE. INDEX=N.A.NIL=0.0. TRC+ = LESS THAN 0.1. TRC\* = LESS THAN 0.00  
 1. SALINITY:0.07%. THE "30 MIN" API MUD FILTRATE LOSS IS 10 MLS. THE ABOVE RES  
 ULTS PERTAIN TO THE WATER EXTRACTED FROM MUD. DST CHAMBER O.P. = 0 KPA RECOVER  
 Y = 1 LITRE MUD SALINITY = 0.07%

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138171 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): -1730509

AGAT ENGINEERING LTD Lab. Sample ID. WE6082B

Well identifier Well name KB elev. Gr. elev  
 0495052614000 AMOCO PEMBINA 14-26-49-5 792.10 788.30

Interval Sampled from: 1721.00 to: 1736.50 meters KB

Formation Sampled: BSL QTZ

Sample produced by: DST # 3 Sampling point: BHS 158  
 DST Recovery

13.50 M MUD  
 Date: Sampled: 1985/11/04 Received: 1985/11/07 Analyzed: 1985/11/11

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	802.	51.465	34.9	Cl	625.	26.008	17.6
K	9.	0.336	0.2	HCO3	476.	11.509	7.8
Ca	3.	0.221	0.1	SO4	164.	5.037	3.4
Mg	0.90000	0.109	0.1	CO3	108.	5.310	3.6
Fe	0.10000	0.005	0.0				

Specific gravity 1.0020 @ 0. C  
 PH 9.30 @ 25. C Resistivity ohm/m 2.67000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 741. Calculated TDS : 1876.

Sample appearance:

BR, BA, SR, REF. INDEX AND I=N.A.N.A.-NOT ANALYZED. TRC+ = LESS THAN 0.1. TRC\*  
 = LESS THAN 0.001. SALINITY = 0.12%. THE "30 MIN" API MUD FILTRATE LOSS IS 10  
 MLS. THE ABOVE RESULTS PERTAIN TO THE WATER EXTRACTED FROM THE MUD. DST CHAMBE  
 R O.P. = 0 KPA RECOVERY = 2 LITRES MUD. SALINITY = 0.12%

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138171 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): -1730510

AGAT ENGINEERING LTD Lab. Sample ID. W2593

Well identifier Well name KB elev. Gr. elev  
 0495052614000 AMOCO PEMBINA 14-26-49-5 792.10 788.30

Interval Sampled from: 1738.00 to: 1743.00 meters KB

Formation Sampled: NORD

Sample produced by: Sampling point: SIGHT GLASS  
 Date: Sampled: 1985/12/30 Received: 1985/12/31 Analyzed: 1986/01/06

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	26900.	45.182	1170.1	Cl	46500.	50.647	1311.6
K	377.	0.372	9.6	HCO3	793.	0.502	13.0
Ca	1240.	2.389	61.9	SO4	144.	0.116	3.0
Mg	238.	0.756	19.6				
Fe	26.	0.036	0.9				

Specific gravity 1.0470 @ 0. C  
 PH 6.50 @ 25. C Resistivity ohm/m 0.11000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 28651. Calculated TDS : 77163.

Sample appearance:

BR, BA, SR, REF. INDEX AND I=N.A. N.A.=NOT ANALYZED. NIL=0.0. TRC+ = LESS THAN 0  
 .1. TRC\* = LESS THAN 0.001. SALINITY = 8.02%. N.D. = NOT DETECTED.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138171 Chemistry number: 4  
 AGSWDB Hard copy number (HRDCPNO): -1730511

AGAT ENGINEERING LTD Lab. Sample ID. W2573

Well identifier Well name KB elev. Gr. elev  
 0495052614000 AMOCO PEMBINA 14-26-49-5 792.10 788.30

Interval Sampled from: 1738.00 to: 1743.00 meters KB

Formation Sampled: NORD

Sample produced by: Sampling point: RIG TANK  
 Date: Sampled: 1985/12/22 Received: 1985/12/27 Analyzed: 1986/01/02

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	20000.	45.363	870.0	Cl	34200.	50.302	964.7
K	269.	0.359	6.9	HCO3	888.	0.759	14.6
Ca	898.	2.337	44.8	SO4	157.	0.170	3.3
Mg	165.	0.708	13.6				
Fe	1.0000	0.002	0.0				

Specific gravity 1.0380 @ 0. C  
 PH 7.60 @ 25. C Resistivity ohm/m 0.12000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 21246. Calculated TDS : 57103.

Sample appearance:

BR, BA, SR, REFRACTIVE INDEX AND I=N.A. N.A.=NOT ANALYZED. NIL=0.0. TRC+ = LESS  
 THAN 0.1. TRC\* = LESS THAN 0.001. SALINITY = 5.94%. N.D. = NOT DETECTED.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138155 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1843306

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E86-1499-4

Well identifier Well name KB elev. Gr. elev  
 0495043406000 ANDEX ET AL PEMBINA 6-34-49-4 785.10 780.30

Interval Sampled from: 1645.00 to: 1659.00 meters KB

Formation Sampled: BNFF

Sample produced by: DST # 1 Sampling point: DOWNHOLE SAMPLER

DST Recovery  
 23.00 M MUD  
 25.00 M GAS- AND OIL-CUT MUD  
 32.00 M BRACKISH WATER-CUT MUD

Date: Sampled: 1986/11/21 Received: 1986/11/25 Analyzed: 1986/12/04

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	12320.	45.410	535.9	Cl	20200.	48.281	569.8
K	167.	0.362	4.3	HCO3	615.	0.854	10.1
Ca	573.	2.423	28.6	SO4	506.	0.893	10.5
Mg	255.	1.778	21.0				

Specific gravity 1.0220 @ 25. C Refractive Index 1.33860 @ 25. C  
 PH 7.40 @ 23. C Resistivity ohm/m 0.19900 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 12434. Calculated TDS : 34271.  
 TDS by Evapor. @ 110 C: 33680. TDS at Ignition : 32590.

Sample appearance:

ORGANICS: MUCH. A MCALLISTER PETRO IND. DOWNHOLE SAMPLER WAS RECEIVED AT 689 K PA. IT CONTAINED GAS AND 1300 ML OF OIL STAINED WATERY MUD. ANALYSIS PERFORMED ON SALT WATER EXTRACTED FROM THE MUD.

Remarks:

Fe MUCH [E86-1499-1]:SAMPLED FROM TOP|RESISTIVITY: 3.33 OHM METERS @ 25 C.|SAM  
 PLE CONSISTED OF MUD.|[E86-1499-2]:SAMPLED FROM MIDDLE.|RESISTIVITY:0.448 OHM  
 METERS @ 25 C.|[SAMPLE CONSISTED OF MUD.|[E86-1499-3]:SAMPLED FROM TOP OF TOOL|  
 RESISTIVITY:0.225 OHM METERS @ 25 C.|SAMPLE CONSISTED OF SLIGHTLY OIL FLECKED  
 WATERY MUD.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138155 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): -1843308

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E86-1500-1

Well identifier Well name KB elev. Gr. elev  
 0495043406000 ANDEX ET AL PEMBINA 6-34-49-4 785.10 780.30

Interval Sampled from: 1640.00 to: 1644.00 meters KB

Formation Sampled: NORD

Sample produced by: DST # 2 Sampling point: TOP OF TOOL

DST Recovery  
 10.00 M OIL-CUT MUD  
 Date: Sampled: 1986/11/21 Received: 1986/11/25 Analyzed: 1986/12/04

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	4810.	45.080	209.2	Cl	7800.	47.404	220.0
K	60.	0.331	1.5	HCO3	730.	2.578	12.0
Ca	146.	1.570	7.3	SO4	432.	1.938	9.0
Mg	62.	1.099	5.1				

Specific gravity 1.0040 @ 25. C Refractive Index 1.33500 @ 25. C  
 PH 8.20 @ 23. C Resistivity ohm/m 0.47500 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 5255. Calculated TDS : 14054.  
 TDS by Evapor. @ 110 C: 13590. TDS at Ignition : 12940.

Sample appearance:

ORGANICS: MUCH. SAMPLE ANALYSED CONSISTED OF SLIGHTLY SALTY WATER EXTRACTED FROM SLIGHTLY OIL FLECKED MUD.

Remarks:

Fe TRACE

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138155 Chemistry number: 4  
 AGSWDB Hard copy number (HRDCPNO): -1843311

CHEMICAL & GEOLOGICAL LAB LTD

Lab. Sample ID. E86-1496-4

Well identifier Well name KB elev. Gr. elev  
 0495043406000 ANDEX ET AL PEMBINA 6-34-49-4 785.10 780.30

Interval Sampled from: 1639.20 to: 1644.00 meters KB

Formation Sampled: NORD

Sample produced by: DST # 4 Sampling point: DOWN HOLE SAMPLE

DST Recovery

40.00 M GAS- AND OIL-CUT MUD

Date: Sampled: 1986/11/23 Received: 1986/11/25 Analyzed: 1986/11/28

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	4490.	44.373	195.3
K	58.	0.337	1.5
Ca	218.	2.472	10.9
Mg	79.	1.477	6.5

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	7090.	45.436	200.0
HCO3	839.	3.124	13.8
SO4	588.	2.782	12.2

Specific gravity 1.0090 @ 25. C  
 PH 8.20 @ 23. C

Refractive Index 1.33550 @ 25. C  
 Resistivity ohm/m 0.47700 @ 25. C

Hydrogen Sulfide Description:

Organics Description:

Calculated sodium: 4796.

Calculated TDS: 13184.  
 TDS at Ignition: 12470.

TDS by Evapor. @ 110 C: 13260.

Sample appearance:

BAKER OIL TOOLS DOWNHOLE SAMPLER 119 RECEIVED UNDER ATMOSPHERIC PRESSURE. CONTAINED IN THE CHAMBER WAS 500 ML OF WATERY MUD AND OIL (40% OIL). ANALYSIS DETERMINED ON SLIGHTLY SALTY WATER EXTRACTED FROM THE MUD.

Remarks:

Fe TRACE [E86-1496-1]: SAMPLED FROM TOP | RESISTIVITY: 2.54 OHM METER @ 25 C. | SAMPLE CONSISTED OF SLIGHTLY OIL STAINED MUD. | [E86-1496-2]: SAMPLED FROM MIDDLE | RESISTIVITY: 2.26 OHM METERS @ 25 C. | SAMPLE CONSISTED OF SLIGHTLY OIL STAINED MUD. | [E86-1496-3]: SAMPLED FROM BOTTOM | RESISTIVITY: 0.976 OHM METERS @ 25 C. | SAMPLE CONSISTED OF OIL STAINED MUD. (12% OIL).

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138170 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1876511

GEOTECH Analytical

Lab. Sample ID. 5212-W1

Well identifier Well name KB elev. Gr. elev  
 0495052411000 COLGAS PEMBINA 11-24-49-5 804.40 799.70

Interval Sampled from: 1742.00 to: 1754.00 meters KB

Formation Sampled: BNFF

Sample produced by: DST # 4

Sampling point: TOP OF TOOL

DST Recovery

25.00 M MUD

300.00 M MUD-CUT WATER

Date: Sampled: 1987/02/27 Received: 1987/03/03 Analyzed: 1987/03/05

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	930.	48.421	40.5
K	13.	0.389	0.3
Ca	4.	0.245	0.2
Mg	0.41000	0.040	0.0
Fe	3.	0.107	0.1

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	343.	11.581	9.7
HCO3	616.	12.084	10.1
SO4	863.	21.508	18.0
CO3	141.	5.625	4.7

Other Determinations

Parameter	mg/l
barium	0.24000
boron	0.65000
strontium	0.34000

PH 8.20 @ 25. C  
 Calculated sodium: 970.

Refractive Index 1.34500 @ 0. C  
 Resistivity ohm/m 2.70300 @ 25. C  
 Calculated TDS: 2625.

Sample appearance:

B-0.649. I-<1.00 CATIONS/ANIONS: 0.97.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 82310 Chemistry number: 6  
 AGSWDB Hard copy number (HRDCPNO): 43888

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. 8327-9

Well identifier Well name KB elev. Gr. elev  
 0525051816000 IMP CDN-SUP TOMAHAWK 16-18-52-5 799.80 795.20

Interval Sampled from: 1976.32 to: 1988.52 meters KB

Formation Sampled: GRAMINIA

Sample produced by: DST # 9 Sampling point: DST #9  
 DST Recovery

103.60 M MUD-CUT SULPHUROUS SALT WATER Analyzed: 1956/06/14  
 Date: Sampled: 1956/04/14

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Ca	10603.	18.558	529.1	Cl	79440.	78.595	2240.7
Mg	560.	1.616	46.1	HCO3	150.	0.086	2.5
				SO4	1522.	1.112	31.7
				CO3	28.	0.033	0.9

Specific gravity 1.0900 @ 16. C  
 PH 7.70 @ 0. C  
 Organics Description :  
 Calculated sodium: 39102. Resistivity ohm/m 0.07900 @ 20. C  
 Calculated TDS : 131329.  
 TDS at Ignition : 129150.

Remarks:

PRI. SAL. 74.72, SECOND. SAL. 25.14, SECOND. ALKALI. .14, CL SAL. 98.60, SO4 S AL. 1.40  
 -----

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 82310 Chemistry number: 7  
 AGSWDB Hard copy number (HRDCPNO): 43889

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. 8327-10

Well identifier Well name KB elev. Gr. elev  
 0525051816000 IMP CDN-SUP TOMAHAWK 16-18-52-5 799.80 795.20

Interval Sampled from: 2694.43 to: 2708.15 meters KB

Formation Sampled: ELK POINT

Sample produced by: DST # 10 Sampling point: DST #10  
 DST Recovery

246.90 M SALT WATER Analyzed: 1956/06/14  
 Date: Sampled: 1956/05/19

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Ca	26277.	24.200	1311.2	Cl	140013.	72.887	3949.3
Mg	1680.	2.551	138.2	HCO3	110.	0.033	1.8
				SO4	811.	0.312	16.9
				CO3	28.	0.017	0.9

Specific gravity 1.1520 @ 16. C  
 PH 7.30 @ 0. C  
 Organics Description :  
 Calculated sodium: 57930. Resistivity ohm/m 0.05570 @ 20. C  
 Calculated TDS : 226793.  
 TDS at Ignition : 221460.

Remarks:

PRI. SAL. 63.48, SECOND. SAL. 36.44, SECOND. ALKALI. .08, CL SAL. 99.58, SO4 S AL. .42  
 -----

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 82310 Chemistry number: 8  
 AGSWDB Hard copy number (HRDCPNO): 43890

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. 8327-11

Well identifier Well name KB elev. Gr. elev  
 0525051816000 IMP CDN-SUP TOMAHAWK 16-18-52-5 799.80 795.20

Interval Sampled from: 2753.87 to: 2769.11 meters KB

Formation Sampled: ELK POINT

Sample produced by: DST # 11 Sampling point: DST #11

DST Recovery  
 91.40 M MUD-CUT SALT WATER  
 CATIONS

ION	mg/l	%MEQ	MEQ/L
Ca	26277.	24.230	1311.2
Mg	1540.	2.342	126.7

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	140013.	72.978	3949.3
HCO3	138.	0.042	2.3
SO4	1016.	0.391	21.2
CO3	28.	0.017	0.9

Specific gravity 1.1520 @ 16. C  
 PH 7.90 @ 0. C  
 Organics Description :  
 Calculated sodium: 58304.

Resistivity ohm/m 0.05550 @ 20. C  
 Calculated TDS : 227246.  
 TDS at Ignition : 220960.

Remarks:

PRI. SAL. 63.80, SECOND. SAL. 36.12, SECOND. ALKALI. .08, CL SAL. 99.46, SO4 S AL. .54

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 82314 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 43891

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7021-31875

Well identifier Well name KB elev. Gr. elev  
 0525052105000 AMOCO A-1 TOMAHAWK 5-21-52-5 786.10 782.10

Interval Sampled from: 1622.15 to: 1631.59 meters KB

Formation Sampled: BASAL QUARTZ

Sample produced by: DST # 2 Sampling point: BOTTOM

DST Recovery  
 45.70 M WATER-CUT MUD  
 Date: Sampled: 1973/12/07 Received: 1973/12/18 Analyzed: 1973/12/23

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na+K	9377.		
Ca	356.	3.943	17.8
Mg	44.	0.804	3.6

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	14695.	91.993	414.5
HCO3	781.	2.841	12.8
SO4	91.	0.421	1.9

Specific gravity 1.0175 @ 16. C  
 PH 7.50 @ 0. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 9376.

Refractive Index 1.33610 @ 24. C  
 Resistivity ohm/m 0.24900 @ 25. C  
 Calculated TDS : 24946.

Remarks:

FE TRACE.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 82307 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 43878

CHEMICAL & GEOLOGICAL LAB LTD

Lab. Sample ID. C81-6414-4

Well identifier Well name KB elev. Gr. elev  
 0525051801000 COLGAS TOMAHAWK 1-18-52-5 802.90 799.20

Interval Sampled from: 1640.00 to: 1650.00 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 1 Sampling point: BOTTOM

DST Recovery 156.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1981/01/13 Received: 1981/01/19 Analyzed: 1981/01/30

CATIONS

ANIONS

ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	9146.	44.610	397.8	Cl	15130.	47.855	426.8
K	164.	0.470	4.2	HCO3	769.	1.413	12.6
Ca	561.	3.139	28.0	SO4	258.	0.602	5.4
Mg	207.	1.910	17.0				

Specific gravity 1.0160 @ 25. C Refractive Index 1.33760 @ 25. C  
 PH 7.50 @ 25. C Resistivity ohm/m 0.25400 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 9190. Calculated TDS: 25724.  
 TDS by Evapor. @ 110 C: 30410. TDS at Ignition: 22140.

Sample appearance:

PALE YELLOW FILTRATE REC'D FROM A SAMPLE CONTAINING APPROX. 50% SED. AND A LAYER OF HYDRO.

Remarks:

FE TRACE. C81-6414-2 TOP RESIS: 1.56, PALE YELLOW FILTRATE REC'D FROM THE WATER PORTION OF THE SAMPLE. -3: MID RESIS: .473, SAME AS -2. BOTH RESIS OHM/M @ 25 C.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 82308 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 43879

CHEMICAL & GEOLOGICAL LAB LTD

Lab. Sample ID. E82-10675-2

Well identifier Well name KB elev. Gr. elev  
 0525051806000 COLGAS ET AL SUNDANCE 6-18-52-5 820.90 816.50

Interval Sampled from: 1656.00 to: 1666.00 meters KB

Formation Sampled: NORD 4440

Sample produced by: DST # 1 Sampling point: MIDDLE

DST Recovery 60.00 M OIL-CUT MUD  
 Date: Sampled: 1982/12/29 Received: 1982/01/05 Analyzed: 1982/01/26

CATIONS

ANIONS

ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	1332.	46.782	57.9	Cl	1475.	33.593	41.6
K	14.	0.289	0.4	HCO3	689.	9.117	11.3
Ca	36.	1.450	1.8	SO4	377.	6.338	7.8
Mg	22.	1.462	1.8	CO3	36.	0.969	1.2

Specific gravity 1.0030 @ 25. C Refractive Index 1.33410 @ 25. C  
 PH 9.10 @ 19. C Resistivity ohm/m 1.78000 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 1341. Calculated TDS: 3626.  
 TDS by Evapor. @ 110 C: 4040. TDS at Ignition: 2660.

Sample appearance:

THE SAMPLE CONSISTED OF MUDDY WATER WITH A TRACE OF OIL.

Remarks:

FE PRES.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 82310 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 43884

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. 8327-2

Well identifier Well name KB elev. Gr. elev  
 0525051816000 IMP CDN-SUP TOMAHAWK 16-18-52-5 799.80 795.20

Interval Sampled from: 1565.45 to: 1576.12 meters KB

Formation Sampled: BLAIRMORE

Sample produced by: DST # 3 Sampling point:

DST Recovery  
 61.00 M MUD  
 102.10 M SALT WATER

Date: Sampled: 1956/03/21

Analyzed: 1956/06/14

CATIONS

ION	mg/l	%MEQ	MEQ/L
Ca	318.	2.298	15.9
Mg	132.	1.573	10.9

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	22094.	90.246	623.2
HCO3	615.	1.460	10.1
SO4	257.	0.775	5.4
CO3	756.	3.649	25.2

Specific gravity 1.0270 @ 16. C  
 PH 11.40 @ 0. C  
 Organics Description :  
 Calculated sodium: 14648.

Resistivity ohm/m 0.18900 @ 20. C  
 Calculated TDS : 38507.  
 TDS at Ignition : 37290.

Remarks:

PRI. SAL. 94.68, PRI. ALKALI. 1.30, SECOND. ALKALI. 4.02, CL SAL. 99.16, SO4 S AL. .84

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 82310 Chemistry number: 5  
 AGSWDB Hard copy number (HRDCPNO): 43887

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. #327-8

Well identifier Well name KB elev. Gr. elev  
 0525051816000 IMP CDN-SUP TOMAHAWK 16-18-52-5 799.80 795.20

Interval Sampled from: 1822.70 to: 1836.42 meters KB

Formation Sampled: WABAMUN

Sample produced by: DST # 8 Sampling point: DST #8

DST Recovery  
 804.70 M MUD-CUT SULPHUROUS SALT WATER

Date: Sampled: 1956/04/09

Analyzed: 1956/06/14

CATIONS

ION	mg/l	%MEQ	MEQ/L
Ca	12678.	17.423	632.6
Mg	1820.	4.124	149.8

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	100293.	77.908	2828.9
HCO3	315.	0.142	5.2
SO4	551.	0.316	11.5
CO3	95.	0.087	3.2

Specific gravity 1.1140 @ 16. C  
 PH 6.60 @ 0. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 47511.

Resistivity ohm/m 0.06800 @ 20. C  
 Calculated TDS : 163103.  
 TDS at Ignition : 158120.

Remarks:

PRI. SAL. 72.54, SECOND. SAL. 27.16, SECOND. ALKALI. .30, CL SAL. 99.60, SO4 S AL. .40



-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80828 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 44632

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E77-8828-2

Well identifier Well name KB elev. Gr. elev  
 0515043411000 COLGAS ET AL HIGHVALE 11-34-51-4 789.70 785.80

Interval Sampled from: 1542.90 to: 1555.09 meters KB

Formation Sampled: NORDEGG

Sample produced by: DST # 3 Sampling point: MIDDLE

DST Recovery  
 97.50 M GAS-CUT MUD

Date: Sampled: 1977/08/09 Received: 1977/08/12 Analyzed: 1977/08/23

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	6092.	45.136	265.0	Cl	9780.	46.987	275.9
Ca	275.	2.337	13.7	HCO3	725.	2.024	11.9
Mg	180.	2.523	14.8	SO4	280.	0.993	5.8

Specific gravity 1.0140 @ 16. C Refractive Index 1.33650 @ 25. C  
 PH 7.40 @ 24. C Resistivity ohm/m 0.38700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 6094. Calculated TDS : 16965.  
 TDS by Evapor. @ 110 C: 18305. TDS at Ignition : 15889.

Sample appearance:

THE SAMPLE CONSISTED OF MUDDY WATER.

Remarks:

FE PRES. E77-8828-1 TOP RESIS: .396, MUDDY WATER. -3 BOTTOM RESIS: .479, MUD S  
 AMPLE. RESIS OHM/M @ 25 C.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80828 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): 44633

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E77-8829

Well identifier Well name KB elev. Gr. elev  
 0515043411000 COLGAS ET AL HIGHVALE 11-34-51-4 789.70 785.80

Interval Sampled from: 1555.09 to: 1597.15 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 5 Sampling point: MIDDLE

DST Recovery  
 1365.50 M SALT WATER

Date: Sampled: 1977/08/11 Received: 1977/08/12 Analyzed: 1977/08/23

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	27368.	40.651	1190.4	Cl	51200.	49.315	1444.2
Ca	3606.	6.144	179.9	HCO3	1079.	0.604	17.7
Mg	1139.	3.200	93.7	SO4	121.	0.086	2.5

Specific gravity 1.0600 @ 16. C Refractive Index 1.34730 @ 25. C  
 PH 6.10 @ 24. C Resistivity ohm/m 0.10500 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 27378. Calculated TDS : 83974.  
 TDS by Evapor. @ 110 C: 91300. TDS at Ignition : 81380.

Sample appearance:

THE SAMPLE CONSISTED OF COLORLESS WATER WITH A LAYER OF MUD.

Remarks:

FE MUCH.

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 82303 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 43872

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E82-13879

Well identifier Well name KB elev. Gr. elev  
 0525050716000 PCP TOMAHAWK 16-7-52-5 799.80 796.00

Interval Sampled from: 1650.00 to: 1657.00 meters KB

Formation Sampled: NORDEGG

Sample produced by: DST # 1 Sampling point: DHS

DST Recovery  
 100.00 M GAS- AND OIL-CUT MUD

Date: Sampled: 1982/03/01 Received: 1982/03/05 Analyzed: 1982/03/26

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	23783.	41.715	1034.5
K	305.	0.315	7.8
Ca	2571.	5.173	128.3
Mg	841.	2.791	69.2

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	43600.	49.591	1229.8
HCO3	325.	0.215	5.3
SO4	239.	0.201	5.0

Specific gravity 1.0480 @ 25. C Refractive Index 1.34590 @ 25. C  
 PH 6.10 @ 24. C Resistivity ohm/m 0.10900 @ 25. C

Hydrogen Sulfide Description:

Organics Description:

Calculated sodium: 23972.

TDS by Evapor. @ 110 C: 76260.

Calculated TDS : 71383.

TDS at Ignition : 68400.

Sample appearance:

A LYNES UNITED DHS #89 REC'D AT ATM. PRESSURE. IT CONTAINED 2.3 L OF WATER ONLY.

Remarks:

FE PRESENT.

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 82303 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 43873

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E82-13618-3

Well identifier Well name KB elev. Gr. elev  
 0525050716000 PCP TOMAHAWK 16-7-52-5 799.80 796.00

Interval Sampled from: 1650.00 to: 1657.00 meters KB

Formation Sampled: NORDEGG

Sample produced by: DST # 1 Sampling point: BOTTOM

DST Recovery  
 100.00 M GAS- AND OIL-CUT MUD

Date: Sampled: 1982/03/09 Received: 1982/03/11 Analyzed: 1982/03/25

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	21263.	41.254	924.9
K	317.	0.362	8.1
Ca	2643.	5.883	131.9
Mg	680.	2.496	56.0

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	39300.	49.444	1108.5
HCO3	356.	0.260	5.8
SO4	325.	0.302	6.8

Specific gravity 1.0460 @ 25. C Refractive Index 1.34450 @ 25. C  
 PH 7.80 @ 23. C Resistivity ohm/m 0.13000 @ 25. C

Hydrogen Sulfide Description:

Organics Description:

Calculated sodium: 21458.

TDS by Evapor. @ 110 C: 67820.

Calculated TDS : 64581.

TDS at Ignition : 59420.

Sample appearance:

THE SAMPLE CONSISTED OF OIL STAINED MUDDY, SALT WATER.

Remarks:

FE PRES. E82-13618-1; TOP RESIS: 1.99, OIL STAINED MUD. -2; MIDDLE RESIS: .217  
 OIL STAINED MUDDY WATER. BOTH RESIS OHM/M @ 25 C.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80826 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44625  
 CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. D77-2233-3

Well identifier Well name KB elev. Gr. elev  
 0515042910000 COLGAS ET AL HIGHVALE 10-29-51-4 799.50 795.50

Interval Sampled from: 1621.54 to: 1639.82 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 1 Sampling point: BOTTOM  
 DST Recovery

56.40 M MUD  
 91.40 M GAS- AND OIL-CUT MUD  
 61.00 M OIL- AND WATER-CUT MUD

Date: Sampled: 1977/11/15 Received: 1977/11/18 Analyzed: 1977/12/02

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	33096.	44.691	1439.6	Cl	56400.	49.387	1590.8
Ca	2140.	3.315	106.8	HCO3	862.	0.439	14.1
Mg	778.	1.987	64.0	SO4	280.	0.181	5.8

Specific gravity 1.0660 @ 16. C Refractive Index 1.34860 @ 25. C  
 PH 7.50 @ 21. C Resistivity ohm/m 0.09400 @ 25. C

Hydrogen Sulfide Description:

Organics Description:

Calculated sodium: 33108.

TDS by Evapor. @ 110 C: 101680.

Calculated TDS : 93130.  
 TDS at Ignition : 87560.

Sample appearance:

THE SAMPLE CONSISTED OF MUDDY WATER.

Remarks:

FE PRES. D77-2233-1 TOP RESIS; .253, MUD SAMPLE. -2 MID RESIS; .121, WATERY MU  
 D SAMPLE. BOTH RESIS OHM/M @ 25 C.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80826 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 44626

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. b77-2234-3

Well identifier Well name KB elev. Gr. elev  
 0515042910000 COLGAS ET AL HIGHVALE 10-29-51-4 799.50 795.50

Interval Sampled from: 1582.52 to: 1606.30 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 2 Sampling point: BOTTOM  
 DST Recovery

61.00 M GAS- AND OIL-CUT MUD  
 667.50 M GAS-CUT SALT WATER  
 243.80 M OIL- AND GAS-CUT SALT WATER

Date: Sampled: 1977/11/15 Received: 1977/11/18 Analyzed: 1977/12/02

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	30673.	44.073	1334.2	Cl	53100.	49.476	1497.8
Ca	2372.	3.910	118.4	HCO3	735.	0.398	12.0
Mg	740.	2.011	60.9	SO4	191.	0.131	4.0

Specific gravity 1.0620 @ 16. C Refractive Index 1.34820 @ 25. C  
 PH 6.80 @ 21. C Resistivity ohm/m 0.09800 @ 25. C

Hydrogen Sulfide Description:

Organics Description:

Calculated sodium: 30684.

TDS by Evapor. @ 110 C: 93980.

Calculated TDS : 87448.  
 TDS at Ignition : 82820.

Sample appearance:

THE SAMPLE CONSISTED OF MURKY WATER.

Remarks:

FE PRES. D77-2234-1 TOP RESIS: .192, VERY MUDDY WATER. -2 MIDDLE RESIS: .107,  
 MUDDY WATER. BOTH RESIS OHM/M @ 25 C.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80827 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44628

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E78-3618-5

Well identifier Well name KB elev. Gr. elev  
 0515043401000 ANDEX ET AL HIGHVALE 1-34-51-4 802.20 798.10

Interval Sampled from: 1948.00 to: 1956.00 meters KB

Formation Sampled: WINT.

Sample produced by: DST # 1 Sampling point: BOTTOM  
 DST Recovery

60.00 M MUD  
 280.00 M GAS-CUT MUD  
 1320.00 M GAS-CUT SALT WATER

Date: Sampled: 1978/11/13 Received: 1978/11/15 Analyzed: 1978/11/29

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na+K	48818.		
Ca	11490.	15.514	573.4
Mg	2582.	5.749	212.5

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	102500.	78.231	2891.2
HCO3	437.	0.194	7.2
SO4	553.	0.312	11.5

Specific gravity 1.1240 @ 25. C Refractive Index 1.36300 @ 25. C  
 PH 6.90 @ 21. C Resistivity ohm/m 0.05700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description  
 Calculated sodium: 48838.  
 TDS by Evapor. @ 110 C: 185100. Calculated TDS : 166178.  
 TDS at Ignition : 163700.

Sample appearance:

THE SAMPLE CONSISTED OF MURKY SALT WATER.

Remarks:

FE TRACE. E78-3618-1 - TOP RESIS OF THE FILTRATE: .125, MUD. -2 - 1000 FT. FROM THE TOP RESIS: .057, MURKY WATER, H2S PRES. -3 - 150 FT. FROM THE TOP RESIS: .061, SAME AS -2. 4 - 57 FT. FROM TOP RESIS: .097, WATERY MUD. TRACE OF H2S. ALL RESIS OHM/M @ 25 C.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80827 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 44629

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E78-3659-3

Well identifier Well name KB elev. Gr. elev  
 0515043401000 ANDEX ET AL HIGHVALE 1-34-51-4 802.20 798.10

Interval Sampled from: 1727.00 to: 1748.00 meters KB

Formation Sampled: WABAMUN

Sample produced by: DST # 3 Sampling point: BOTTOM  
 DST Recovery

96.00 M GAS-CUT MUD  
 CATIONS

ION	mg/l	%MEQ	MEQ/L
Na+K	2422.		
Ca	9.	0.420	0.4
Mg	4.	0.308	0.3

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	2439.	64.340	68.8
HCO3	1298.	19.895	21.3
SO4	665.	12.949	13.8
CO3	67.	2.088	2.2

Specific gravity 1.0070 @ 25. C Refractive Index 1.33420 @ 25. C  
 PH 9.00 @ 22. C Resistivity ohm/m 0.96200 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description  
 Calculated sodium: 2422. Calculated TDS : 6245.  
 TDS by Evapor. @ 110 C: 7940. TDS at Ignition : 5540.

Sample appearance:

THE ANALYSIS DETERMINED ON WATER FILTERED FROM MUD.

Remarks:

FE NIL. E78-3659-1 - TOP RESIS OF THE FILTRATE; 1.05, MUD SAMPLE. -2 - MIDDLE RESIS OF THE FILTRATE: .962, MUD SAMPLE. -4 - DHS A LYNES UNITED DHS REC'D AT ATM. PRESSURE. CONTAINED IN THE CHAMBER WAS A SMALL QUANTITY OF MUD ONLY. THERE WAS INSUFFICIENT SAMPLE FOR ANY ANALYSIS. ALL RESIS OHM/M @ 25 C.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80801 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 44599  
 CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E81-7087-3

Well identifier Well name KB elev. Gr. elev  
 0515041816000 ANDEX ET AL HIGHVALE 16-18-51-4 799.00 794.90

Interval Sampled from: 1651.00 to: 1656.00 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 2 Sampling point: BOTTOM

DST Recovery 36.00 M OIL-CUT MUD  
 69.00 M OIL-CUT SALT WATER  
 Date: Sampled: 1981/09/20 Received: 1981/09/23 Analyzed: 1981/10/13

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	35876.	44.312	1560.5	Cl	62000.	49.659	1748.8
K	851.	0.618	21.8	HCO3	276.	0.128	4.5
Ca	2755.	3.904	137.5	SO4	372.	0.220	7.7
Mg	496.	1.159	40.8				

Specific gravity 1.0700 @ 25. C Refractive Index 1.34980 @ 25. C  
 PH 7.10 @ 21. C Resistivity ohm/m 0.07700 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 36391. Calculated TDS : 102150.  
 TDS by Evapor. @ 110 C: 106400. TDS at Ignition : 96320.

Sample appearance:

THE SAMPLE CONSISTED OF MUDDY SALT WATER WITH A SCUM OF OIL PRES.

Remarks:

FE PRES. E81-7087-1: TOP RESIS: .179, MUD. TRACE OF OIL. -2: MIDDLE RESIS: .09  
 0, SL. MUDDY WATER, OIL SCUM. H2S PRES. BOTH RESIS OHM/M @ 25 C.  
 -----

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80811 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44606

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E82-736-1

Well identifier Well name KB elev. Gr. elev  
 0515042114000 ANDEX COLGAS HIGHVALE 14-21-51-4 814.60 810.50

Interval Sampled from: 1620.00 to: 1622.00 meters KB

Formation Sampled: BF 6440

Sample produced by: Swabbing Sampling point: WELLHEAD  
 Date: Sampled: 1982/05/21 Received: 1982/05/25 Analyzed: 1982/05/26

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	29920.	44.682	1301.4	Cl	50300.	48.710	1418.8
K	534.	0.469	13.7	HCO3	1449.	0.815	23.7
Ca	2042.	3.498	101.9	SO4	270.	0.193	5.6
Mg	578.	1.633	47.6				

Specific gravity 1.0580 @ 25. C Refractive Index 1.34730 @ 25. C  
 PH 7.10 @ 20. C Resistivity ohm/m 0.08800 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 29860. Calculated TDS : 83762.  
 TDS by Evapor. @ 110 C: 86300. TDS at Ignition : 80760.

Sample appearance:

THE ANALYSIS IS CHARACTERISTIC OF A FORMATION WATER.

Remarks:

FE MUCH.  
 -----

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 80811 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 44607

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E82-736-2

Well identifier Well name KB elev. Gr. elev  
 0515042114000 ANDEX COLGAS HIGHVALE 14-21-51-4 814.60 810.50

Interval Sampled from: 1620.00 to: 1622.00 meters KB

Formation Sampled: BF 6440

Sample produced by: Swabbing Sampling point: WELLHEAD  
 Date: Sampled: 1982/05/21 Received: 1982/05/25 Analyzed: 1982/05/26

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	30280.	44.747	1317.1	Cl	50700.	48.585	1430.1
K	573.	0.498	14.7	HCO3	1486.	0.827	24.4
Ca	2146.	3.638	107.1	SO4	280.	0.198	5.8
Mg	539.	1.507	44.4				

Specific gravity 1.0590 @ 25. C Refractive Index 1.34740 @ 25. C  
 PH 7.20 @ 20. C Resistivity ohm/m 0.08800 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 30092. Calculated TDS: 84488.  
 TDS by Evapor. @ 110 C: 87440. TDS at Ignition: 81860.

Sample appearance:

THE ANALYSIS IS CHARACTERISTIC OF A FORMATION WATER.

Remarks:

FE PRES.

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 80811 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): 44608

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. B82-6697

Well identifier Well name KB elev. Gr. elev  
 0515042114000 ANDEX COLGAS HIGHVALE 14-21-51-4 814.60 810.50

Interval Sampled from: 1628.00 to: 1638.00 meters KB

Formation Sampled: ELRSL 3360

Sample produced by: Sampling point: TOP OF TOOL  
 Date: Sampled: 1982/11/09 Received: 1982/11/18 Analyzed: 1982/12/03

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	13500.	46.131	587.2	Cl	22000.	48.748	620.5
K	145.	0.291	3.7	HCO3	451.	0.581	7.4
Ca	625.	2.450	31.2	SO4	436.	0.713	9.1
Mg	168.	1.086	13.8				

Specific gravity 1.0240 @ 25. C Refractive Index 1.33930 @ 25. C  
 PH 7.80 @ 21. C Resistivity ohm/m 0.18200 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 13611. Calculated TDS: 37062.  
 TDS by Evapor. @ 110 C: 38000. TDS at Ignition: 34300.

Sample appearance:

ANALYSIS DETERMINED ON SALT WATER REC'D FROM OIL CUT MUD.

Remarks:

FE TRACE. E82-6697-1: TOP RESIS: 1.12, MUD. -2: MIDDLE RESIS: .229, WATER REC'D FROM OIL CUT MUD. -4: DHS STRAT HUGHES DHS WAS REC'D EMPTY. BOTH RESIS OHM/M @ 25 C.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80782 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): 44588

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E82-5374-2

Well identifier Well name KB elev. Gr. elev  
 0515041513000 ANDEX ET AL HIGHVALE 13-15-51-4 826.30 822.20

Interval Sampled from: 1630.00 to: 1639.00 meters KB

Formation Sampled: RUN 6100

Sample produced by: DST # 1 Sampling point: DHS  
 DST Recovery

500.00 M CLEAN OIL  
 Date: Sampled: 1982/10/07 Received: 1982/10/12 Analyzed: 1982/10/29

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	25040.	45.799	1089.2
K	326.	0.351	8.3
Ca	1602.	3.361	79.9
Mg	330.	1.142	27.2

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	41000.	48.628	1156.5
HCO3	960.	0.662	15.7
SO4	66.	0.058	1.4

Specific gravity 1.0480 @ 25. C Refractive Index 1.34430 @ 25. C  
 PH 6.90 @ 23. C Resistivity ohm/m 0.10600 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 24520. Calculated TDS : 67990.  
 TDS by Evapor. @ 110 C: 70280. TDS at Ignition : 63560.

Sample appearance:

STRATR HUGHES TESTERS DHS REC'D UNDER ATM. PRESSURE AND CONTAINED 3.0 L OF MUD  
 DY WATER CUT OIL.

Remarks:

FE PRES.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80795 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44594

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. #84-9739

Well identifier Well name KB elev. Gr. elev  
 0515041616000 ANDEX ET AL HIGHVALE 16-16-51-4 798.90 794.80

Interval Sampled from: 1605.00 to: 1610.00 meters KB

Formation Sampled: ELRSL. 3360

Sample produced by: Sampling point:  
 Date: Sampled: 1984/10/19 Received: 1984/10/27 Analyzed: 1984/11/05

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	4880.	44.808	212.3
K	99.	0.534	2.5
Ca	171.	1.801	8.5
Mg	67.	1.164	5.5

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	7870.	46.859	222.0
HCO3	1303.	4.508	21.4
SO4	74.	0.325	1.5

Specific gravity 1.0090 @ 25. C Refractive Index 1.33540 @ 25. C  
 PH 8.10 @ 25. C Resistivity ohm/m 0.44300 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 5307. Calculated TDS : 14130.  
 TDS by Evapor. @ 110 C: 16460. TDS at Ignition : 13260.

Sample appearance:

THE WATER HAD A TRACE OF HYDRO. SCUM PRES.

Remarks:

FE PRES.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80799 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44596

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E82-10976-5

Well identifier Well name KB elev. Gr. elev  
 0515041808000 ANDEX ET AL HIGHVALE 8-18-51-4 783.60 779.50

Interval Sampled from: 1592.00 to: 1602.00 meters KB

Formation Sampled: OST

Sample produced by: DST # 1 Sampling point: DHS

DST Recovery  
 30.00 M OIL-CUT MUD  
 315.00 M OIL-CUT MUD

Date: Sampled: 1982/01/15 Received: 1982/01/18 Analyzed: 1982/01/25

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	27400.	46.293	1191.8
K	374.	0.372	9.6
Ca	1093.	2.118	54.5
Mg	379.	1.211	31.2

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	45200.	49.521	1274.9
HCO3	576.	0.367	9.4
SO4	146.	0.118	3.0

Specific gravity 1.0490 @ 25. C Refractive Index 1.34590 @ 25. C  
 PH 6.40 @ 23. C Resistivity ohm/m 0.10400 @ 25. C

Hydrogen Sulfide Description:  
 Organics Description :

Calculated sodium: 27629. Calculated TDS : 74730.  
 TDS by Evapor. @ 110 C: 77060. TDS at Ignition : 70500.

Sample appearance:

A QUINN TESTERS DHS #1506 REC'D AT 3500 KPA. IT CONTAINED GAS AND 1.4 L OF OIL CUT MUD.

Remarks:

FE PRES. E82-10976-1: TOP OF TOOL SAMLL QUANTITY OF OILY MUD. INSUFFICIENT FOR ANALYSIS. -2: 190 M ABO TOOL RESIS: .103, SL. OIL CUT WATERY MUD. -3: 322 M A BO TOOL RESIS: .111, SL. OIL CUT MUDDY WATER. ALL RESIS OHM/M @ 25 C.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80801 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44598

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E81-7483

Well identifier Well name KB elev. Gr. elev  
 0515041816000 ANDEX ET AL HIGHVALE 16-18-51-4 799.00 794.90

Interval Sampled from: 1651.00 to: 1656.00 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 2 Sampling point: BHS

DST Recovery  
 36.00 M OIL-CUT MUD  
 69.00 M OIL-CUT SALT WATER

Date: Sampled: 1981/09/20 Received: 1981/10/01 Analyzed: 1981/10/19

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	35329.	43.559	1536.7
K	749.	0.543	19.2
Ca	2843.	4.021	141.9
Mg	802.	1.871	66.0

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	62000.	49.570	1748.8
HCO3	490.	0.228	8.0
SO4	352.	0.208	7.3

Specific gravity 1.0700 @ 25. C Refractive Index 1.34980 @ 25. C  
 PH 7.80 @ 23. C Resistivity ohm/m 0.08900 @ 25. C

Hydrogen Sulfide Description:  
 Organics Description :

Calculated sodium: 35783. Calculated TDS : 102020.  
 TDS by Evapor. @ 110 C: 104400. TDS at Ignition : 96240.

Sample appearance:

A LYNES UNITED DHS REC'D UNDER ATM. PRESSURE AND CONTAINED 2.3 L OF MUDDY SALT WATER ONLY.

Remarks:

FE TRACE.



-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80768 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44577

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E82-13903

Well identifier Well name KB elev. Gr. elev  
 0515041106000 ANDEX ET AL HIGHVALE 6-11-51-4 760.70 756.60

Interval Sampled from: 1574.50 to: 1575.50 meters KB

Formation Sampled: BF 6440.

Sample produced by:  
 CATIONS

Sampling point:WELLHEAD  
 ANIONS

ION	mg/l	%MEQ	MEQ/L
Na	26710.	45.754	1161.8
K	651.	0.656	16.6
Ca	1574.	3.093	78.5
Mg	301.	0.975	24.8

ION	mg/l	%MEQ	MEQ/L
Cl	44000.	48.876	1241.1
HCO3	974.	0.629	16.0
SO4	21.	0.017	0.4

Specific gravity 1.0500 @ 25. C  
 PH 6.80 @ 24. C

Refractive Index 1.34500 @ 25. C  
 Resistivity ohm/m 0.11000 @ 25. C

Hydrogen Sulfide Description:

Organics Description :

Calculated sodium: 26537.

Calculated TDS : 72911.

TDS by Evapor. @ 110 C: 76100.

TDS at Ignition : 71540.

Remarks:

FE NIL.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80775 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44584

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. D78-10154-1

Well identifier Well name KB elev. Gr. elev  
 0515041404000 SIEBENS ET AL HIGHVALE 4-14-51-4 777.50 773.60

Interval Sampled from: 1944.62 to: 1965.35 meters KB

Formation Sampled: WINTERBURN

Sample produced by: DST # 4  
 DST Recovery

Sampling point:

27.40 M SALT WATER-CUT MUD  
 1396.00 M SULPHUROUS SALT WATER

Date: Sampled: 1978/06/27 Received: 1978/07/12 Analyzed: 1978/07/31

CATIONS

ANIONS

ION	mg/l	%MEQ	MEQ/L
Na	46681.	33.996	2030.5
K	2775.	1.188	71.0
Ca	13700.	11.446	683.6
Mg	2442.	3.364	200.9

ION	mg/l	%MEQ	MEQ/L
Cl	105400.	49.775	2973.0
HCO3	183.	0.050	3.0
SO4	516.	0.180	10.7

Specific gravity 1.1280 @ 16. C  
 PH 6.50 @ 27. C

Refractive Index 1.36340 @ 25. C  
 Resistivity ohm/m 0.05500 @ 25. C

Hydrogen Sulfide Description:

Organics Description :

Calculated sodium: 48335.

Calculated TDS : 170483.

TDS by Evapor. @ 110 C: 193100.

TDS at Ignition : 172000.

Sample appearance:

BLACK WATER. MUCH H2S PRES.

Remarks:

FE PRES.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80782 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44586

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E84-9738

Well identifier Well name KB elev. Gr. elev  
 0515041513000 ANDEX ET AL HIGHVALE 13-15-51-4 826.30 822.20

Interval Sampled from: 1634.20 to: 1637.00 meters KB

Formation Sampled: ELRSL, 3360

Sample produced by: Sampling point:  
 Date: Sampled: 1984/10/19 Received: 1984/10/25 Analyzed: 1984/11/15

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	28450.	45.274	1237.5	Cl	48800.	50.357	1376.5
K	361.	0.338	9.2	HCO3	1413.	0.847	23.2
Ca	1193.	2.178	59.5	SO4	72.	0.055	1.5
Mg	316.	0.951	26.0				

Specific gravity 1.0530 @ 25. C Refractive Index 1.34600 @ 25. C  
 PH 8.10 @ 25. C Resistivity ohm/m 0.09400 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 30248. Calculated TDS: 81324.  
 TDS by Evapor. @ 110 C: 100900. TDS at Ignition: 73420.

Remarks:

FE NIL.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80782 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 44587

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E84-10664

Well identifier Well name KB elev. Gr. elev  
 0515041513000 ANDEX ET AL HIGHVALE 13-15-51-4 826.30 822.20

Interval Sampled from: 1632.00 to: 1633.00 meters KB  
 Interval Sampled from: 1634.20 to: 1637.00 meters KB

Formation Sampled: ELRSL, 3360

Sample produced by: Sampling point:  
 CATIONS ANIONS

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	26380.	45.127	1147.5	Cl	44840.	49.741	1264.8
K	331.	0.333	8.5	HCO3	1293.	0.833	21.2
Ca	1558.	3.058	77.7	SO4	62.	0.051	1.3
Mg	265.	0.858	21.8				

Other Determinations

Parameter	mg/l
boron	7.
strontium	208.

Specific gravity 1.0500 @ 25. C Refractive Index 1.34470 @ 25. C  
 PH 7.70 @ 22. C Resistivity ohm/m 0.10100 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 27308. Calculated TDS: 74668.  
 TDS by Evapor. @ 110 C: 85470. TDS at Ignition: 71090.

Remarks:

FE PRES.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80748 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 44553  
 CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. D78-9259-3  
 Well identifier Well name KB elev. Gr. elev  
 0515040805000 ANDEX ET AL HIGHVALE 5-8-51-4 757.30 753.20

Interval Sampled from: 1569.72 to: 1584.96 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 2 Sampling point: BOTTOM

DST Recovery  
 137.20 M GAS-CUT MUD  
 45.70 M OIL-CUT MUD  
 Date: Sampled: 1978/06/17 Received: 1978/06/20 Analyzed: 1978/06/20

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na+K	4057.			Cl	4700.	63.374	132.6
Ca	205.	4.890	10.2	HCO3	930.	7.286	15.2
Mg	74.	2.911	6.1	SO4	2164.	21.539	45.1

Specific gravity 1.0080 @ 16. C Refractive Index 1.33520 @ 25. C  
 PH 8.20 @ 25. C Resistivity ohm/m 0.52800 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 4059. Calculated TDS : 11659.  
 TDS by Evapor. @ 110 C: 11950. TDS at Ignition : 11250.

Sample appearance:

THE SAMPLE CONSISTED OF OIL FLECKED WATERY MUD.

Remarks:

FE PRES. D78-9259-1 TOP RESIS: .585, MUD. -2: MIDDLE RESIS: .532, MUD. BOTH RE  
 SIS OHM/M @ 25 C.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80758 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 44568

CORE LABORATORIES CANADA LT. Lab. Sample ID. 7021-81-107

Well identifier Well name KB elev. Gr. elev  
 0515040916000 ANDEX ET AL HIGHVALE 16-9-51-4 782.10 778.00

Interval Sampled from: 1583.00 to: 1587.00 meters KB

Formation Sampled: GLC.

Sample produced by: Sampling point: BRINE H2O SAMPLE  
 Date: Sampled: 1981/02/08 Received: 1981/02/09 Analyzed: 1981/02/11

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	90750.	49.432	3947.4	Cl	140798.	49.732	3971.4
K	241.	0.077	6.2	HCO3	741.	0.152	12.1
Ca	690.	0.431	34.4	SO4	395.	0.103	8.2
Mg	70.	0.072	5.8				

Specific gravity 1.1478 @ 15. C Refractive Index 1.36680 @ 22. C  
 PH 7.70 @ 0. C Resistivity ohm/m 0.04800 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 90853. Calculated TDS : 233170.

Remarks:

FE TRACE. NA CL EQUIV 232981, CHLOROFORM EXTRACTION RESIDUE = <10 MG/L.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80762 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): 44571

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. D77-1666-3

Well identifier Well name KB elev. Gr. elev  
 0515041006000 ANDEX ET AL HIGHVALE 6-10-51-4 772.40 768.40

Interval Sampled from: 1573.38 to: 1579.47 meters KB

Formation Sampled: BF

Sample produced by: DST # 3 Sampling point: BOTTOM

DST Recovery  
 91.40 M CLEAN OIL  
 35.40 M OIL-CUT MUD  
 Date: Sampled: 1977/10/24 Received: 1977/11/01 Analyzed: 1977/12/09

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	7197.	47.768	313.1
Ca	164.	1.249	8.2
Mg	78.	0.979	6.4

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	10025.	43.147	282.8
HCO3	2080.	5.202	34.1
SO4	521.	1.655	10.8

Specific gravity 1.0160 @ 16. C Refractive Index 1.33640 @ 25. C  
 PH 7.30 @ 21. C Resistivity ohm/m 0.32300 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 7199. Calculated TDS : 19009.  
 TDS by Evapor. @ 110 C: 20360. TDS at Ignition : 17740.

Sample appearance:

THE SAMPLE CONSISTED OF WATER WITH A LAYER OF OIL.

Remarks:

FE PRES. D77-1666-2 MIDDLE RESIS; .431 OHM/M @ 25 C. SL. OIL CUT MUD.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 80762 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): 44572

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. D77-1667-3

Well identifier Well name KB elev. Gr. elev  
 0515041006000 ANDEX ET AL HIGHVALE 6-10-51-4 772.40 768.40

Interval Sampled from: 1580.08 to: 1587.40 meters KB

Formation Sampled: BF

Sample produced by: DST # 5 Sampling point: 234 FT.

DST Recovery  
 247.20 M CLEAN OIL  
 26.80 M MUD  
 44.50 M WATER  
 Date: Sampled: 1977/10/24 Received: 1977/11/01 Analyzed: 1977/11/29

CATIONS

ION	mg/l	%MEQ	MEQ/L
Na	26751.	45.807	1163.6
Ca	1228.	2.412	61.3
Mg	548.	1.775	45.1

ANIONS

ION	mg/l	%MEQ	MEQ/L
Cl	44524.	49.439	1255.9
HCO3	657.	0.424	10.8
SO4	175.	0.143	3.6

Specific gravity 1.0530 @ 16. C Refractive Index 1.34530 @ 25. C  
 PH 7.20 @ 21. C Resistivity ohm/m 0.11300 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description :  
 Calculated sodium: 26760. Calculated TDS : 73558.  
 TDS by Evapor. @ 110 C: 81160. TDS at Ignition : 70200.

Sample appearance:

THE SAMPLE CONSISTED OF CLEAR WATER.

Remarks:

FE PRES. D77-1667-4 BOTTOM RESIS; .439 OHM/M @ 25 C. MUD SAMPLE.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138182 Chemistry number: 5  
 AGSWDB Hard copy number (HRDCPNO): -1856310

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E86-1963-1

Well identifier Well name KB elev. Gr. elev  
 0495053514000 ENRON ET AL PEMBINA 14-35-49-5 763.10 758.30

Interval Sampled from: 1683.00 to: 1692.00 meters KB

Formation Sampled: ELRS

Sample produced by: DST # 3 Sampling point: MIDDLE

DST Recovery  
 96.00 M GAS-CUT MUD  
 194.00 M GAS-CUT SALT WATER

Date: Sampled: 1986/12/05 Received: 1986/12/08 Analyzed: 1986/12/15

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	23650.	45.425	1028.7	Cl	39500.	49.197	1114.2
K	299.	0.338	7.6	HCO3	1359.	0.983	22.3
Ca	1169.	2.576	58.3	SO4	169.	0.155	3.5
Mg	365.	1.326	30.0				

Specific gravity 1.0410 @ 25. C Refractive Index 1.34330 @ 25. C  
 PH 6.90 @ 21. C Resistivity ohm/m 0.11300 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 24178. Calculated TDS: 66049.  
 TDS by Evapor. @ 110 C: 64040. TDS at Ignition: 61380.

Sample appearance:

ORGANICS: TRACE. SAMPLE CONSISTED OF SALT WATER WITH AN IRON SUSPENSION.

Remarks:

Fe TRACE

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 138478 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): 39772

CHEMICAL & GEOLOGICAL LAB LTD Lab. Sample ID. E85-550-5

Well identifier Well name KB elev. Gr. elev  
 0505053606000 ANDEX ET AL HIGHVALE 6-36-50-5 755.30 750.50

Interval Sampled from: 1613.00 to: 1630.00 meters KB

Formation Sampled: BANFF

Sample produced by: DST # 1 Sampling point: DHS

DST Recovery  
 202.00 M CLEAN OIL  
 Date: Sampled: 1985/12/12 Received: 1985/12/17 Analyzed: 1985/12/23

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	35530.	44.814	1545.5	Cl	59100.	48.337	1667.0
K	790.	0.586	20.2	HCO3	1005.	0.478	16.5
Ca	2458.	3.557	122.7	SO4	313.	0.189	6.5
Mg	855.	2.040	70.4				

Specific gravity 1.0590 @ 25. C Refractive Index 1.34860 @ 25. C  
 PH 7.40 @ 23. C Resistivity ohm/m 0.08100 @ 25. C  
 Hydrogen Sulfide Description:  
 Organics Description:  
 Calculated sodium: 34419. Calculated TDS: 97639.  
 TDS by Evapor. @ 110 C: 106000. TDS at Ignition: 92500.

Sample appearance:

LYNES DHS REC'D @ATM PRESSURE, 2.3L OF SALT WATER CUT OIL (5% OIL).

Remarks:

FE TRACE. E85-550-2 TOP RES: .139 OHM/M @25C OIL CUT MUDDY WATER (30% OIL). -3  
 BOTTOM OF LAST COLLAR RES: .091 OHM/M @25C SLIGHTLY OIL STAINED MUDDY WATER

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 151481 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1994409

CHEMEX LABS (ALBERTA) LTD. Lab. Sample ID. 88-0201-8061

Well identifier Well name KB elev. Gr. elev  
 0495031411000 362107 PEMBINA 11-14-49-3 770.10 765.90

Interval Sampled from: 1551.00 to: 1556.00 meters KB

Formation Sampled: GLC SS

Sample produced by: Sampling point: RIG TANK  
 Date: Sampled: 1988/03/22 Received: 1988/03/24 Analyzed: 1988/03/29

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	29200.	45.250	1270.1	Cl	50000.	50.244	1410.3
K	297.	0.271	7.6	HCO3	549.	0.321	9.0
Ca	1680.	2.987	83.8	SO4	14.	0.010	0.3
Mg	301.	0.882	24.8				
Fe	28.	0.036	1.0				

Specific gravity 1.0630 @ 0. C Refractive Index 1.34840 @ 0. C  
 PH 6.80 @ 25. C Resistivity ohm/m 0.12400 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 30142. Calculated TDS : 82407.

Sample appearance:

CO3 < 0.5. IRON ANALYZED ON FILTERED SAMPLE.

| AGSWDB WATER ANALYSIS REPORT |

AGSWDB Well site identifier (SITID): 151481 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): -2003302

CHEMEX LABS (ALBERTA) LTD. Lab. Sample ID. 88-0201-8048

Well identifier Well name KB elev. Gr. elev  
 0495031411000 362107 PEMBINA 11-14-49-3 770.10 765.90

Interval Sampled from: 1551.00 to: 1556.00 meters KB

Formation Sampled: GLC SS

Sample produced by: Sampling point: TEST SEPARATOR  
 Date: Sampled: 1988/03/13 Received: 1988/03/15 Analyzed: 1988/03/18

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	29500.	45.583	1283.2	Cl	50000.	50.100	1410.3
K	305.	0.277	7.8	HCO3	2060.	1.199	33.8
Ca	1140.	2.021	56.9	SO4	75.	0.055	1.6
Mg	261.	0.763	21.5				
Fe	1.	0.002	0.0				

Specific gravity 1.0620 @ 0. C Refractive Index 1.34750 @ 0. C  
 PH 7.50 @ 25. C Resistivity ohm/m 0.10600 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 31436. Calculated TDS : 83925.

Sample appearance:

CO3 <, 0.5. IRON ANALYZED ON FILTERED SAMPLE.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 151483 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1958101

AGAT ENGINEERING LTD Lab. Sample ID. WE8500

Well identifier Well name KB elev. Gr. elev  
 0495050302000 BUMPER ET AL PEMBINA 2-3-49-5 772.60 767.80

Interval Sampled from: 1754.00 to: 1759.00 meters KB

Formation Sampled: NORD

Sample produced by: Sampling point: SWAB  
 Date: Sampled: 1987/11/27 Received: 1987/12/02 Analyzed: 1987/12/16

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	11000.	41.265	478.5	Cl	20000.	48.652	564.1
K	382.	0.843	9.8	HCO3	705.	0.996	11.6
Ca	1420.	6.111	70.9	SO4	536.	0.962	11.2
Mg	156.	1.107	12.8				
Fe	21.	0.063	0.7				

Specific gravity 1.0210 @ 0. C  
 PH 7.20 @ 25. C Resistivity ohm/m 0.26000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 11568. Calculated TDS : 34027.

Sample appearance:

SALINITY=3.53%.TRC+=LESS THAN 0.1.N.D.=NOT DETECTED.NIL=0.0.TRC\*=LESS THAN 0.0  
 01.N.A.=NOT ANALYZED.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 151483 Chemistry number: 2  
 AGSWDB Hard copy number (HRDCPNO): -1994410

AGAT ENGINEERING LTD Lab. Sample ID. WE8265D

Well identifier Well name KB elev. Gr. elev  
 0495050302000 BUMPER ET AL PEMBINA 2-3-49-5 772.60 767.80

Interval Sampled from: 1754.00 to: 1762.00 meters KB

Formation Sampled: NORD

Sample produced by: DST # 2 Sampling point: BHS  
 DST Recovery

80.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1987/09/30 Received: 1987/10/06 Analyzed: 1987/10/21

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	3240.	48.499	140.9	Cl	4140.	40.186	116.8
K	38.	0.330	1.0	HCO3	1310.	7.388	21.5
Ca	67.	1.152	3.3	SO4	260.	1.863	5.4
Mg	20.	0.558	1.6				
Fe	2.	0.023	0.1				

Specific gravity 1.0030 @ 0. C  
 PH 8.10 @ 25. C Resistivity ohm/m 0.71000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 3189. Calculated TDS : 8320.

Sample appearance:

BA, SR, BR, I, REF. INDEX=N.A. DST CHAMBER 2: OP, RECOVERY GAS +7000 MLS OIL/MUD. SALINITY=0.75%.TRC+=LESS THAN 0.1.N.D.=NOT DETECTED.NIL=0.0.TRC\*=LESS THAN 0.001.N.A.=NOT ANALYZED. DST CHAMBER 2: O.P. 758 KPA.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 151483 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): -1994411

AGAT ENGINEERING LTD Lab. Sample ID. WE8265C

Well identifier Well name KB elev. Gr. elev  
 0495050302000 BUMPER ET AL PEMBINA 2-3-49-5 772.60 767.80

Interval Sampled from: 1754.00 to: 1762.00 meters KB

Formation Sampled: NORD

Sample produced by: DST # 2 Sampling point: TOP OF TOOL

DST Recovery  
 80.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1987/09/30 Received: 1987/10/06 Analyzed: 1987/10/21

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	2430.	50.344	105.7	Cl	2790.	37.482	78.7
K	21.	0.256	0.5	HCO3	793.	6.190	13.0
Ca	30.	0.723	1.5	SO4	379.	3.758	7.9
Mg	7.	0.286	0.6	CO3	60.	0.952	2.0
Fe	0.50000	0.009	0.0				

Specific gravity 1.0030 @ 0. C  
 PH 8.20 @ 25. C Resistivity ohm/m 0.94000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 2287. Calculated TDS: 5943.

Sample appearance:

BA, SR, BR, I & REF. INDEX=N.A.SALINITY=0.51%.TRC+=LESS THAN 0.1.N.D.=NOT DETE  
 CTED.NIL=0.0.TRC\*=LESS THAN 0.001.N.A.=NOT ANALYZED.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 151483 Chemistry number: 5  
 AGSWDB Hard copy number (HRDCPNO): -1994501

AGAT ENGINEERING LTD Lab. Sample ID. WE8265B

Well identifier Well name KB elev. Gr. elev  
 0495050302000 BUMPER ET AL PEMBINA 2-3-49-5 772.60 767.80

Interval Sampled from: 1754.00 to: 1762.00 meters KB

Formation Sampled: NORD

Sample produced by: DST # 2 Sampling point: RIG FLOOR

DST Recovery  
 80.00 M GAS- AND OIL-CUT MUD  
 Date: Sampled: 1987/09/30 Received: 1987/10/06 Analyzed: 1987/10/21

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	1960.	47.030	85.3	Cl	860.	13.381	24.3
K	37.	0.516	0.9	HCO3	3130.	28.297	51.3
Ca	32.	0.873	1.6	SO4	565.	6.489	11.8
Mg	11.	0.517	0.9	CO3	156.	2.868	5.2
Fe	1.	0.028	0.1				

Specific gravity 1.0010 @ 0. C  
 PH 8.40 @ 25. C Resistivity ohm/m 1.28000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 2069. Calculated TDS: 5232.

Sample appearance:

BA, BR, SR, I & REF. INDEX=N.A.SALINITY=0.16%.TRC+=LESS THAN 0.1.N.D.=NOT DETE  
 CTED.NIL=0.0.TRC\*=LESS THAN 0.001.N.A.=NOT ANALYZED.



AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 151484 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -2162409

AGAT ENGINEERING LTD

Lab. Sample ID. WE9197

Well identifier Well name KB elev. Gr. elev  
 0495051314020 OMV ET AL PEMBINA 14-13-49-5 805.40 800.70

Interval Sampled from: 1737.00 to: 1740.50 meters KB

Formation Sampled: NORD

Sample produced by: DST # 1 Sampling point: TOP OF TOOL

DST Recovery 361.00 M GAS-CUT OIL  
 Date: Sampled: 1988/06/24 Received: 1988/06/29 Analyzed: 1988/07/06

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	22300.	41.314	970.0	Cl	40600.	48.776	1145.2
K	690.	0.752	17.6	HCO3	747.	0.521	12.2
Ca	2790.	5.930	139.2	SO4	372.	0.330	7.7
Mg	678.	2.376	55.8				
Fe	0.40000	0.001	0.0				

Specific gravity 1.0490 @ 0. C  
 PH 7.80 @ 25. C Resistivity ohm/m 0.12000 @ 25. C  
 Hydrogen Sulfide Description:  
 Calculated sodium: 22306. Calculated TDS : 67114.

Sample appearance:

BA, SR, BR, I, REFRACTIVE INDEX=N.A. DST 1. BHS=AL2O.P.=O KPA. RECOVERY=NIL. SA  
 LINITY=6.99%. TRC+=LESS THAN 0.1. N.D.=NOT DETECTED. NIL=0.0. TRC+=LESS THAN 0  
 .001. N.A.=NOT ANALYZED.

AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 151486 Chemistry number: 1  
 AGSWDB Hard copy number (HRDCPNO): -1981309

GEOTECH Analytical

Lab. Sample ID.' 5996-W1

Well identifier Well name KB elev. Gr. elev  
 0495052308020 CNW WESTGROWTH PEMBINA 8-23-49-5 809.70 805.50

Interval Sampled from: 1739.00 to: 1747.00 meters KB

Formation Sampled: NORD

Sample produced by: DST # 2 Sampling point: TOP OF TOOL

DST Recovery 50.00 M OIL-CUT MUD  
 426.00 M OIL-CUT SALT WATER

CATIONS				ANIONS			
ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	34400.	39.568	1496.3	Cl	67500.	50.347	1903.9
K	1110.	0.751	28.4	I	16.	0.003	0.1
Ca	4890.	6.453	244.0	HCO3	703.	0.305	11.5
Mg	1040.	2.263	85.6	SO4	506.	0.279	10.5
Fe	34.	0.032	1.2				

Other Determinations

Parameter	mg/l
barium	18.
strontium	345.

PH 6.70 @ 25. C Refractive Index 1.35500 @ 0. C  
 Calculated sodium: 36708. Resistivity ohm/m 0.07300 @ 25. C  
 Calculated TDS : 111005.

Sample appearance:

B=31.1. CATIONS/ANIONS: 0.97.

-----  
AGSWDB WATER ANALYSIS REPORT

AGSWDB Well site identifier (SITID): 151486 Chemistry number: 3  
 AGSWDB Hard copy number (HRDCPNO): -1981311

GEOTECH Analytical Lab. Sample ID. 5936-W2

Well identifier Well name KB elev. Gr. elev  
 0495052308020 CNW WESTGROWTH PEMBINA 8-23-49-5 809.70 805.50

Interval Sampled from: 1712.00 to: 1718.00 meters KB

Formation Sampled: OST

Sample produced by: DST # 5 Sampling point: MIDDLE

DST Recovery  
 19.00 M MUD  
 267.00 M SALT WATER  
 CATIONS

ANIONS

ION	mg/l	%MEQ	MEQ/L	ION	mg/l	%MEQ	MEQ/L
Na	37400.	39.996	1626.8	Cl	72800.	50.484	2053.4
K	462.	0.290	11.8	I	13.	0.002	0.1
Ca	5290.	6.490	264.0	HCO3	482.	0.194	7.9
Mg	1210.	2.448	99.6	SO4	102.	0.052	2.1
Fe	49.	0.043	1.8				

Other Determinations

Parameter	mg/l
barium	40.
boron	29.
strontium	590.

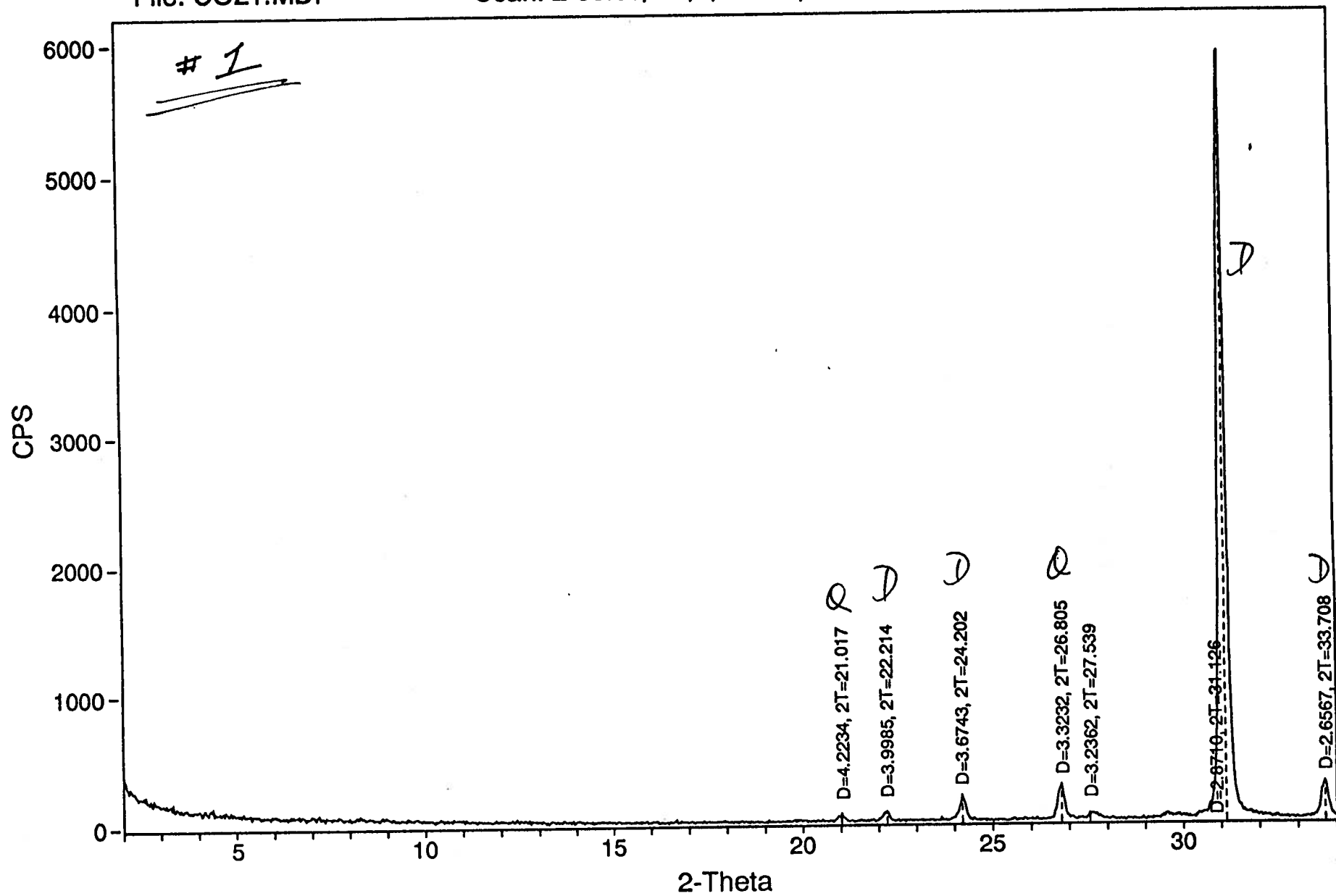
PH 6.80 @ 25. C Refractive Index 1.35500 @ 0. C  
 Calculated sodium: 39087. Resistivity ohm/m 0.07000 @ 25. C  
 Calculated TDS : 118739.

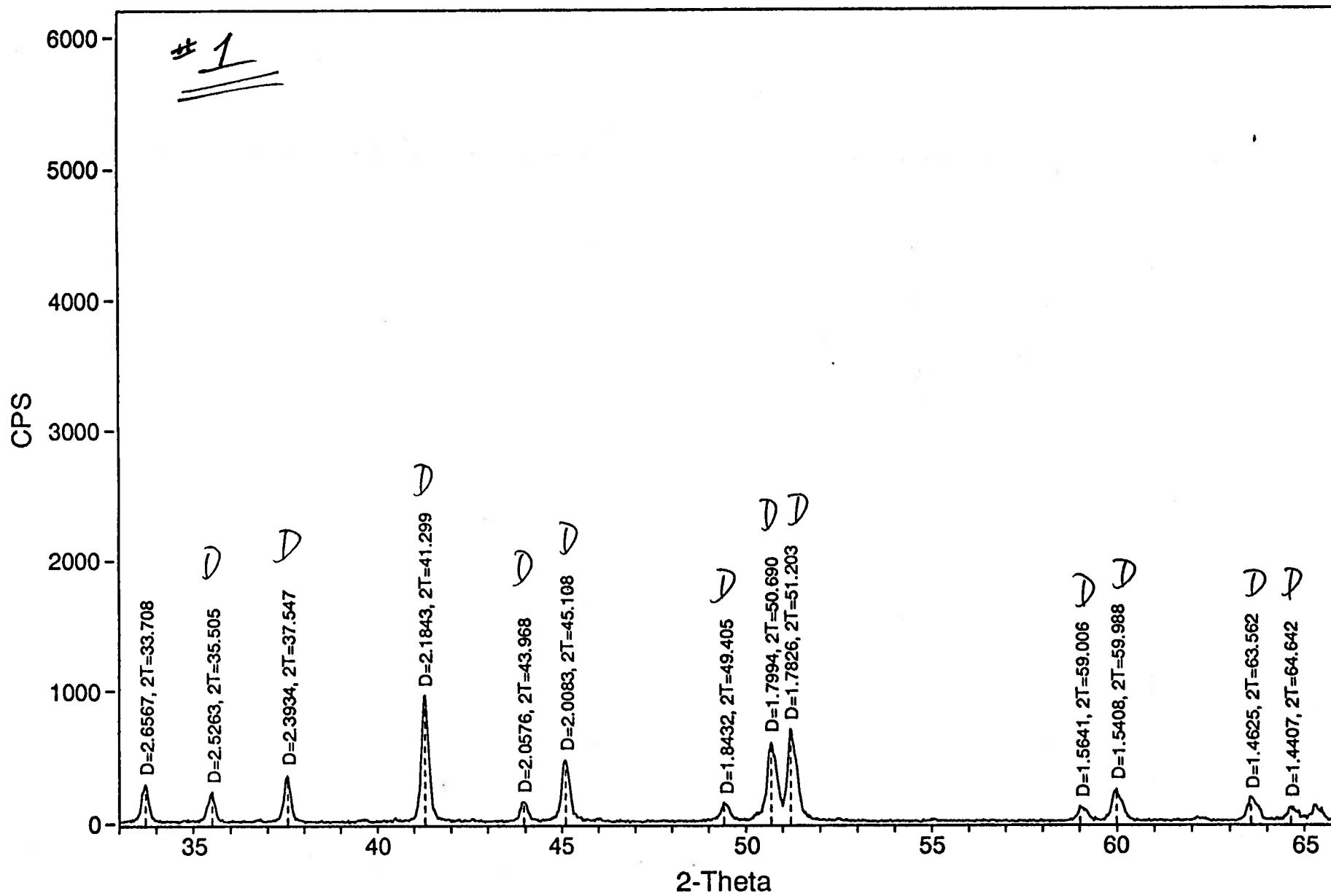
Sample appearance:

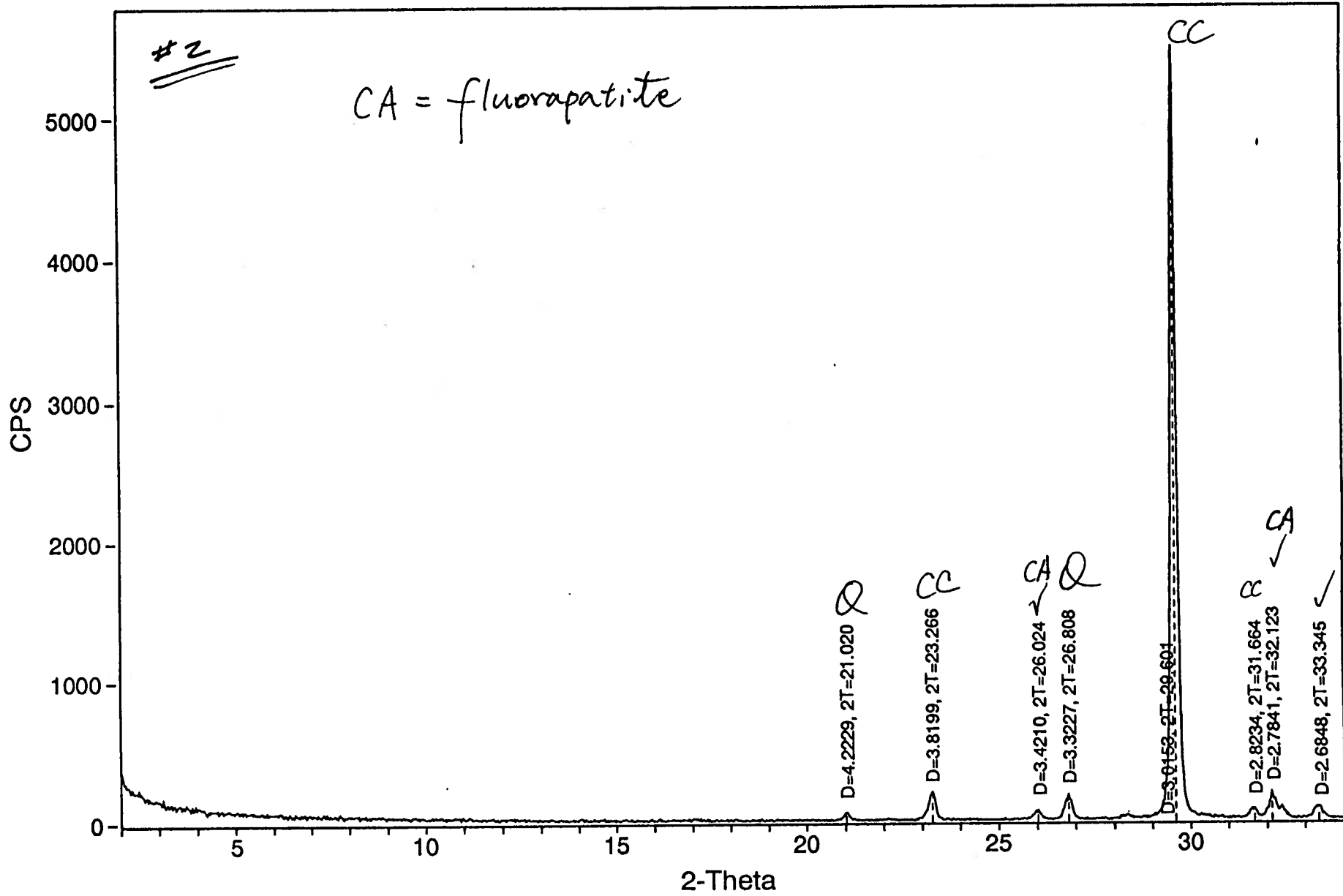
B=29.2. CATIONS/ANIONS: 0.90.  
 -----

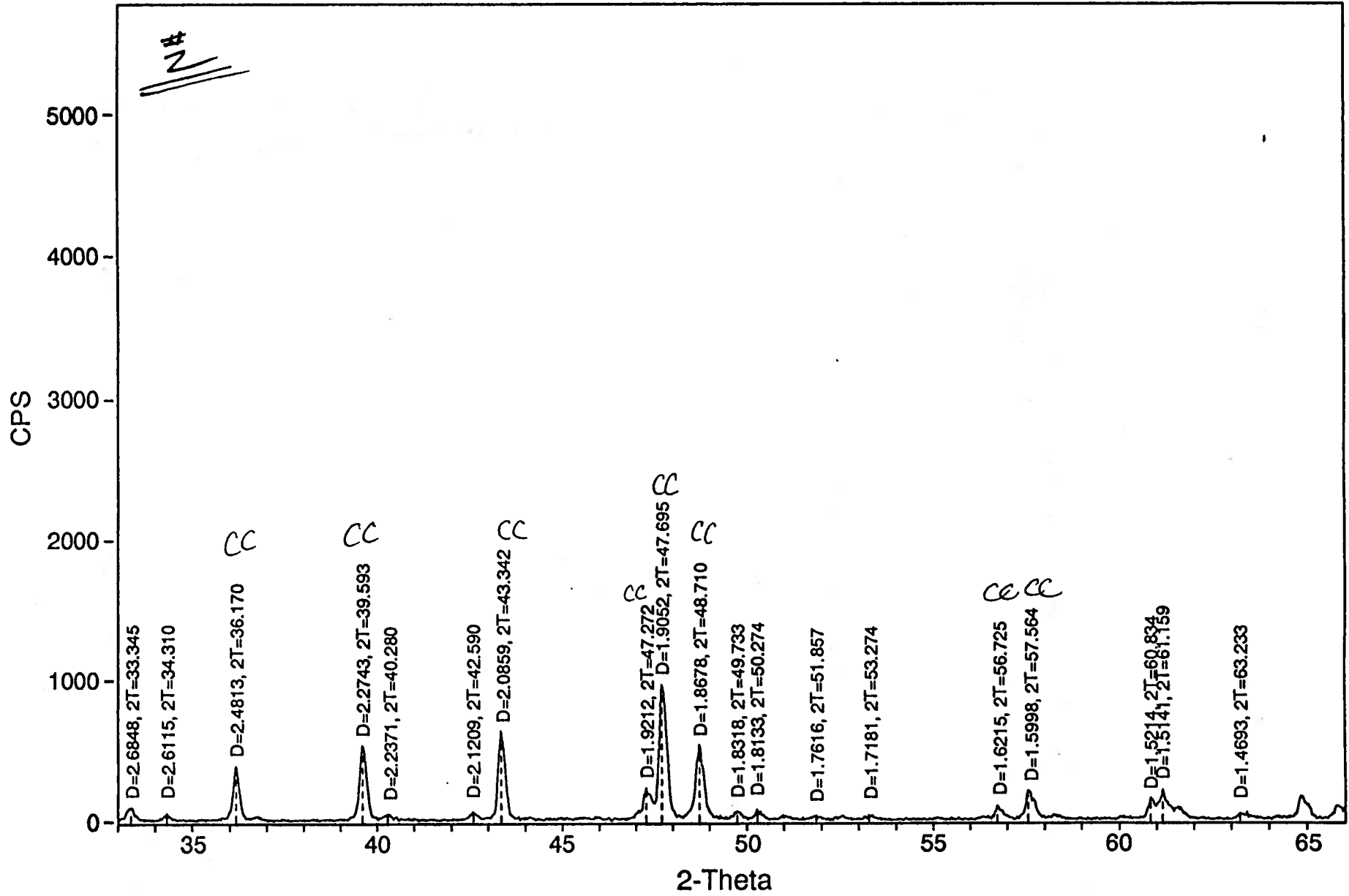
## **APPENDIX 11.3.3**

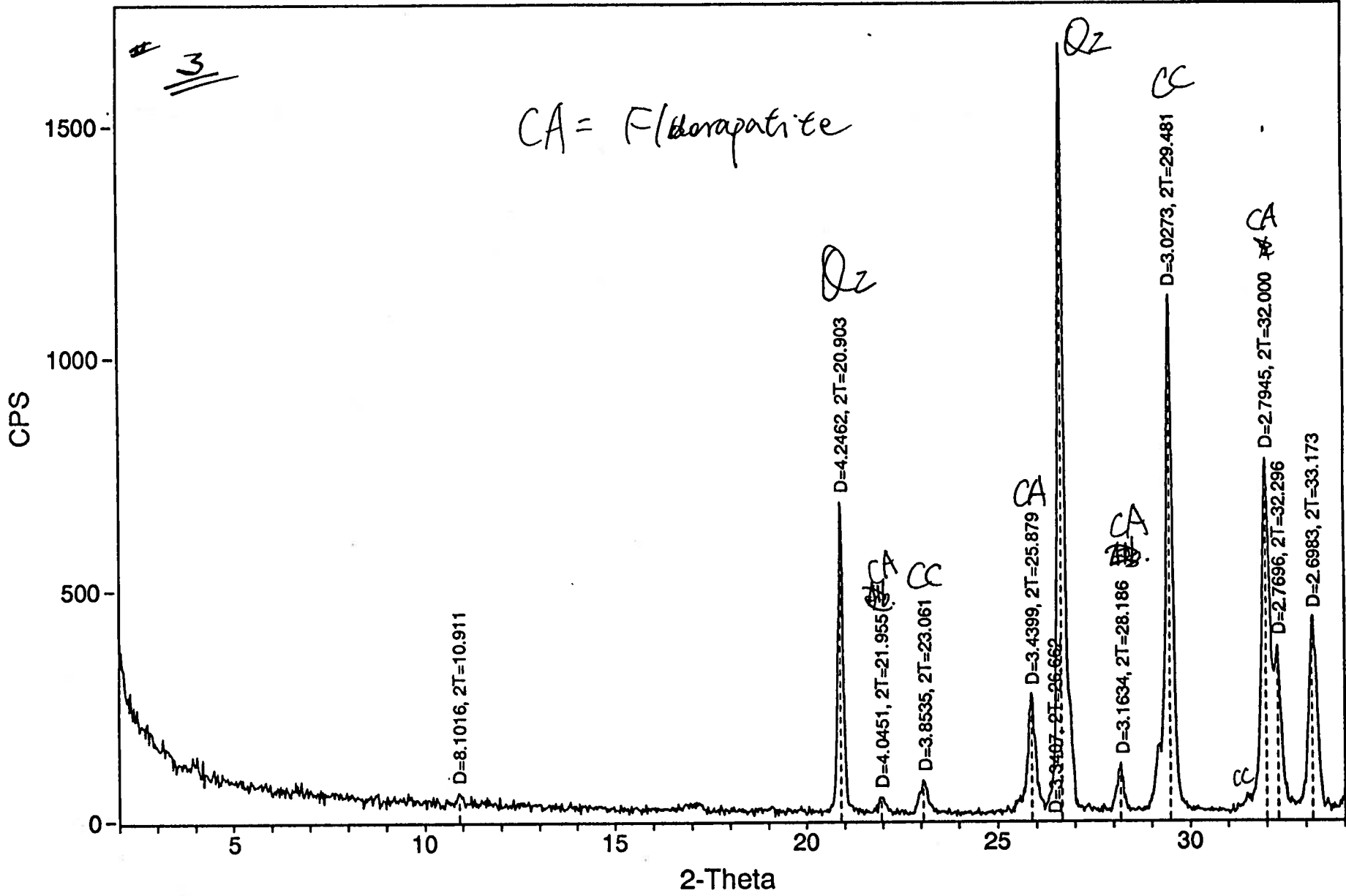
### **X-Ray Diffractograms of Aquifer Mineralogy**



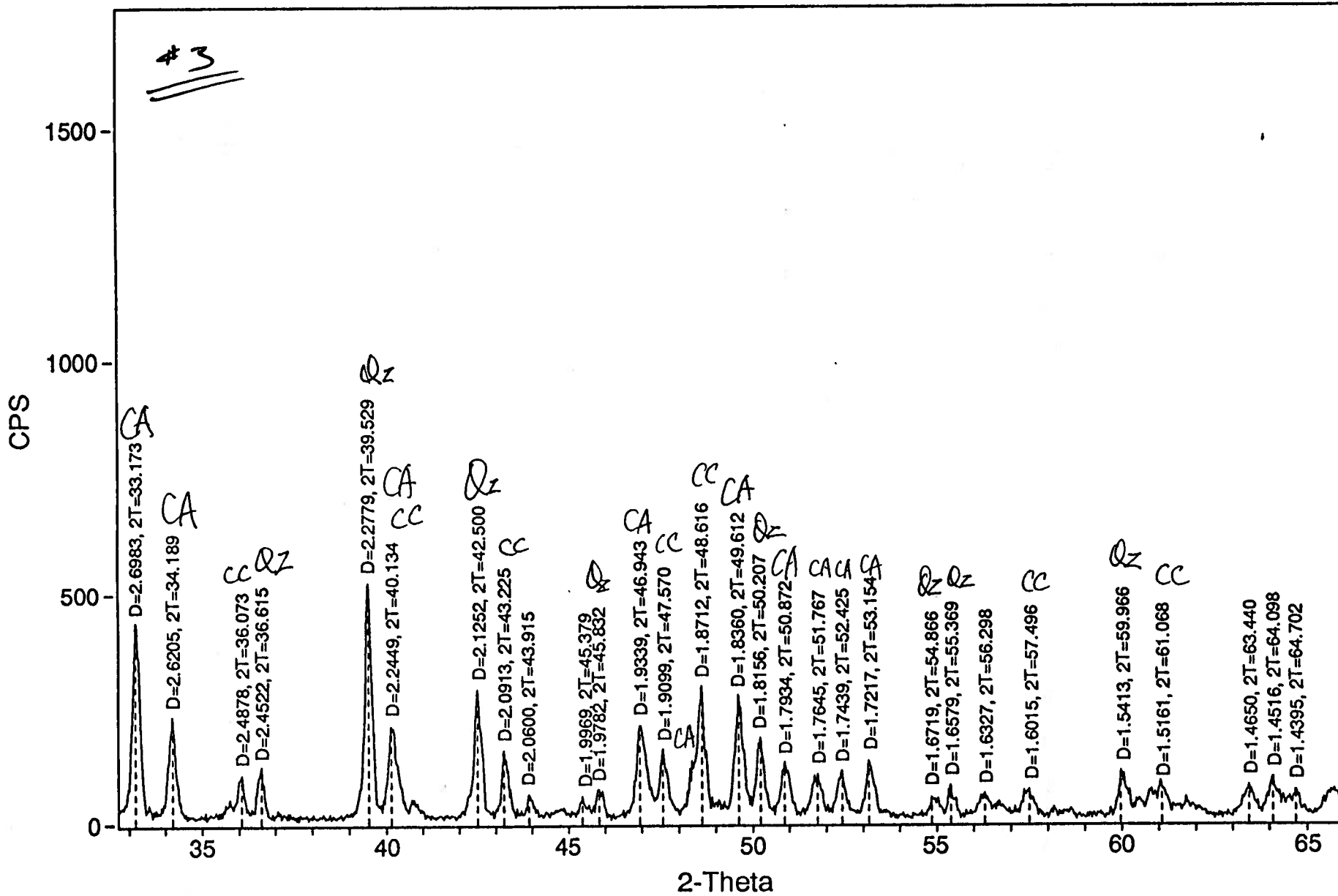


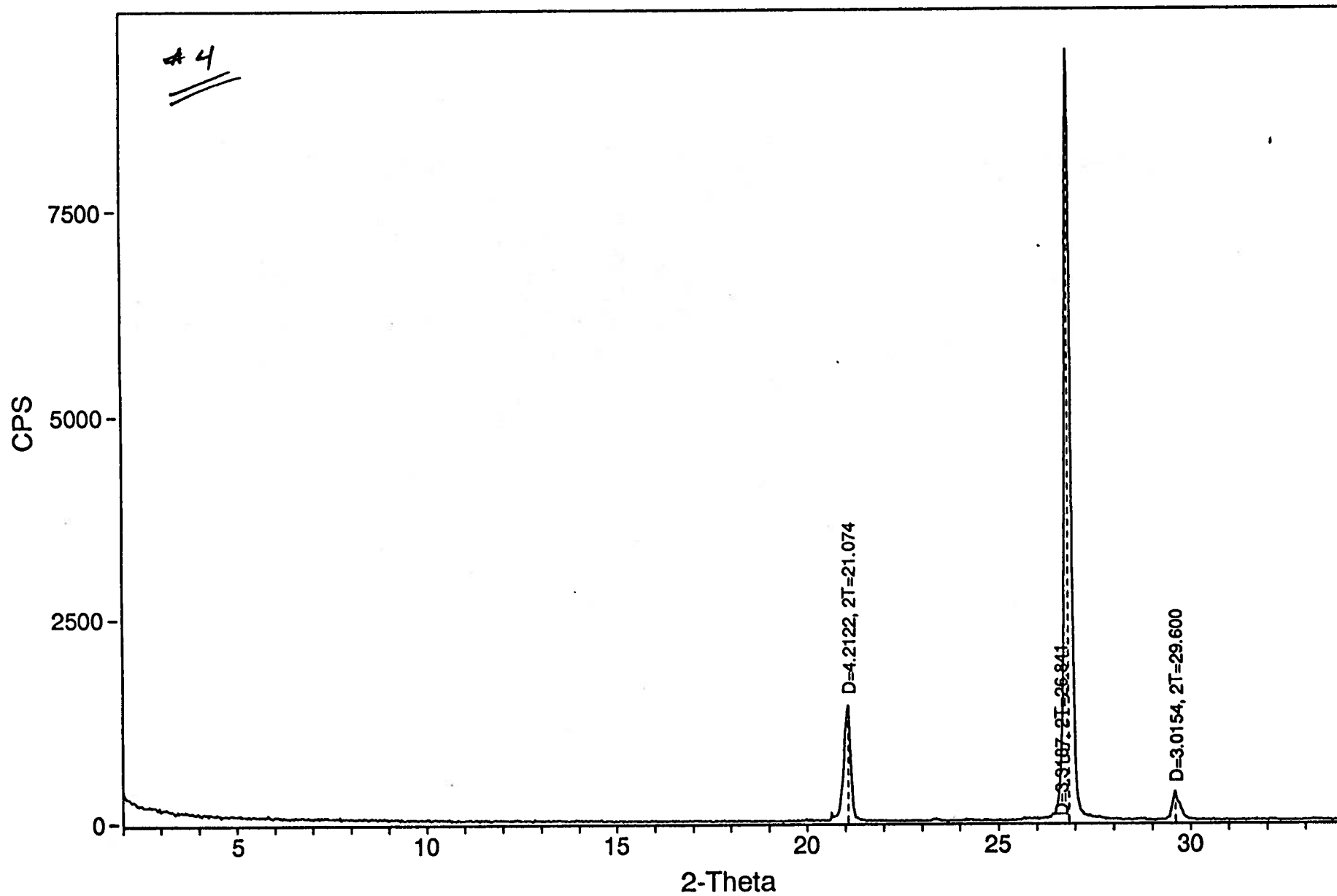


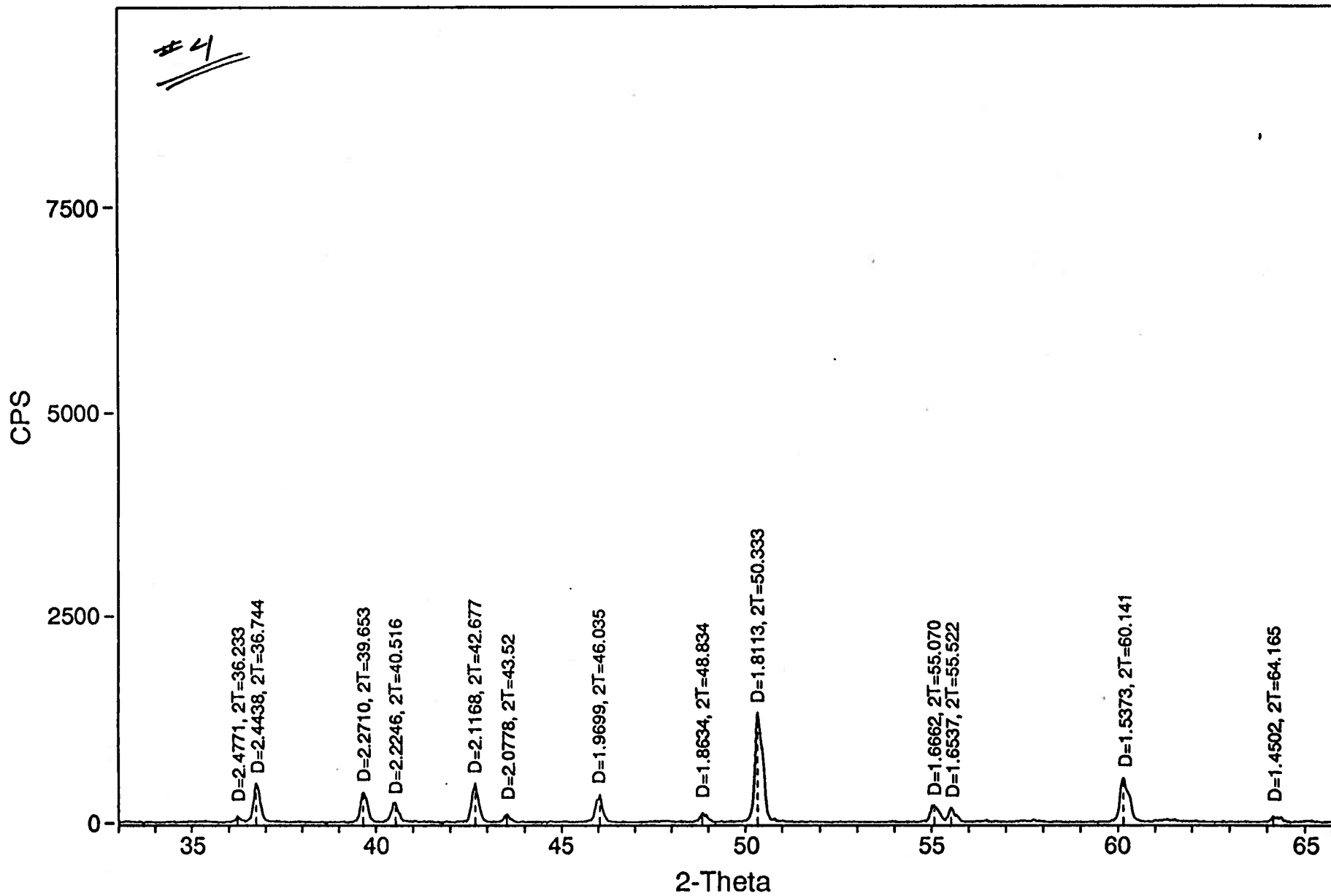


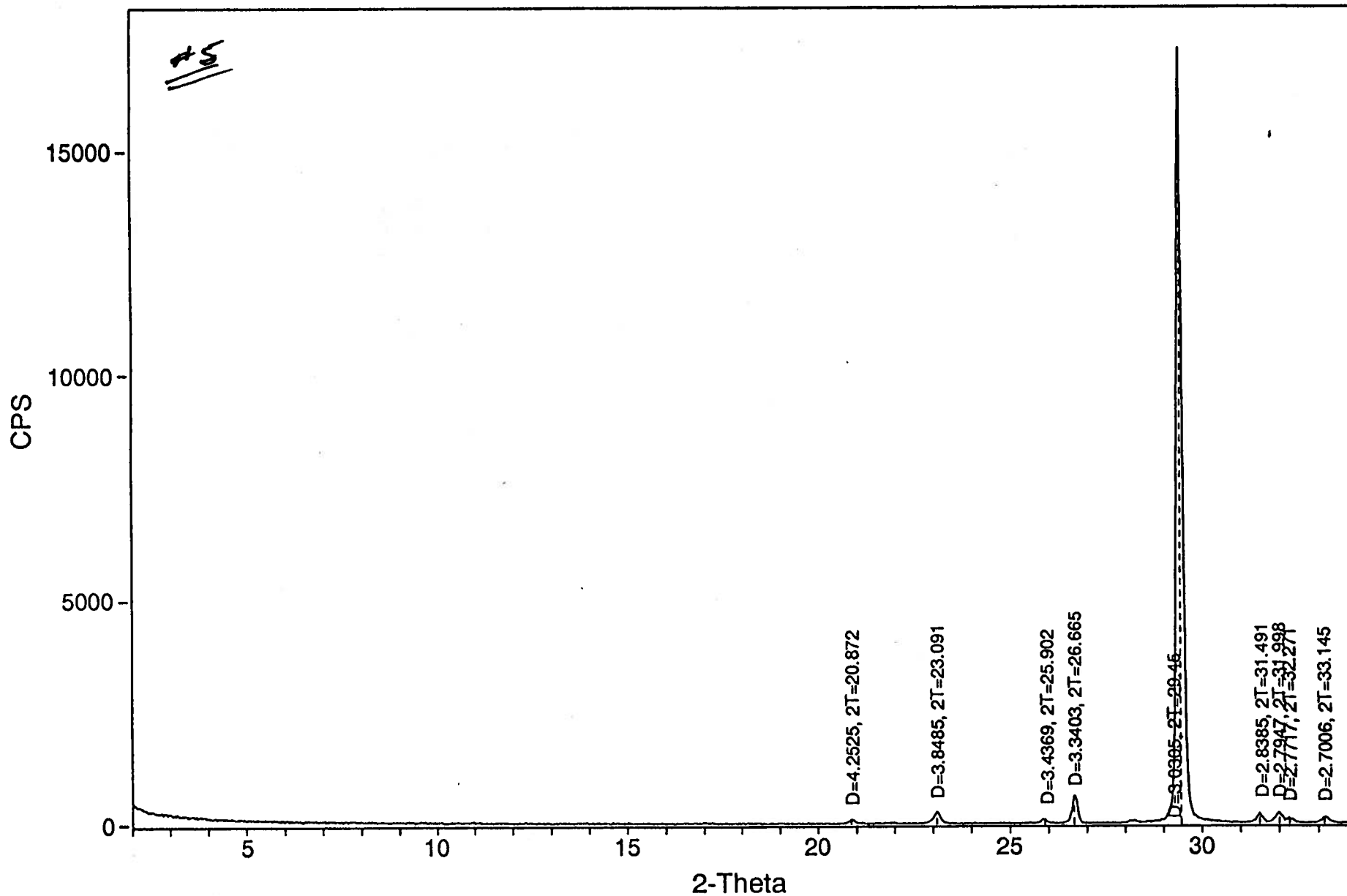


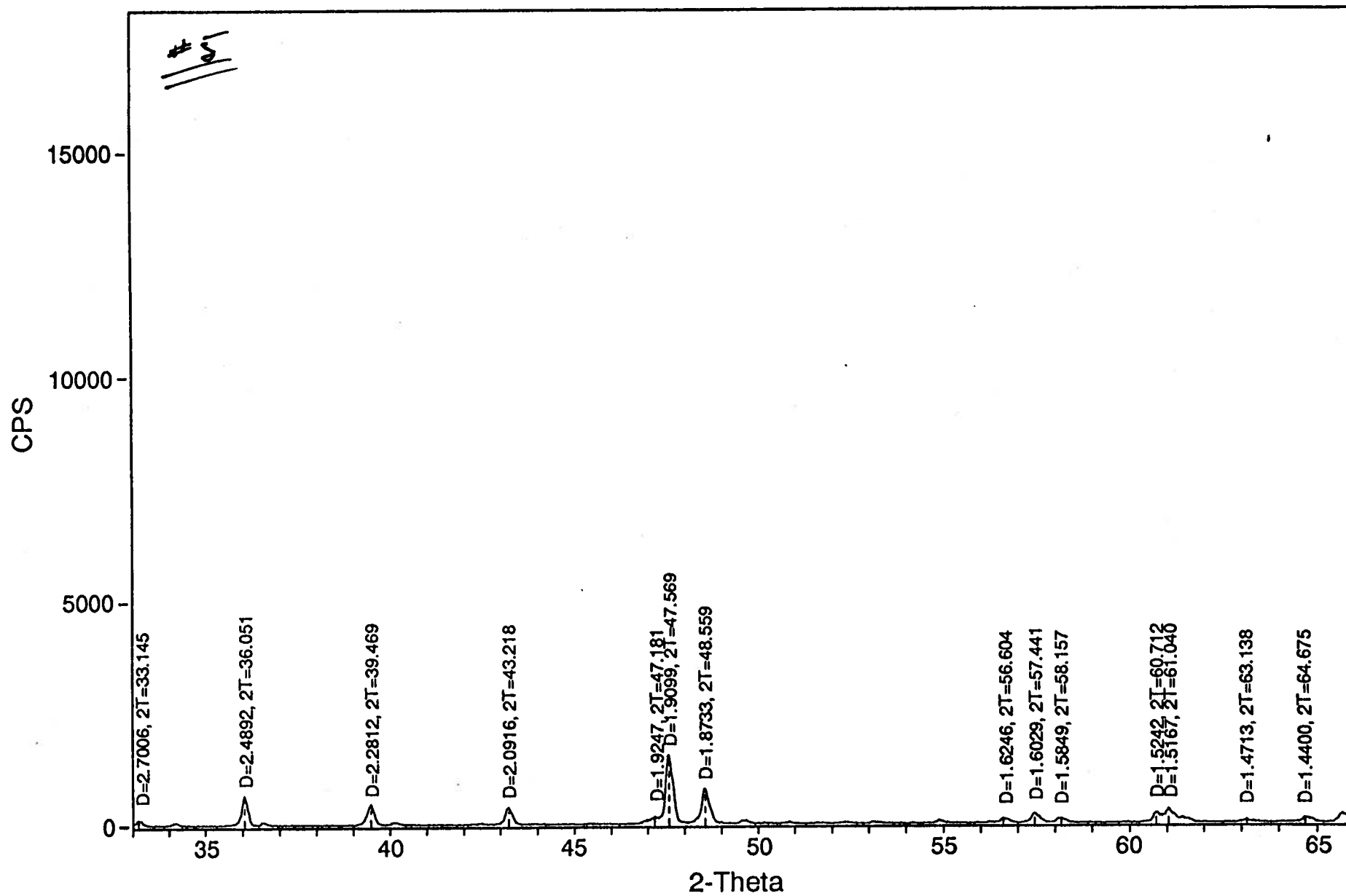


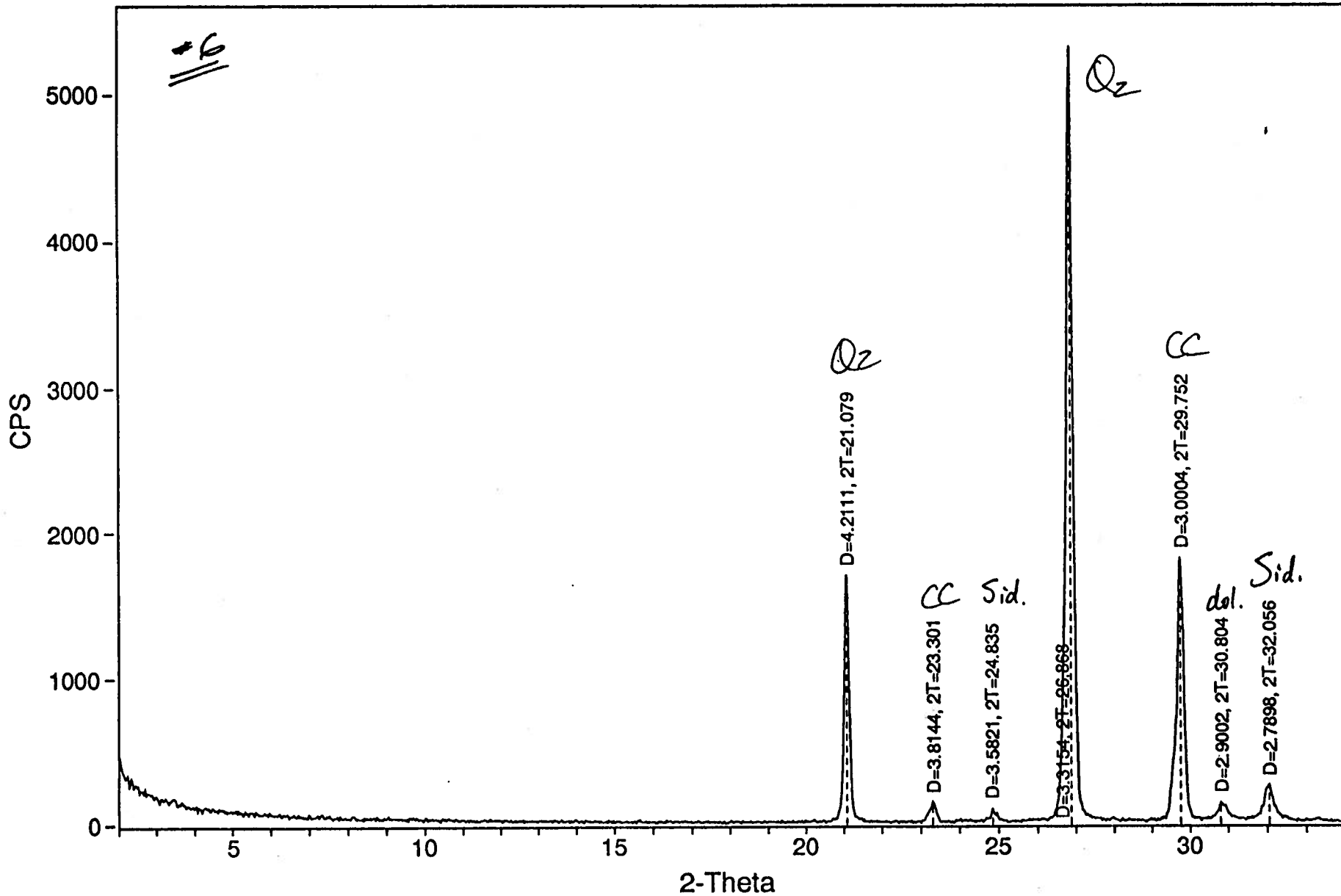


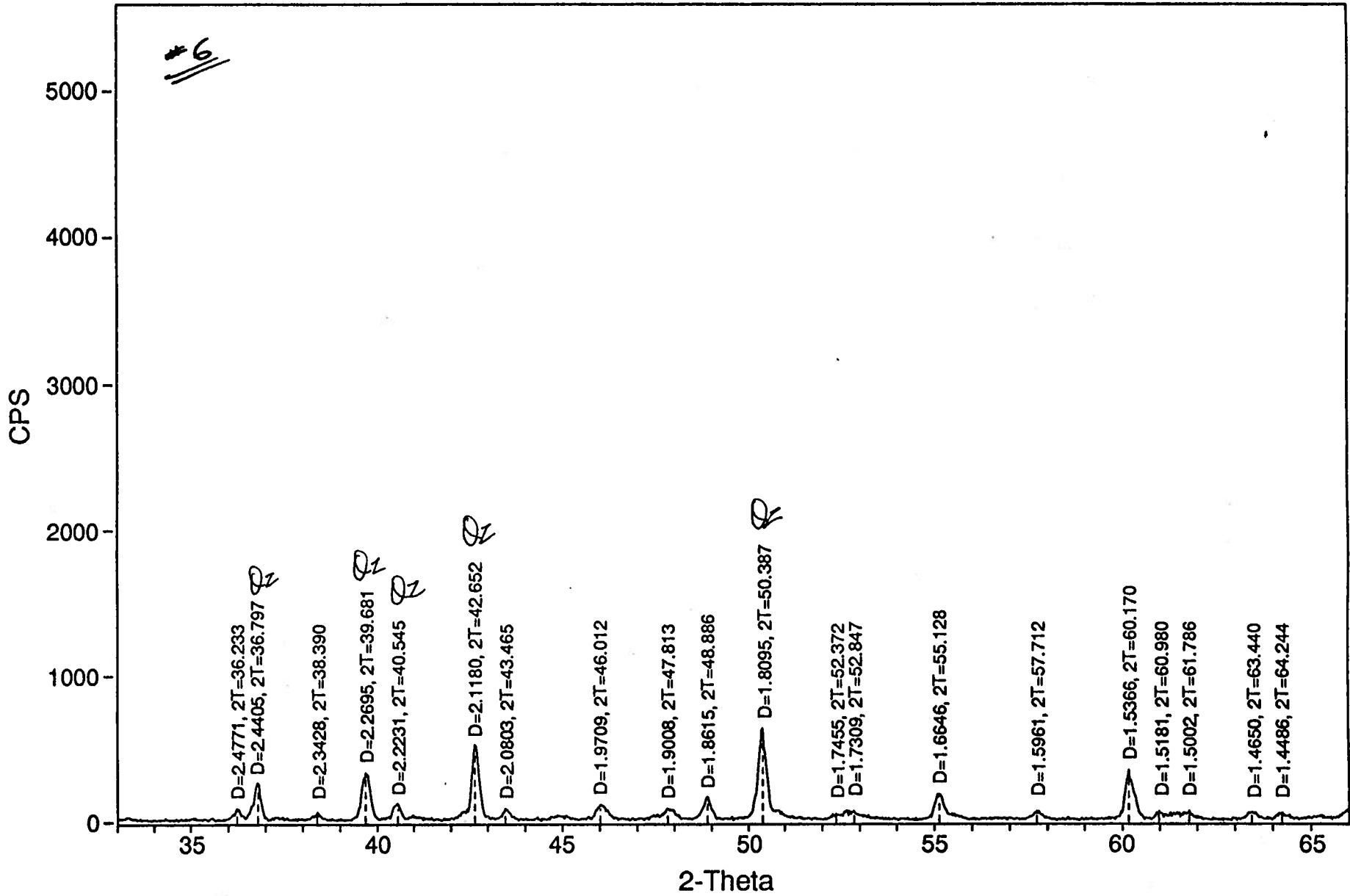


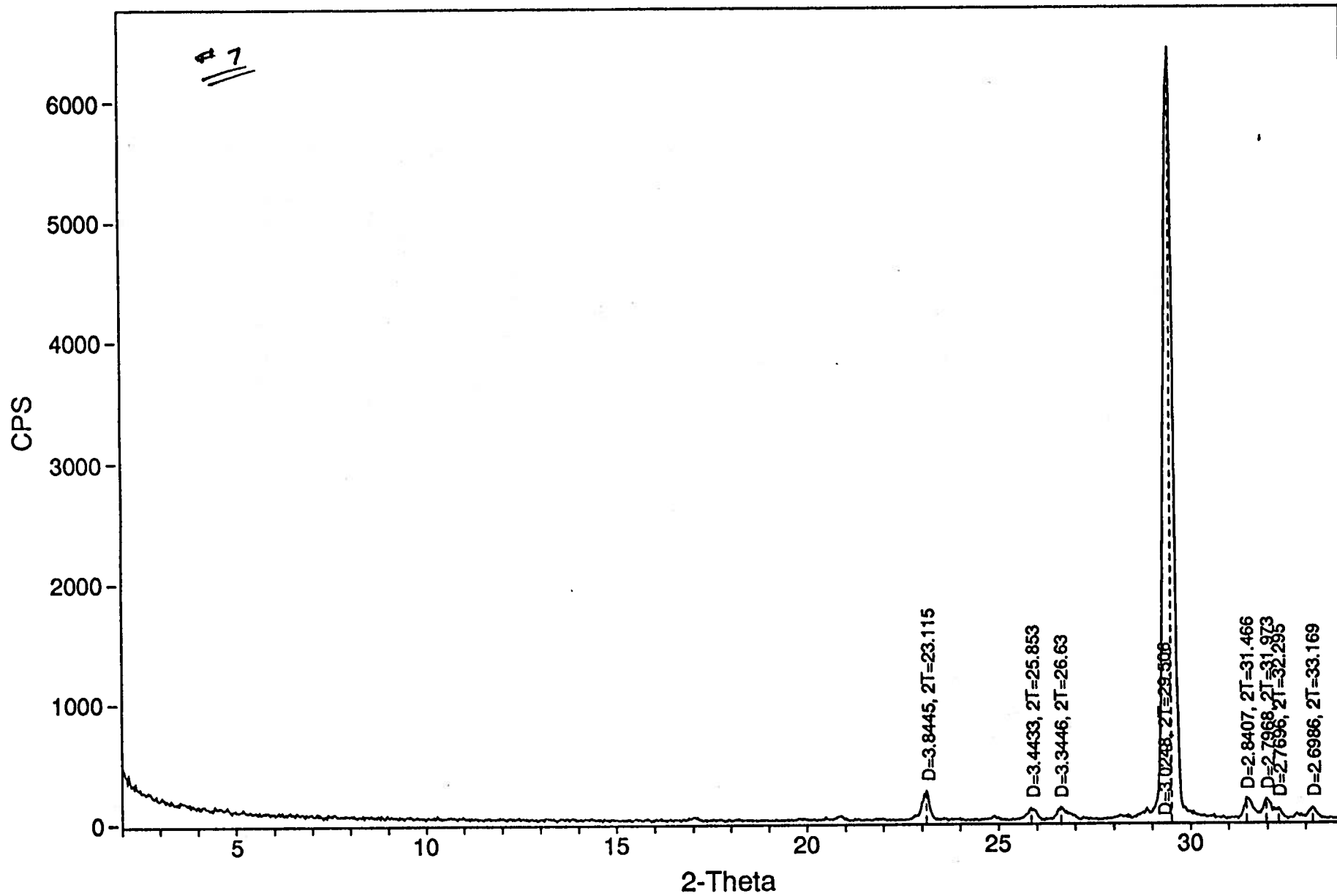




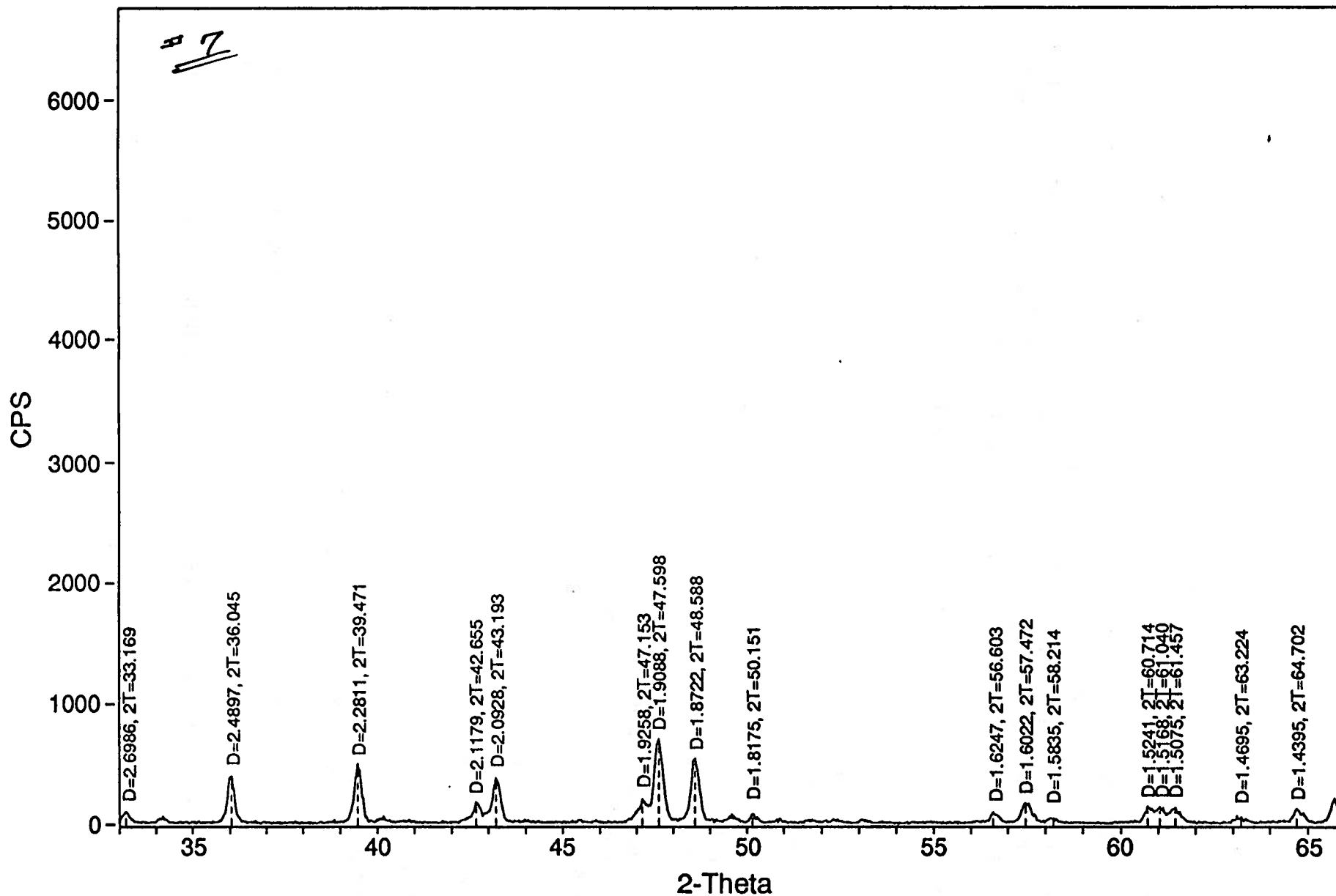












## APPENDIX 11.4.1

### Thermal Aquifer Model Miscellaneous

The thermal aquifer model in STARS 4.0.2 is a semi-analytical used to calculate the water and energy flow between the outflow boundary of the discretized region in the numerical simulation and an adjacent aquifer. This flow is perpendicular to the outflow boundary. Since the numerical simulation is isothermal in this study, only the water flow is considered here. The model assumes the pressure profile as

$$P(t,r) = (P_{ob} - P_{ref} + a r + b r^2) e^{-r/d} + P_{ref} \quad (A.1)$$

where

$$d = (\alpha t)^{0.5} / 2 \quad (A.2)$$

$$\alpha = (\phi \mu c) / k \quad (A.3)$$

- a: fitting parameter,
- b: fitting parameter,
- c: compressibility of water,
- d: diffusion length,
- k: absolute permeability,
- r: radial distance from outflow boundary,
- P: pressure,
- t: time,
- $\alpha$ : diffusion coefficient,
- $\phi$ : porosity,
- $\mu$ : viscosity of water.

subscripts:

- ob: value at outflow boundary,
- ref: reference value at infinitive radial distance.

Beside the physical properties of the aquifer, the only unknowns in Equation (A.1) are a and b.

For a fluid of small compressibility such as water, the governing flow equation in linear flow is:

$$\partial P / \partial t = \alpha (\partial^2 P / \partial r^2) \quad (A.4)$$

Equation (A.4) must be satisfied at the outflow boundary ( $r = 0$ ). Insertion of Equation (A.1) into Equation (A.4) with the derivative of pressure at  $r = 0$  together with a finite-difference discretization of the time derivative gives the first equation for solving  $a$  and  $b$ . The conservation of water flow can be satisfied by integrating Equation (A.4) from 0 to infinity assuming  $\alpha$  as a constant. This gives the second equation for solving  $a$  and  $b$ .

The rate per unit area at which water flows from the outflow boundary is:

$$-\lambda \left( \frac{\partial P}{\partial r} \right) \Big|_{r=0} = -\lambda \left( a - P_{ob} / d \right) \quad (\text{A.5})$$

where  $\lambda$  is the fluid transmissibility and is defined as:

$$\lambda = k / \mu \quad (\text{A.6})$$

**APPENDIX 11.5.a**

**Graphs Generated from PATH.UBC output**

### Figure 11.5.1

Reaction of Brackish Formation Water with  $\text{CO}_2$  at  $25^\circ\text{C}$  as it is injected into the aquifer; plotted as a function of time ('X').

- a: Buildup of the partial pressure of  $\text{CO}_2$  in bars.
- b: Molar amount of  $\text{CO}_2$  injected into the aquifer.
- c: Change in the molality of the aqueous species.

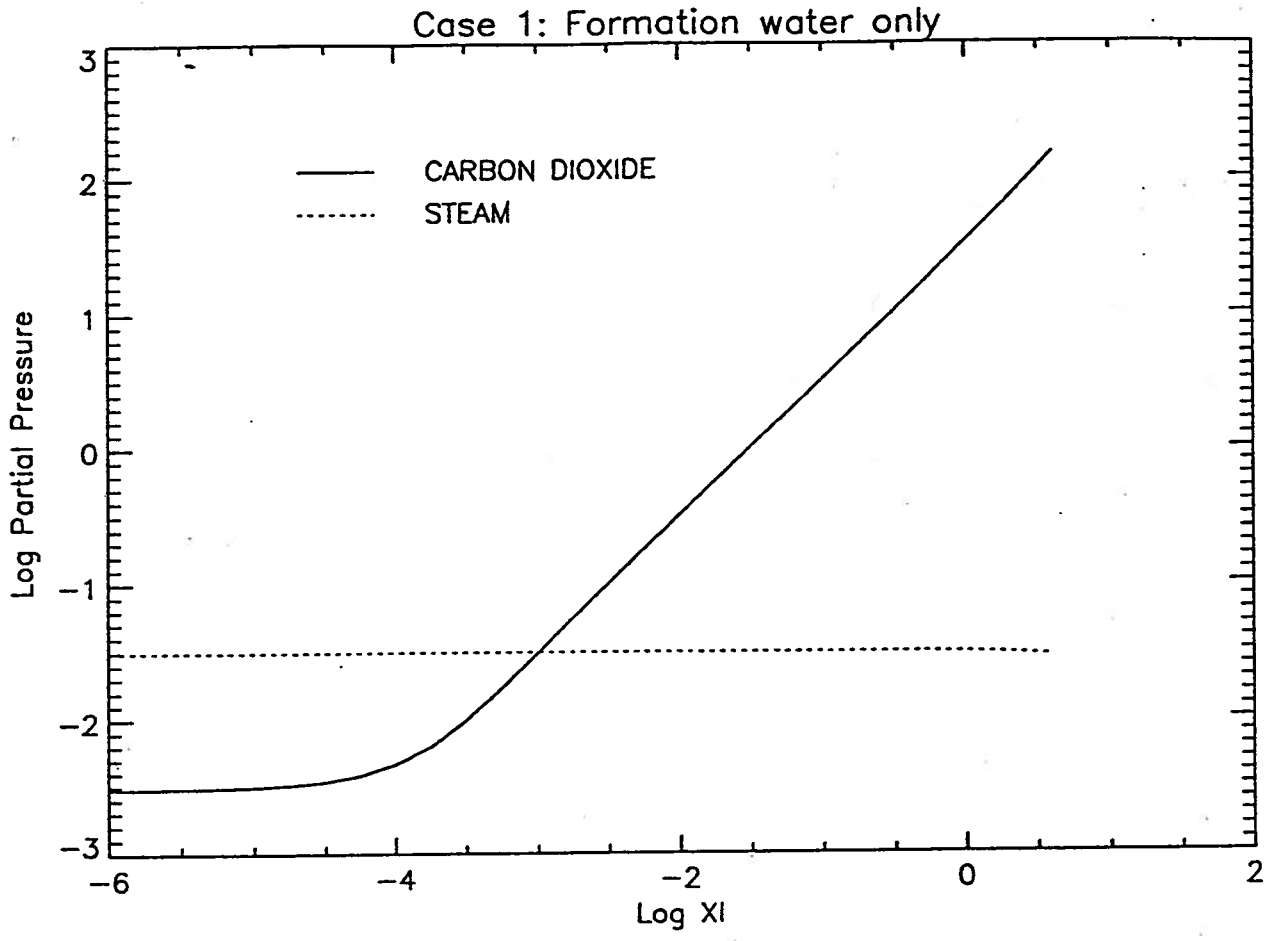


Figure 11.5.1a

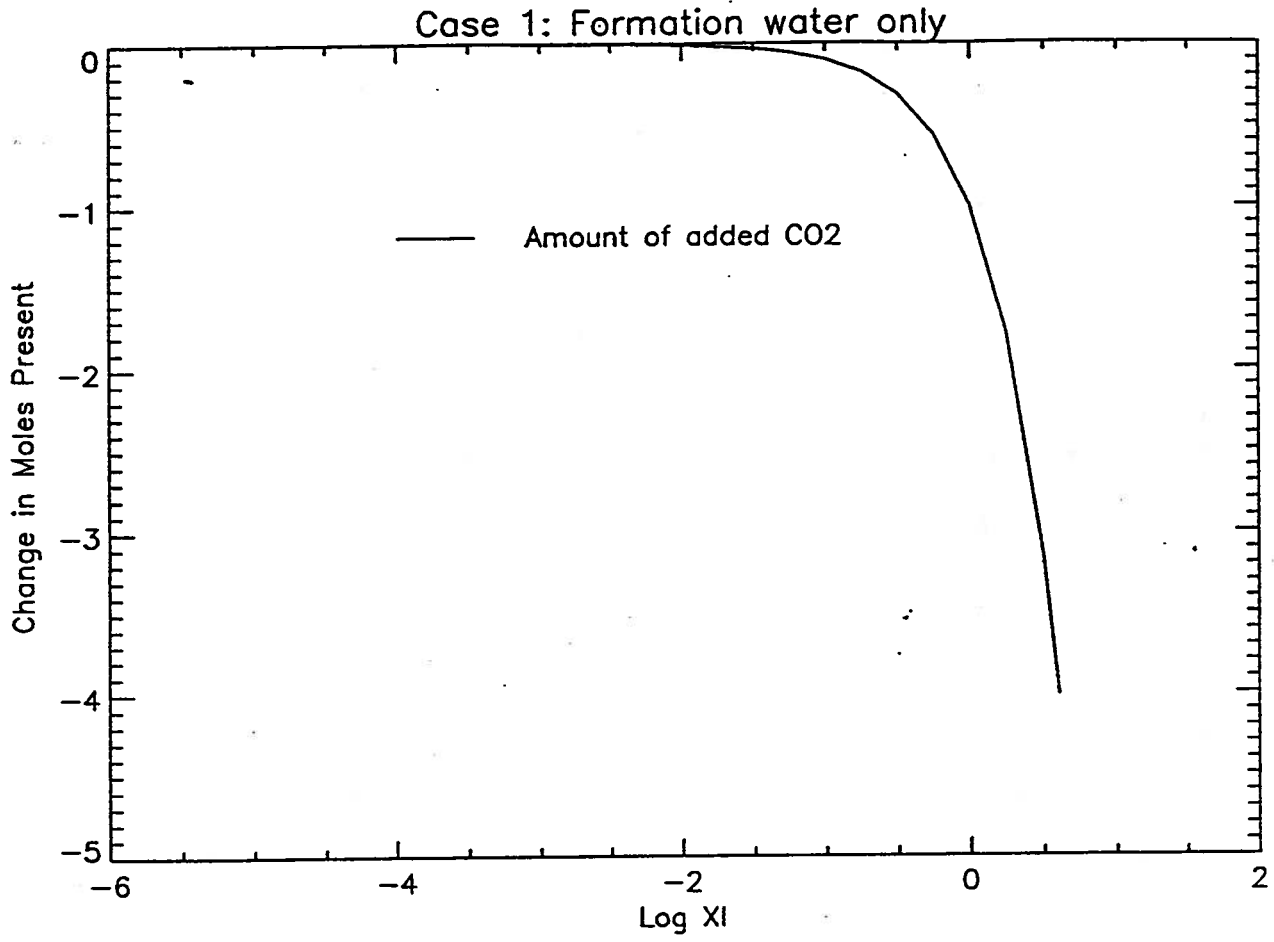


Figure 11.5.1b

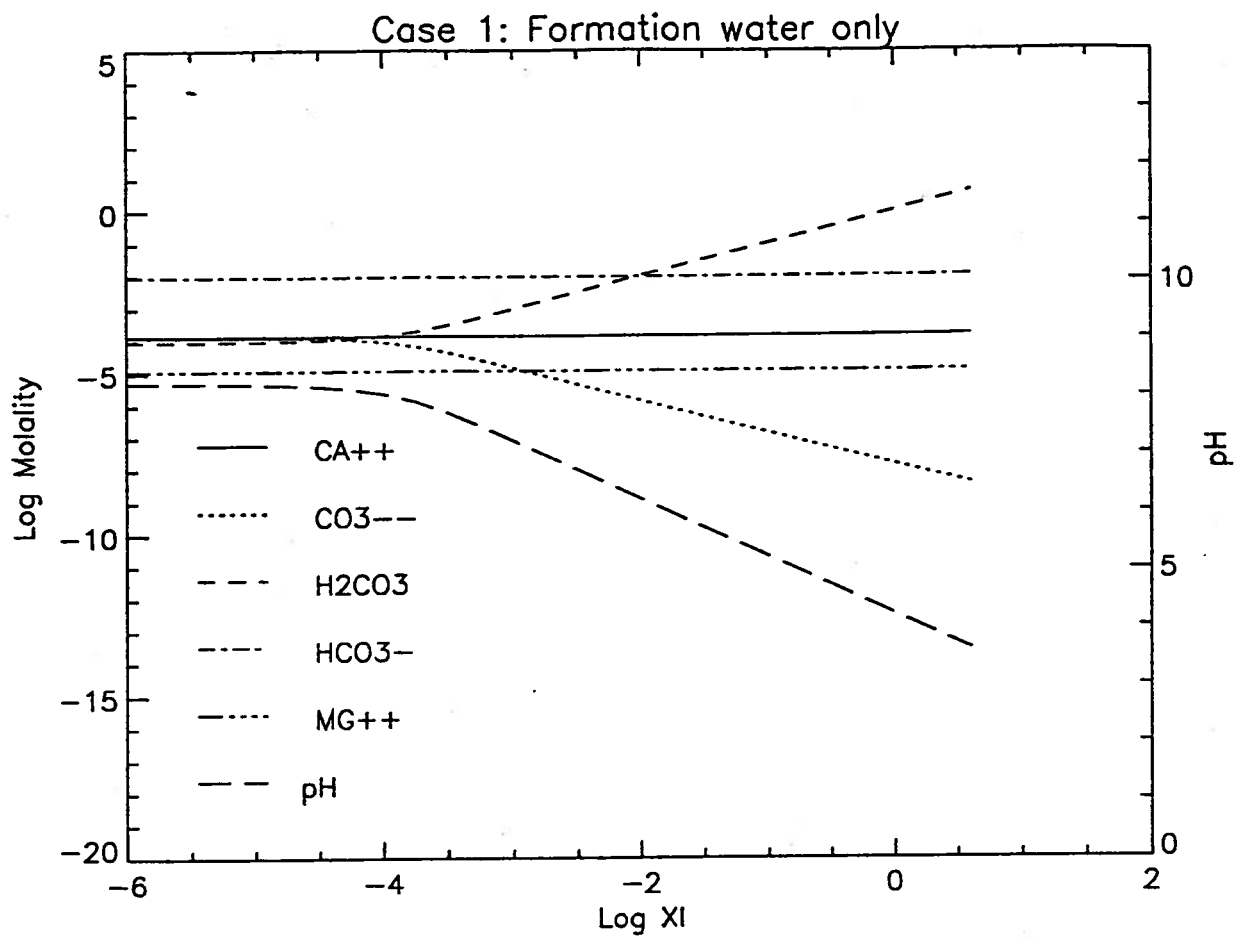


Figure 11.5.1c



### Figure 11.5.2

Reaction of a Formation Water Brine with  $\text{CO}_2$  at  $25^\circ\text{C}$  as it is injected into the aquifer; plotted as a function of time ('XI').

- a: Buildup of the partial pressure of  $\text{CO}_2$  in bars.
- b: Molar amount of  $\text{CO}_2$  injected into the aquifer.
- c: Change in the molality of the aqueous species.

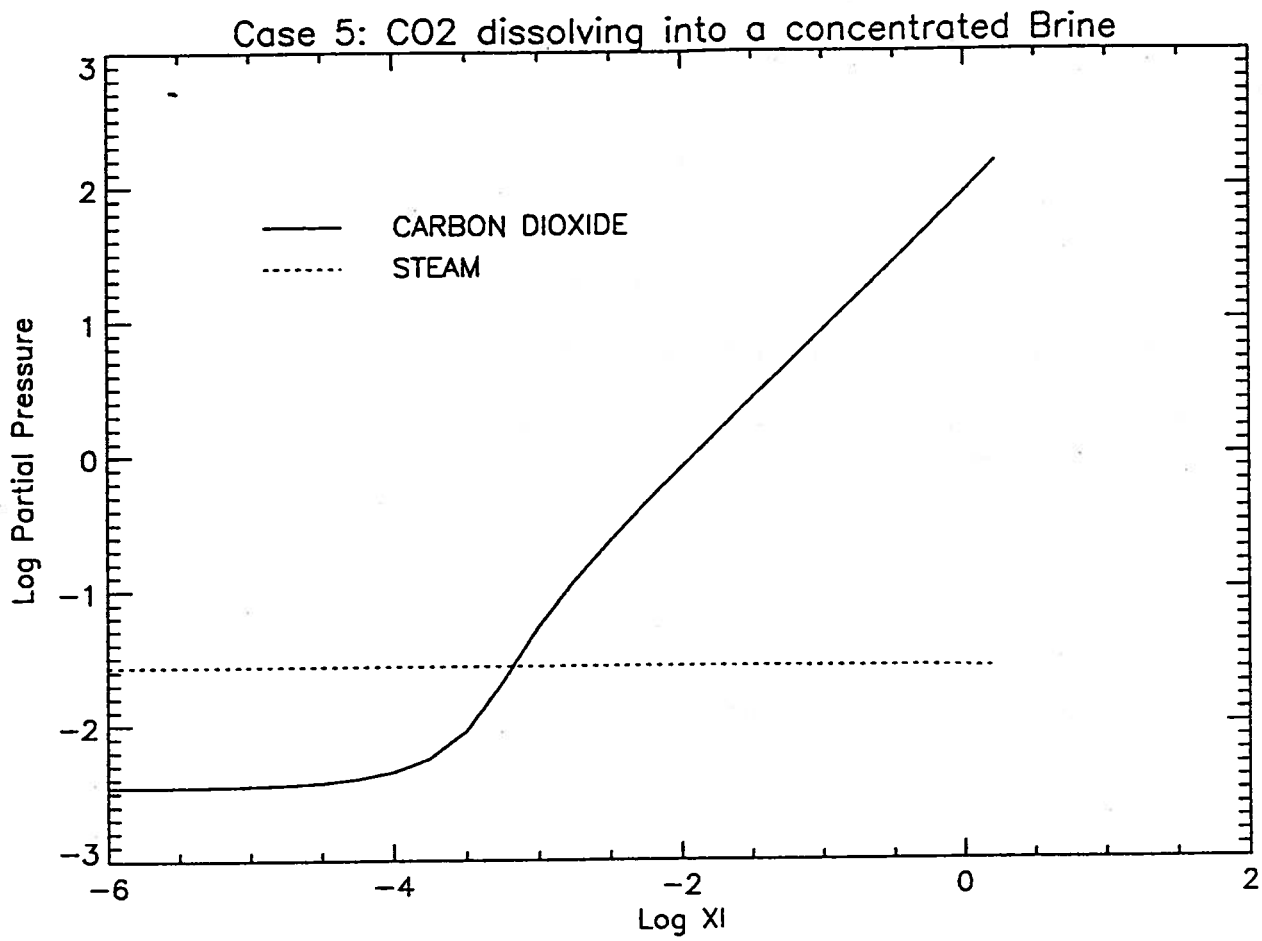


Figure 11.5.2a

Case 5: CO2 dissolving into a concentrated Brine

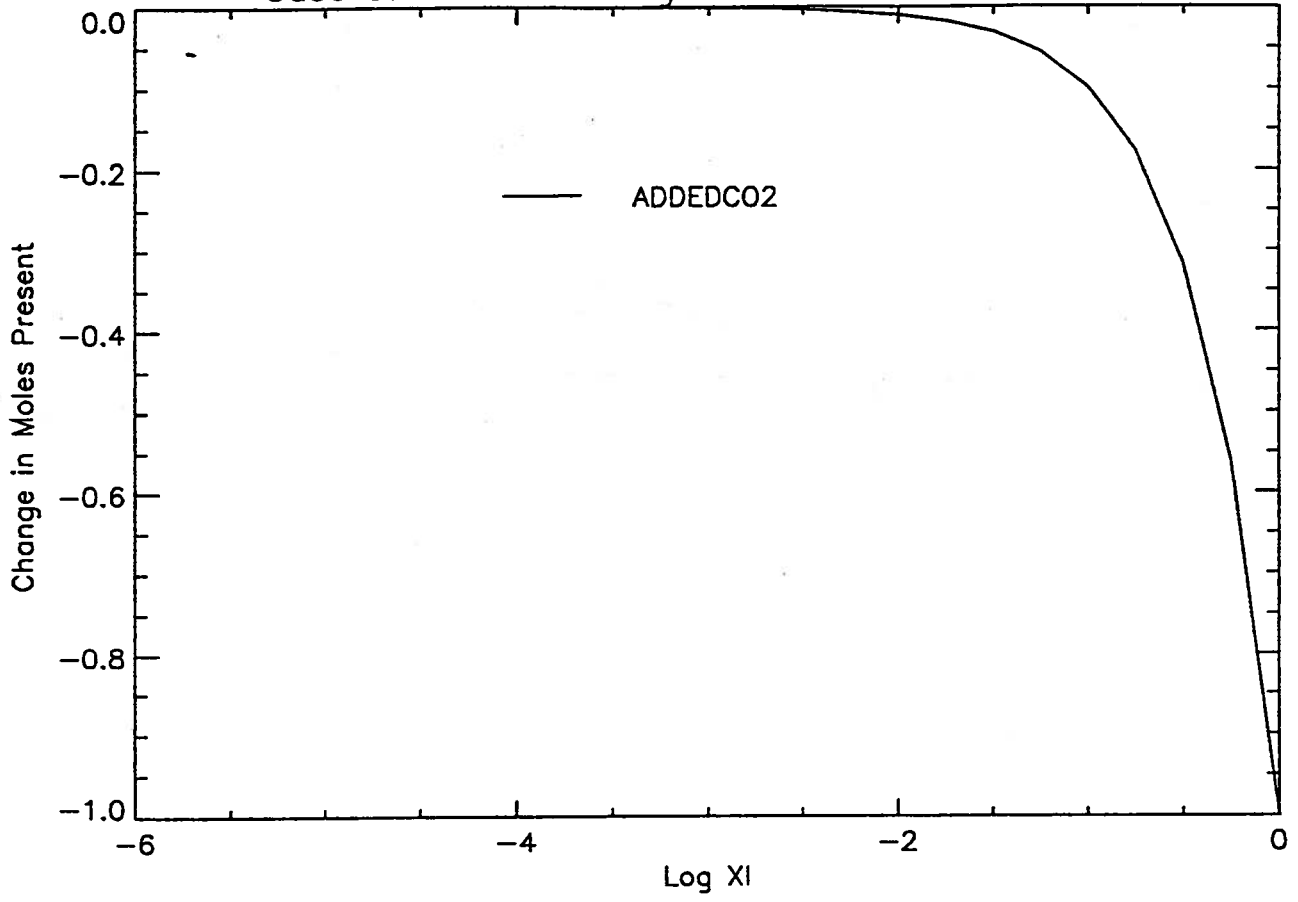


Figure 11.5.2b

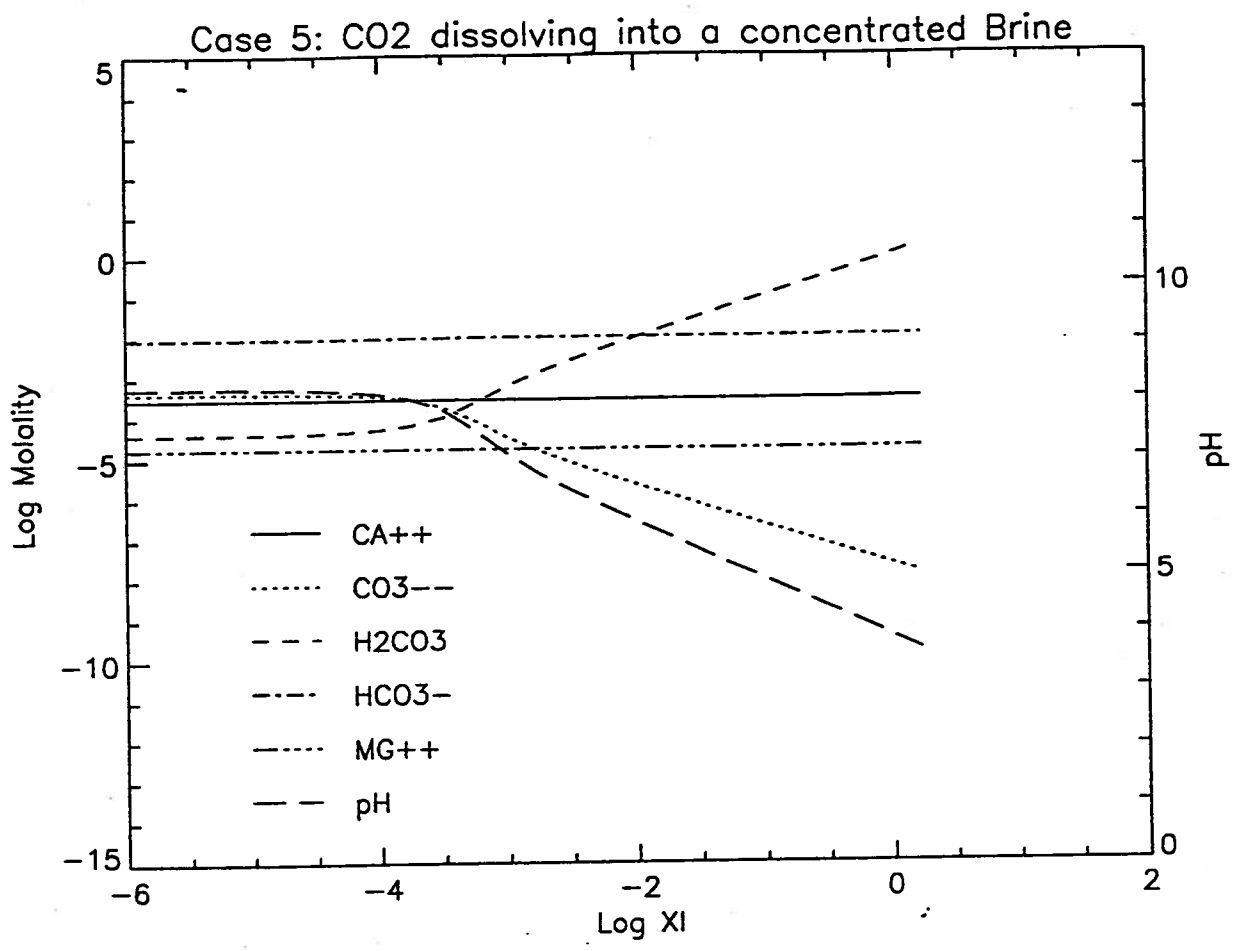


Figure 11.5.2c

### Figure 11.5.3

Reaction of Brackish Formation Water with a calcite-dolomite limestone aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').

- a: Buildup of the partial pressure of CO<sub>2</sub> in bars.
- b1: Molar amount of CO<sub>2</sub> injected into the aquifer.
- b2: Change in the moles of mineral reactants.
- c: Change in the molality of the aqueous species.

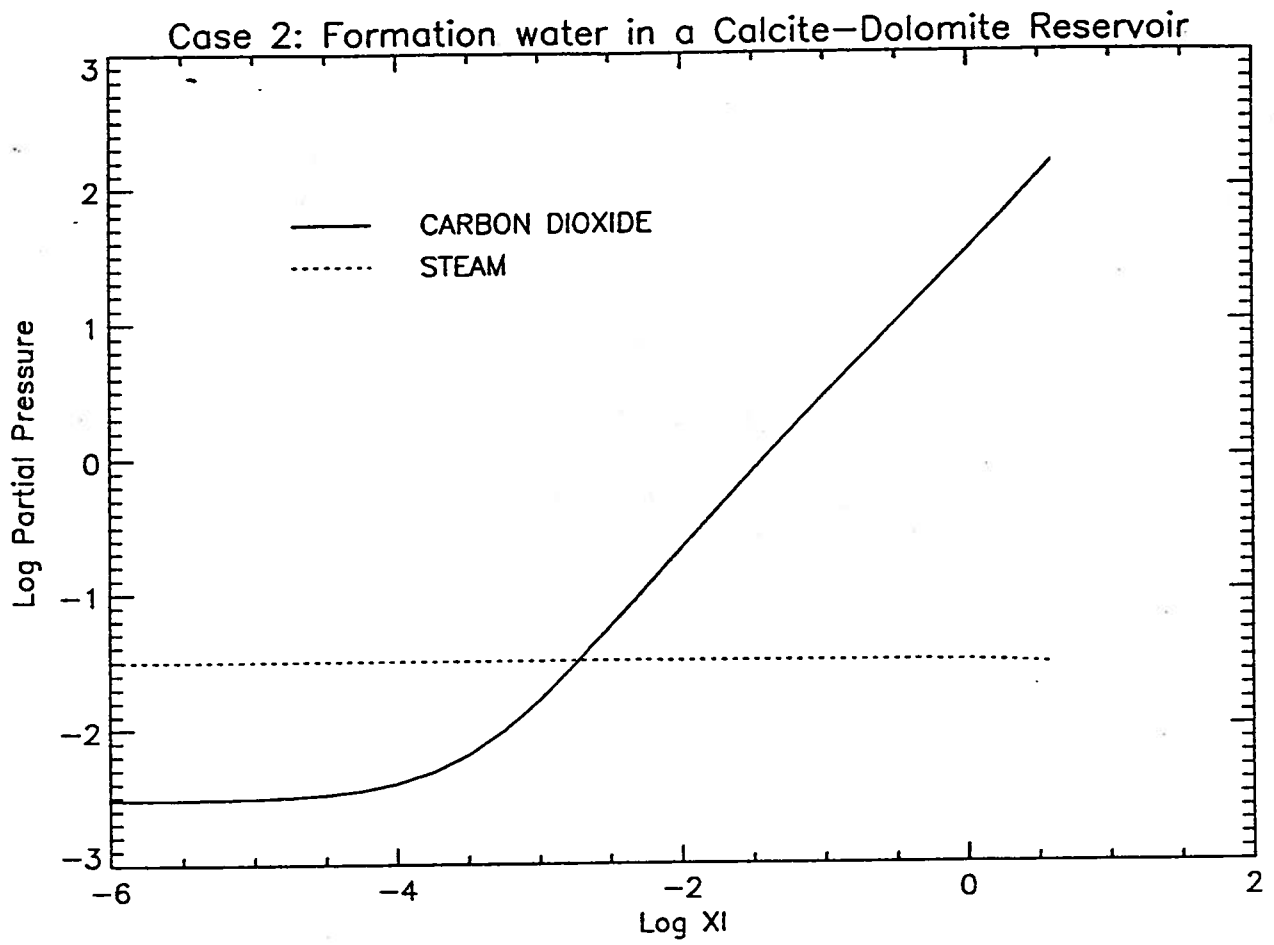


Figure 11.5.3a

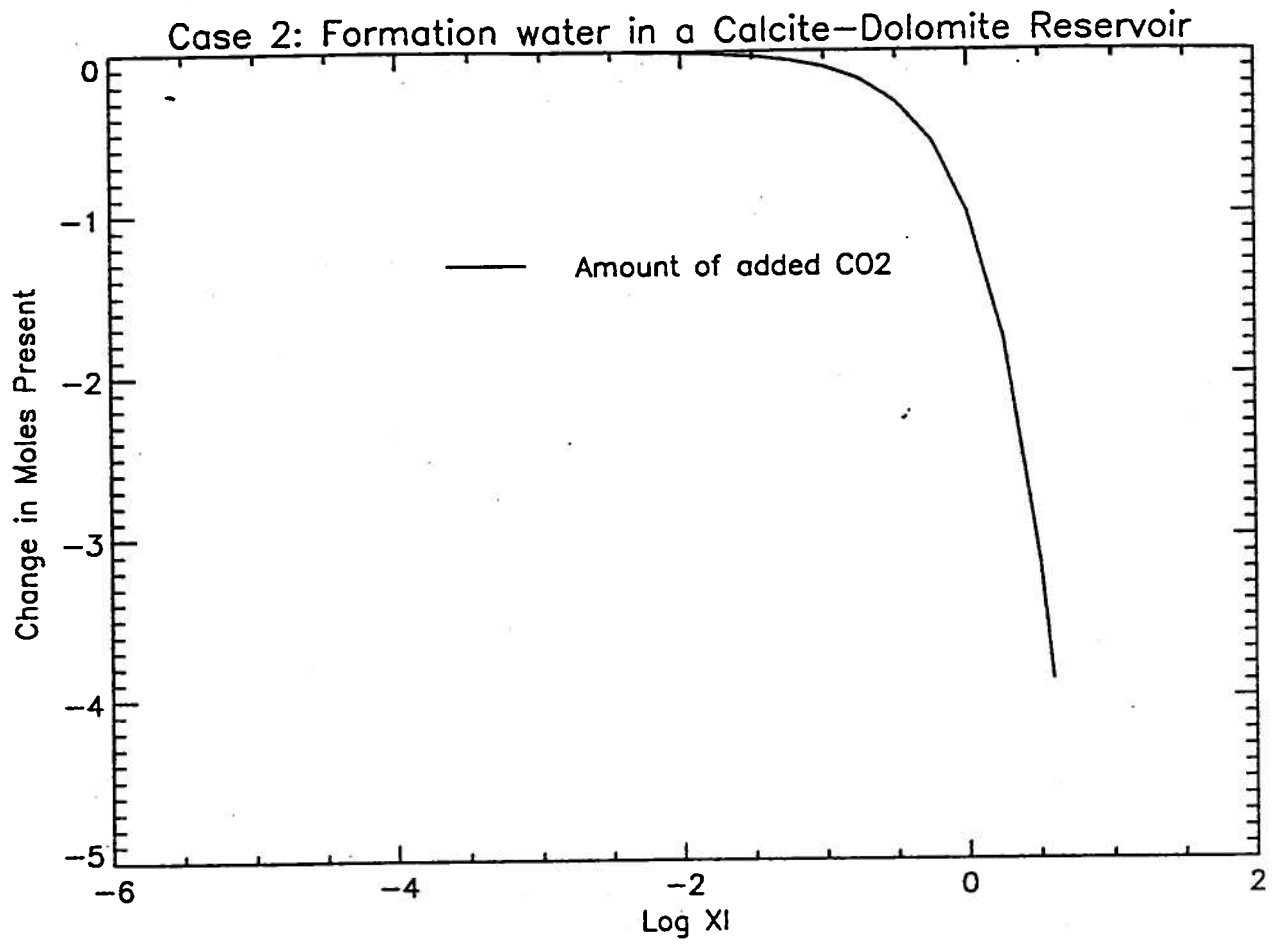


Figure 11.5.3b1

Case 2: Formation water in a Calcite-Dolomite Reservoir

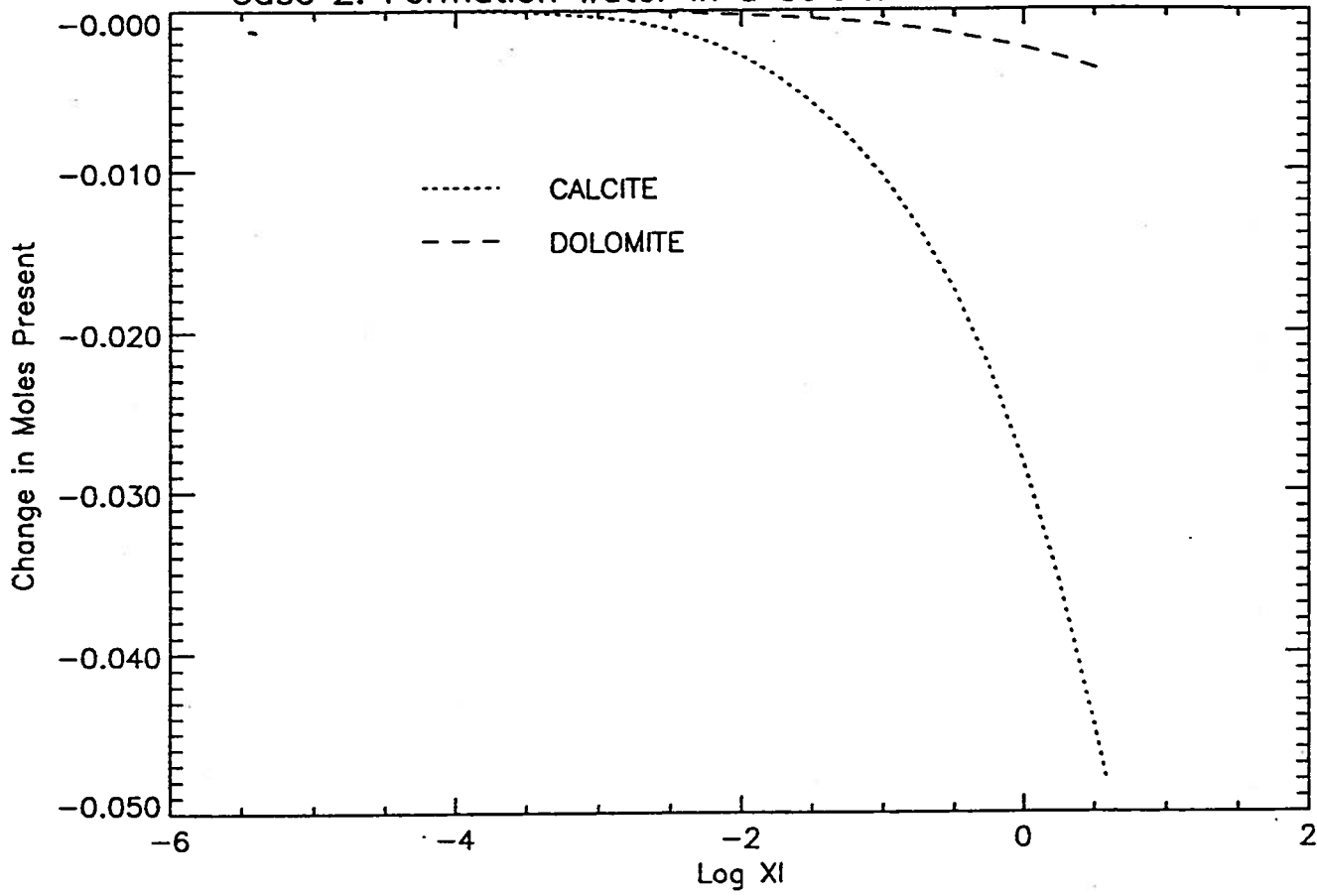


Figure 11.5.3b2



Case 2: Formation water in a Calcite-Dolomite Reservoir

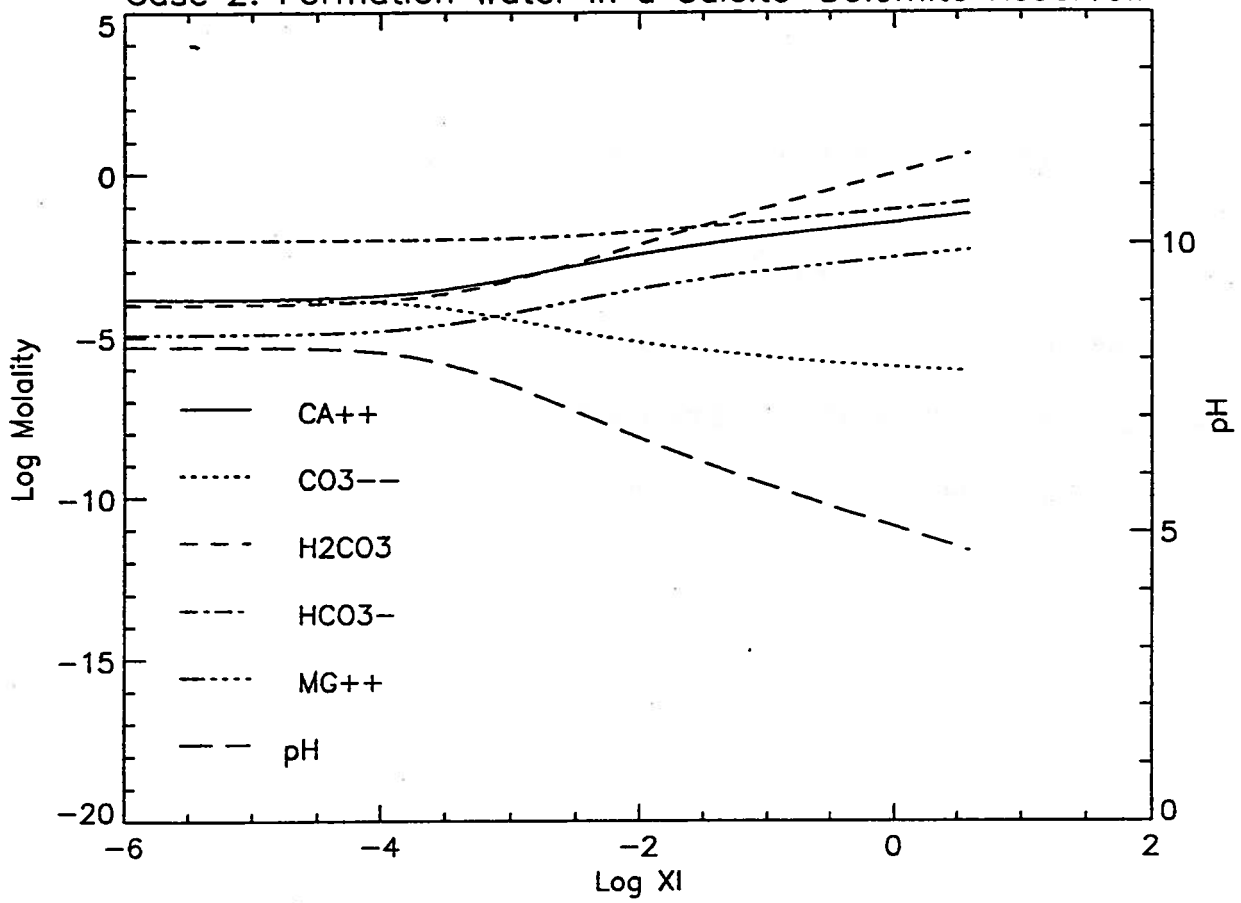


Figure 11.5.3c

### Figure 11.5.4

Reaction of Brackish Formation Water with a calcite-dolomite-quartz limestone aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').

- a: Buildup of the partial pressure of CO<sub>2</sub> in bars.
- b1: Molar amount of CO<sub>2</sub> injected into the aquifer.
- b2: Change in the moles of mineral reactants.
- c: Change in the molality of the aqueous species.

Case 8: Calcite, Dolomite, Quartz Reservoir

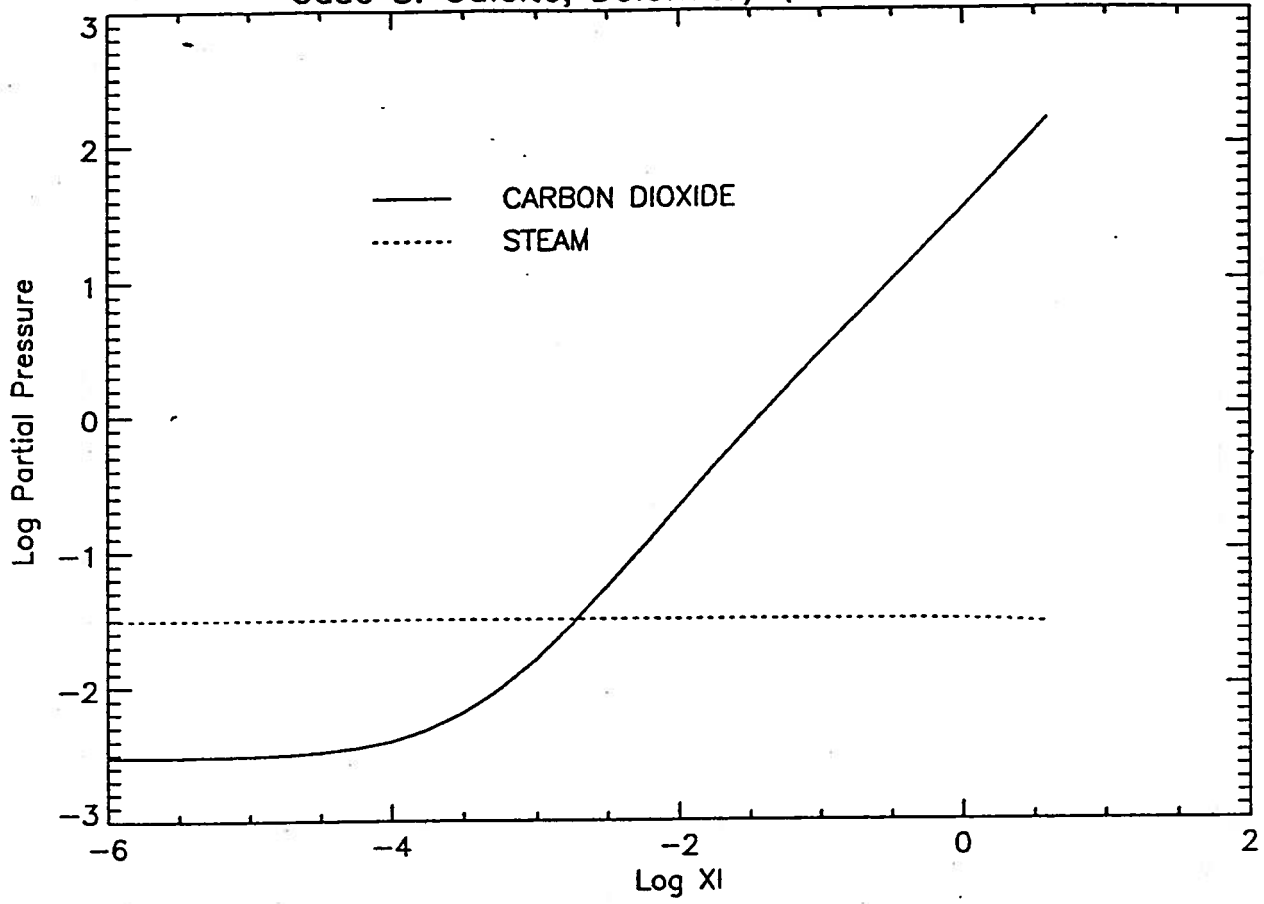


Figure 11.5.4a

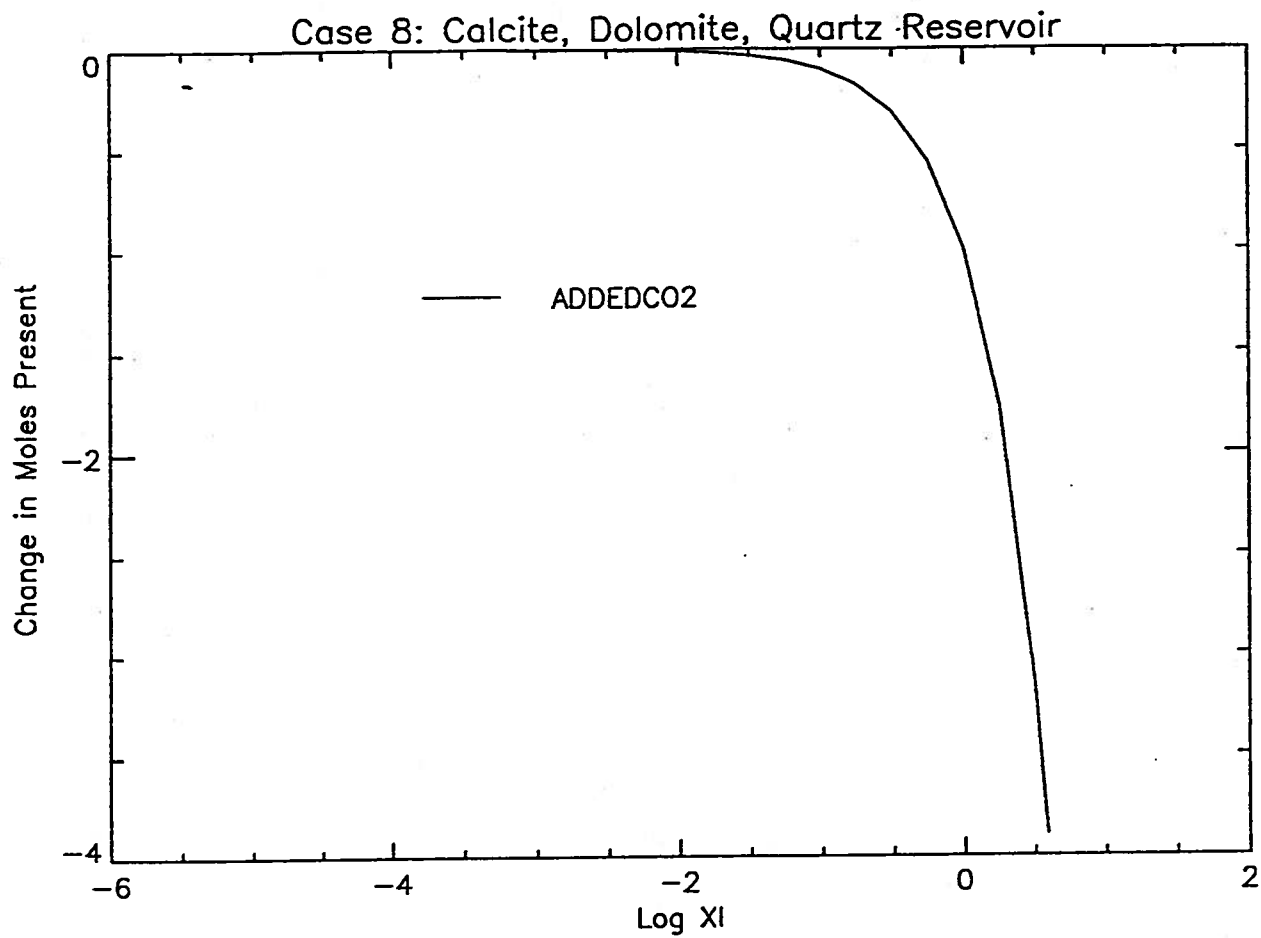


Figure 11.5.4b1

Case 8: Calcite, Dolomite, Quartz Reservoir

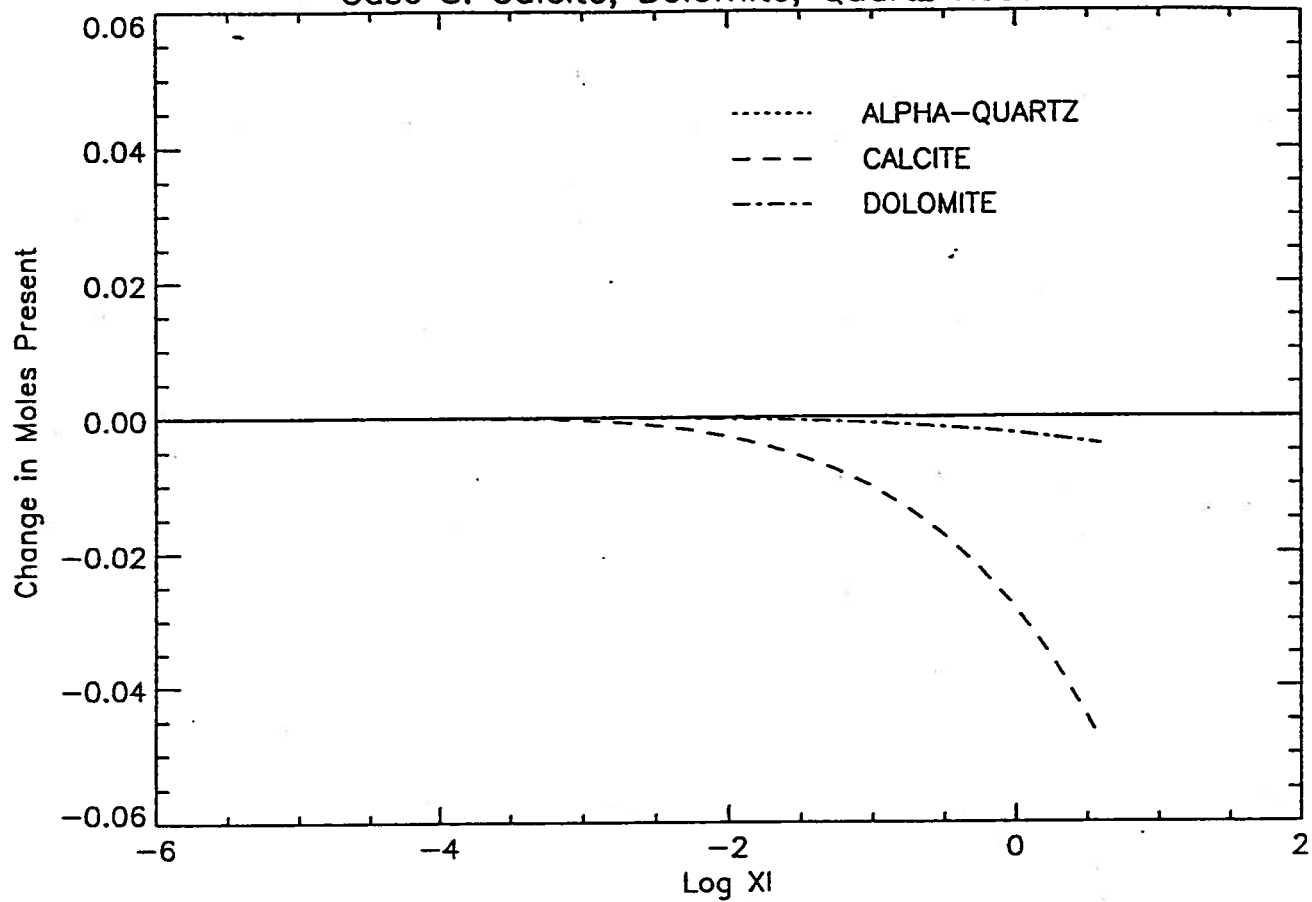


Figure 11.5.4b2

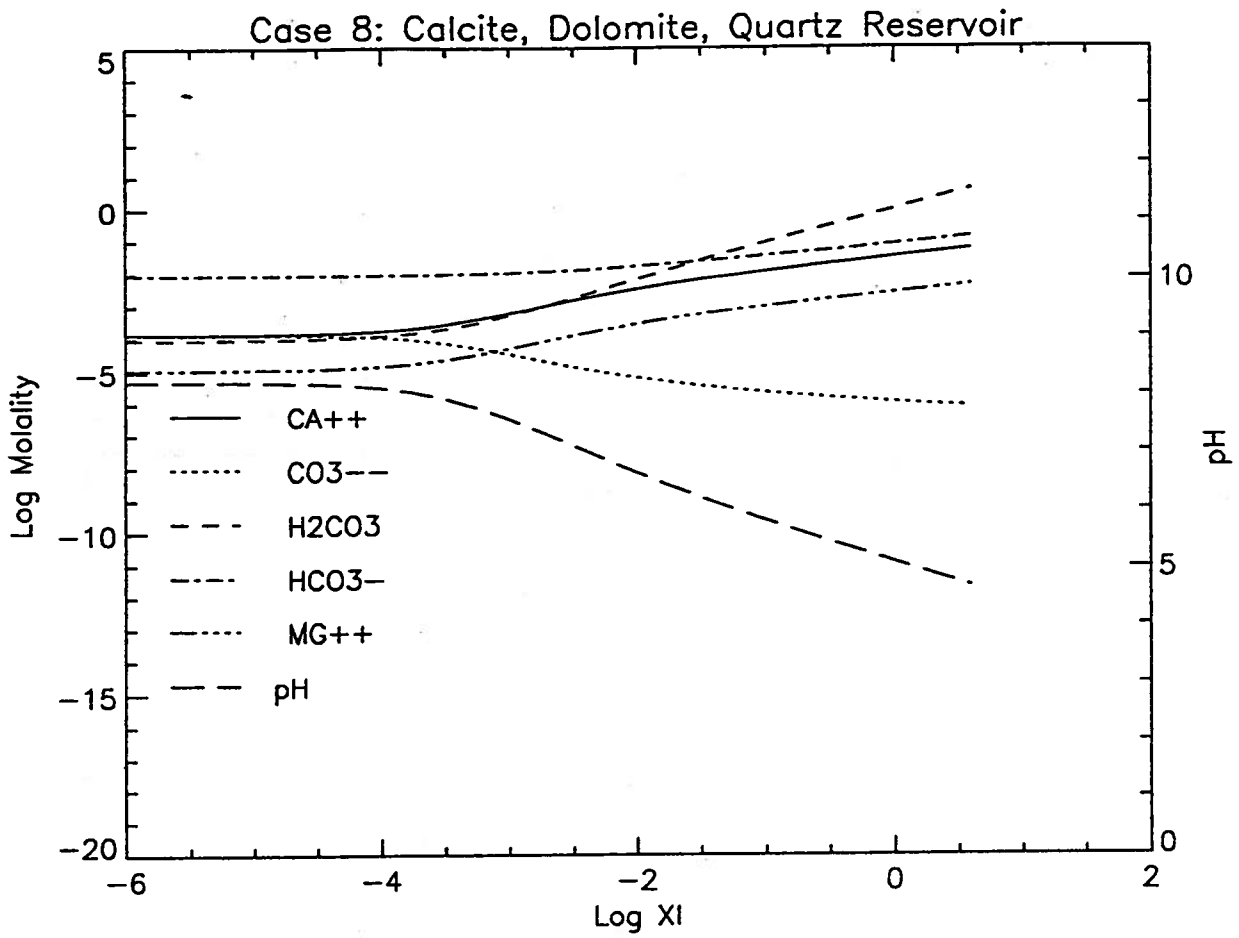


Figure 11.5.4c

### **Figure 11.5.5**

Reaction of a Formation Water Brine with a calcite-dolomite limestone aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').

a: Buildup of the partial pressure of CO<sub>2</sub> in bars.

b1: Molar amount of CO<sub>2</sub> injected into the aquifer.

b2: Change in the moles of mineral reactants.

c: Change in the molality of the aqueous species.

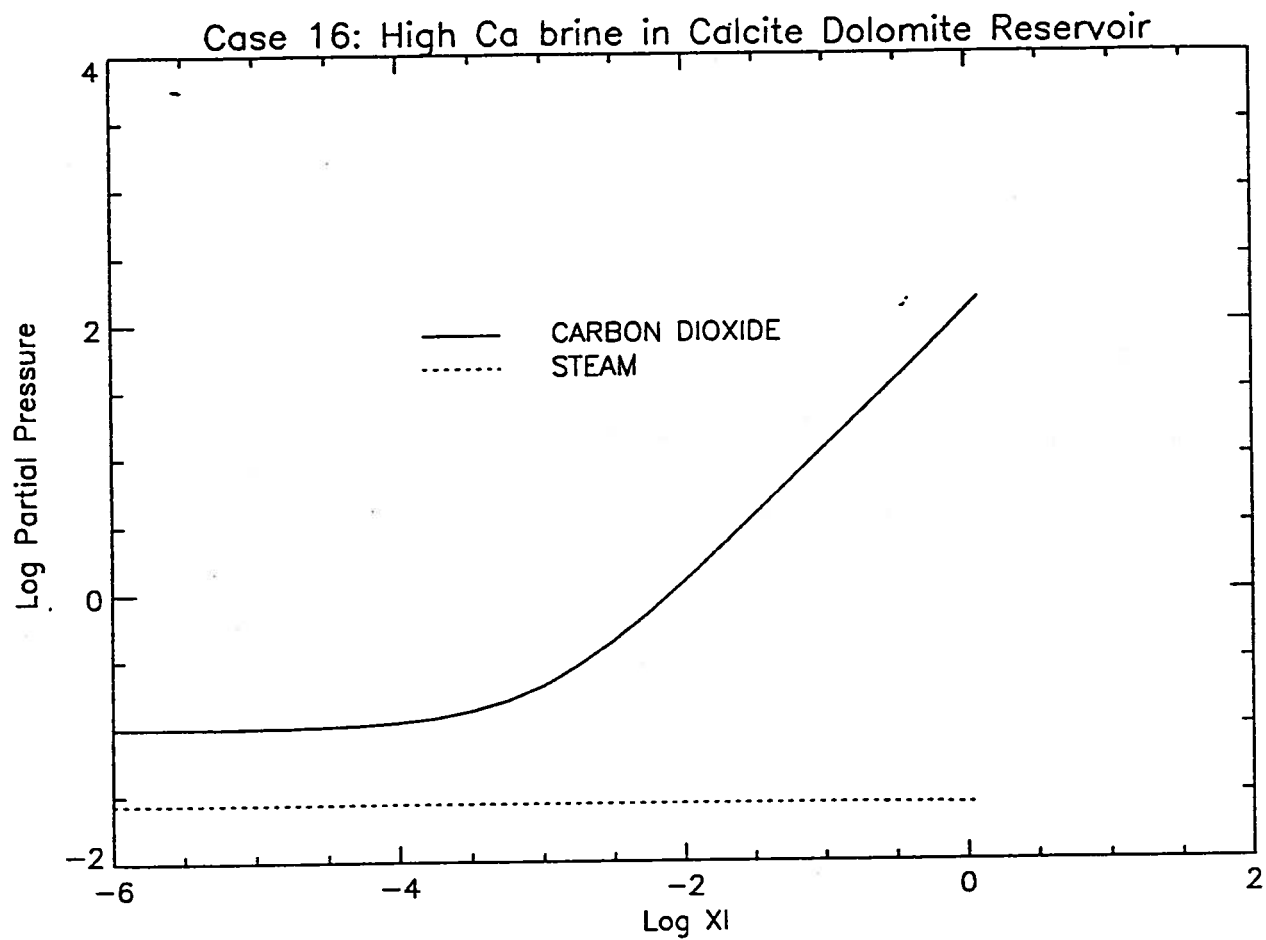


Figure 11.5.5a



Case 16: High Ca brine in Calcite Dolomite Reservoir

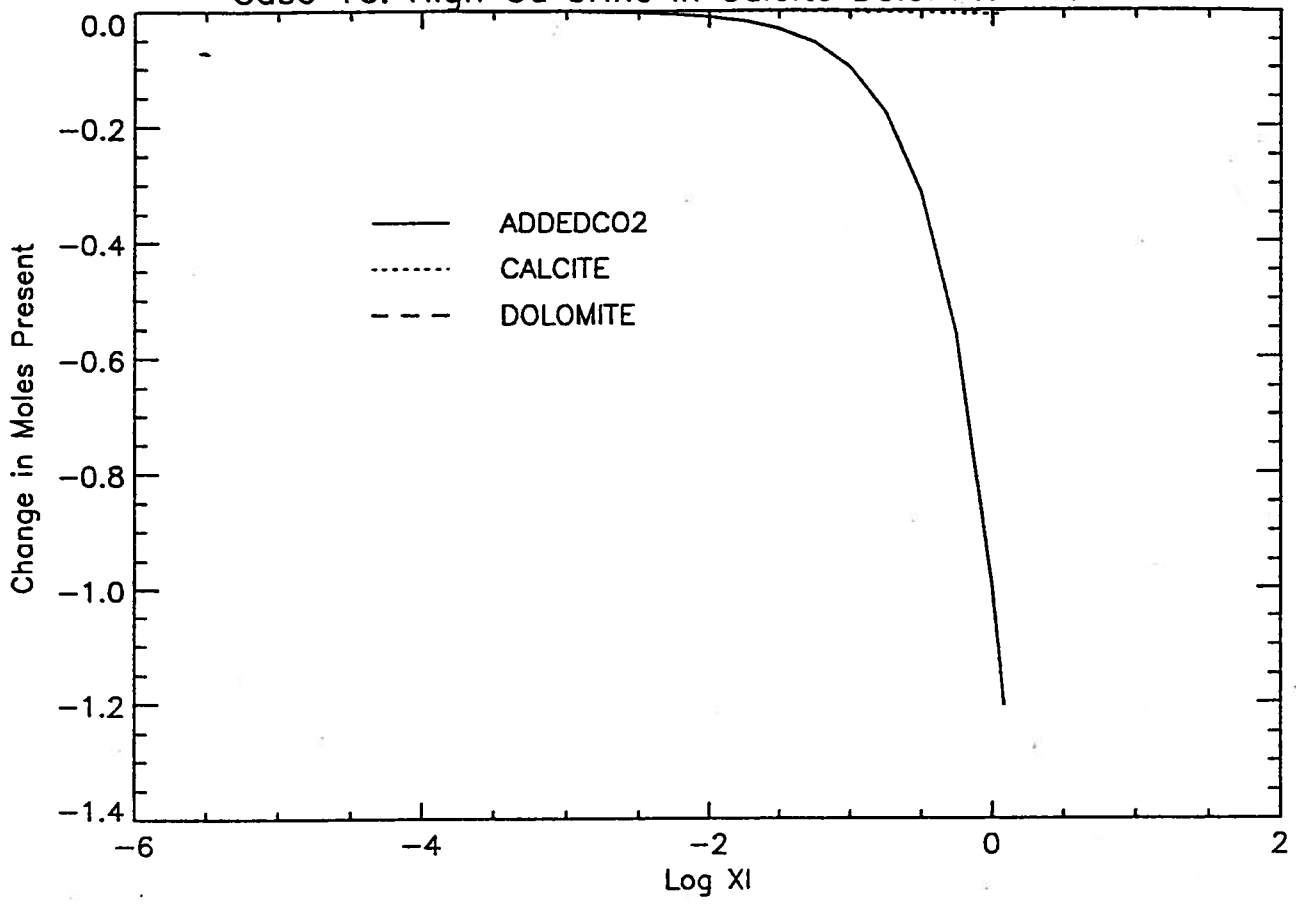


Figure 11.5.5b1

Case 16: High Ca brine in Calcite Dolomite Reservoir

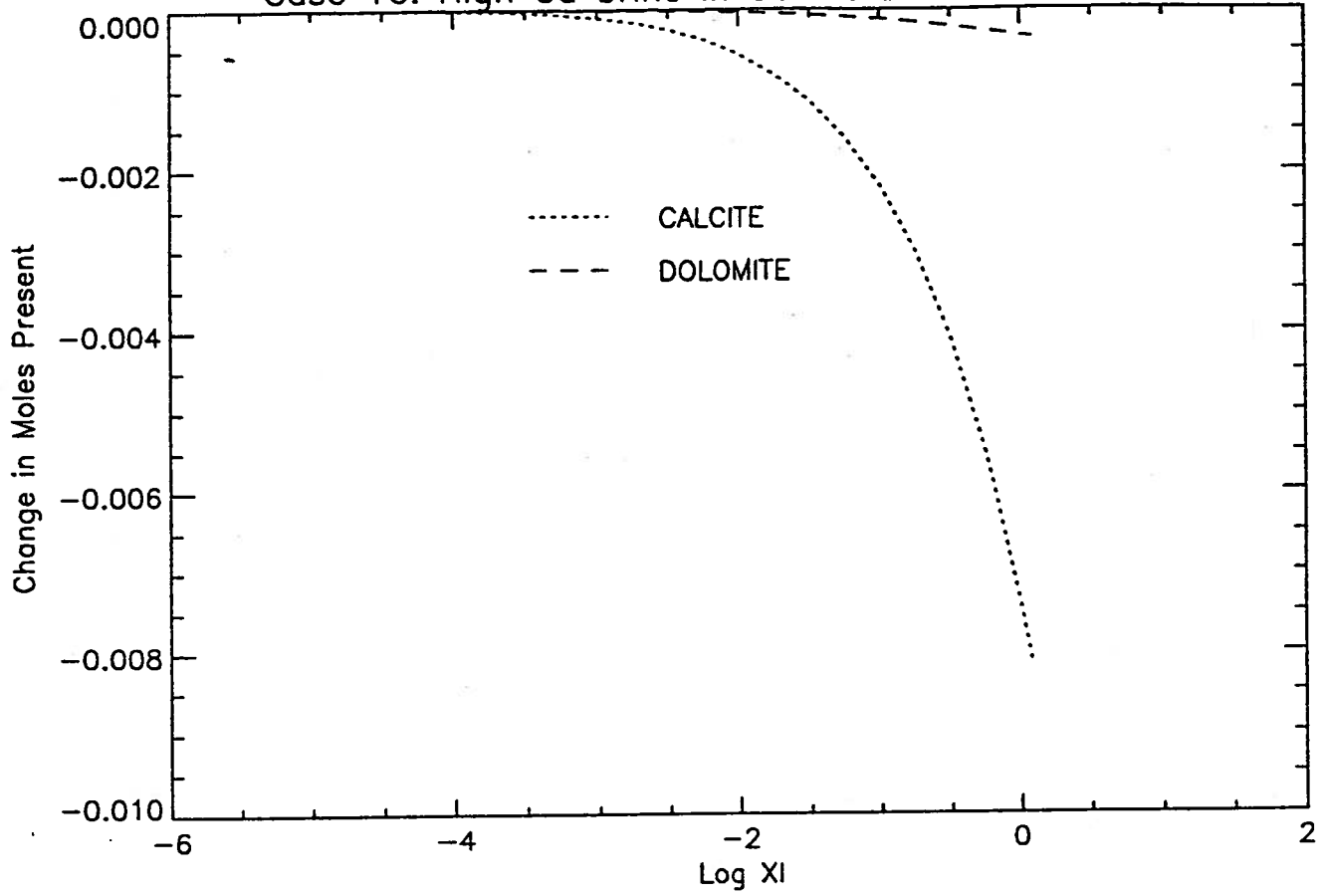


Figure 11.5.5b2

Case 16: High Ca brine in Calcite Dolomite Reservoir

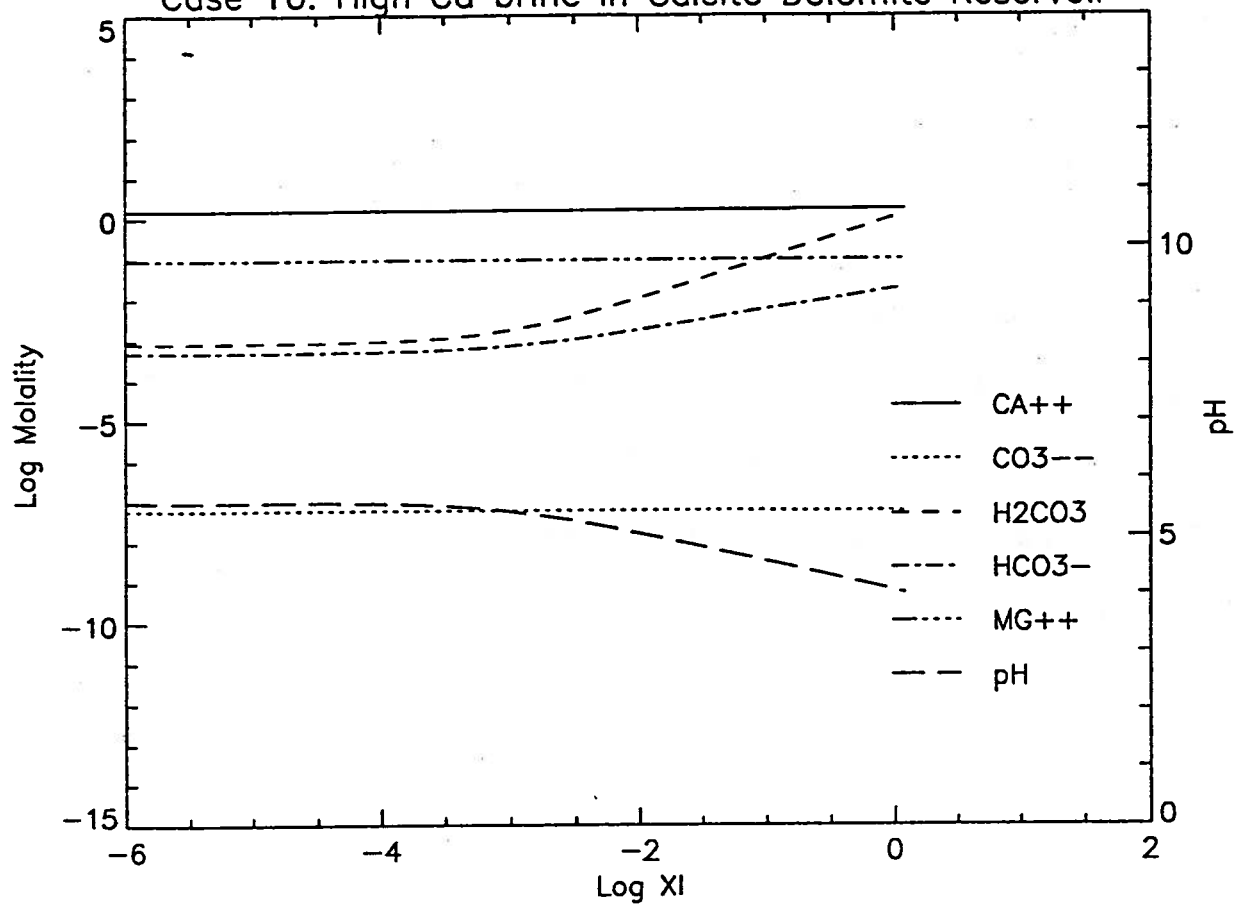


Figure 11.5.5c

### Figure 11.5.6

Reaction of Brackish Formation Water with a calcite-dolomite-clay exchanger limestone aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').

- a: Buildup of the partial pressure of CO<sub>2</sub> in bars.
- b1: Molar amount of CO<sub>2</sub> injected into the aquifer.
- b2: Change in the moles of mineral reactants.
- c1: Change in the molality of the aqueous species.
- c2: Change in the composition of the clay exchanger.

Case 15: Calcite Dolomite Reservoir with Ion Exchange

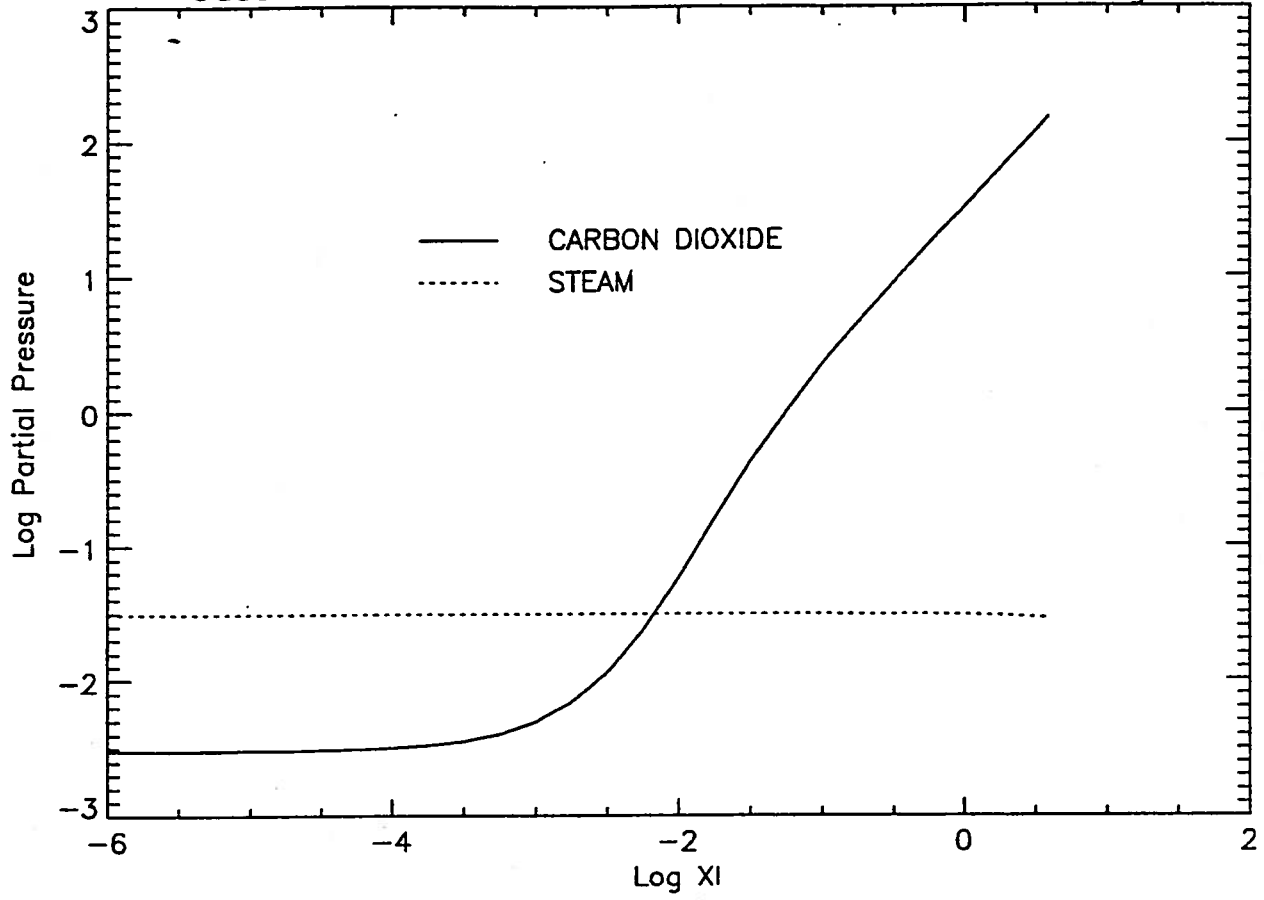


Figure 11.5.6a

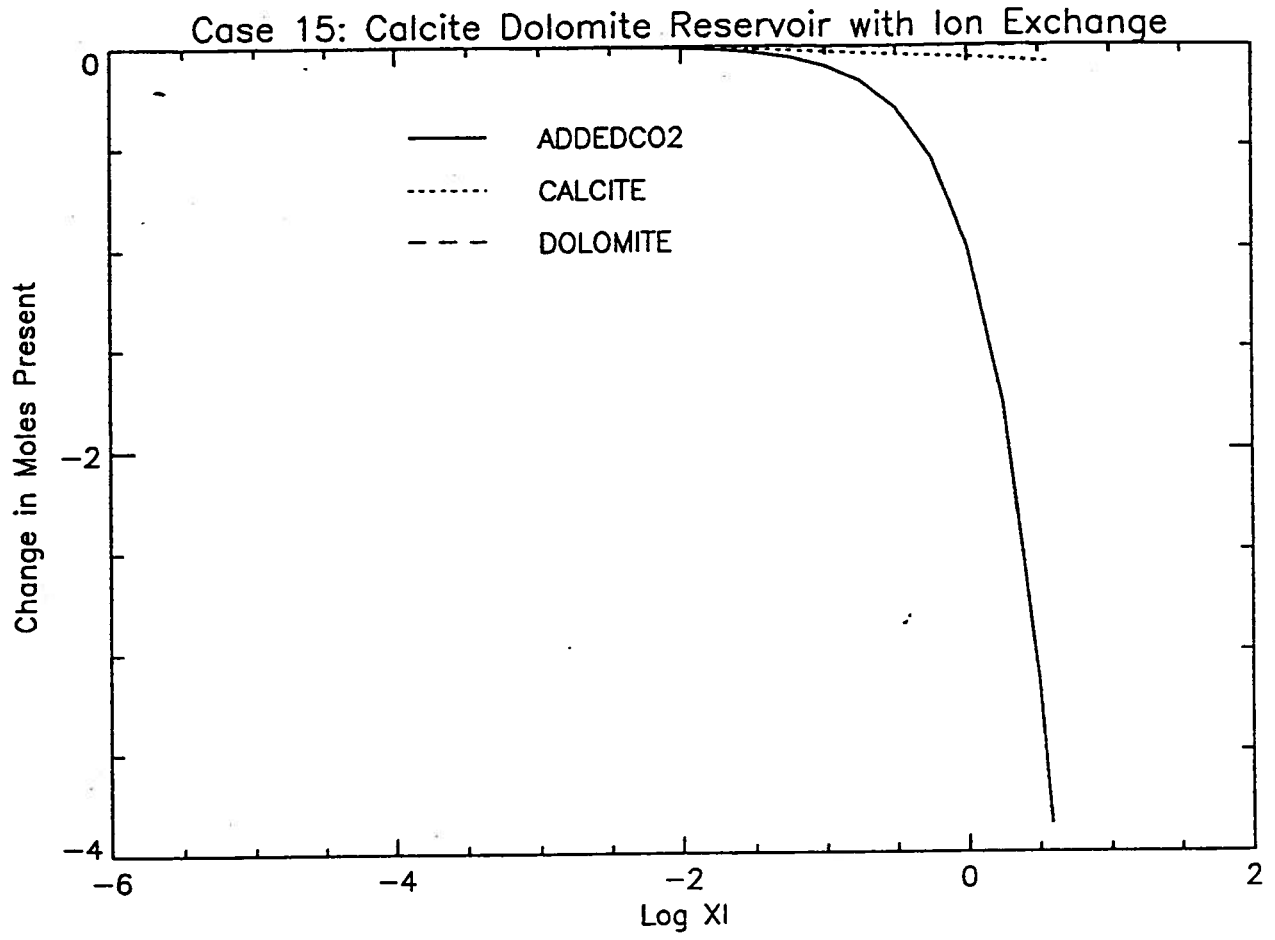


Figure 11.5.6b1

Case 15: Calcite Dolomite Reservoir with Ion Exchange

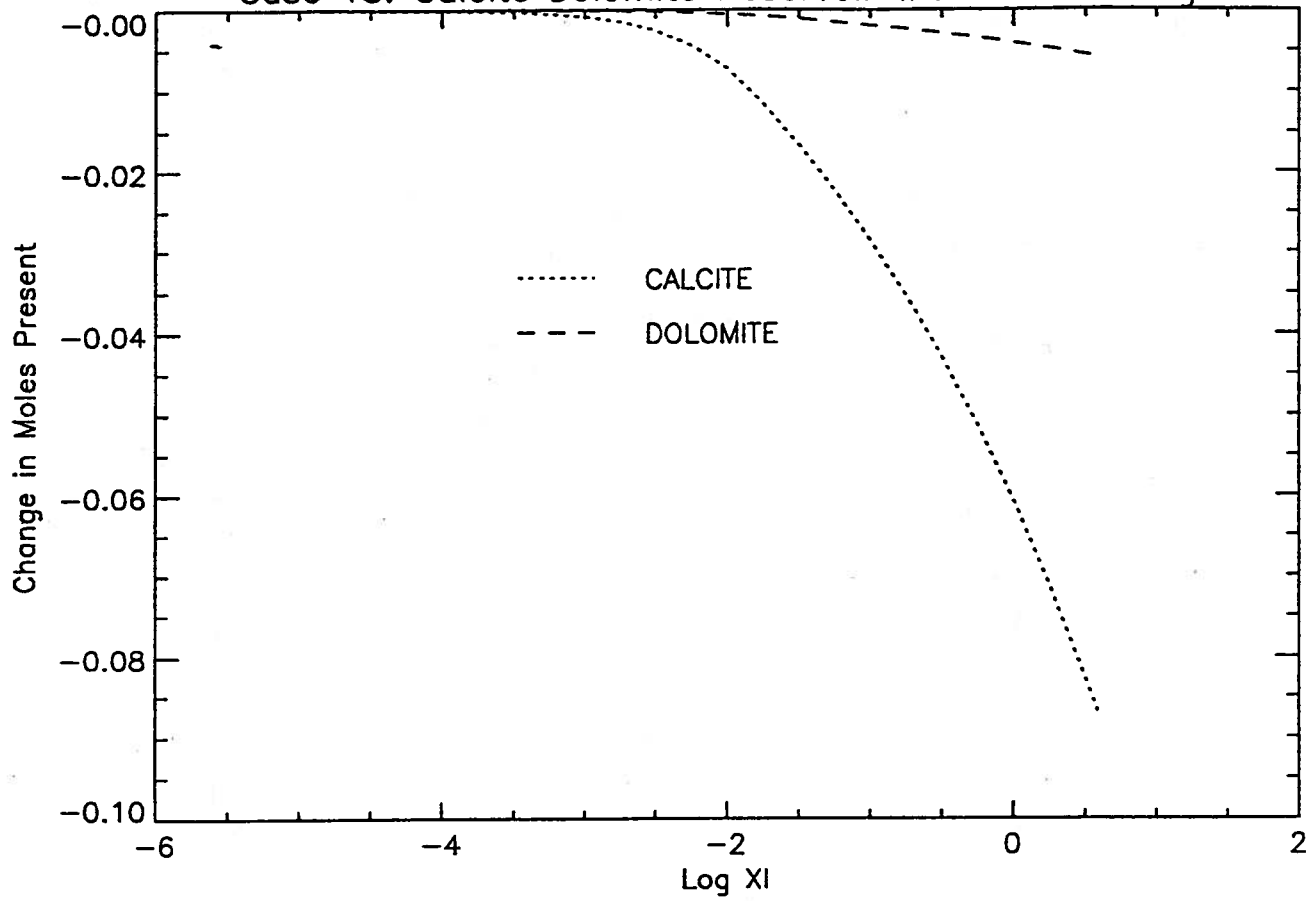


Figure 11.5.6b2

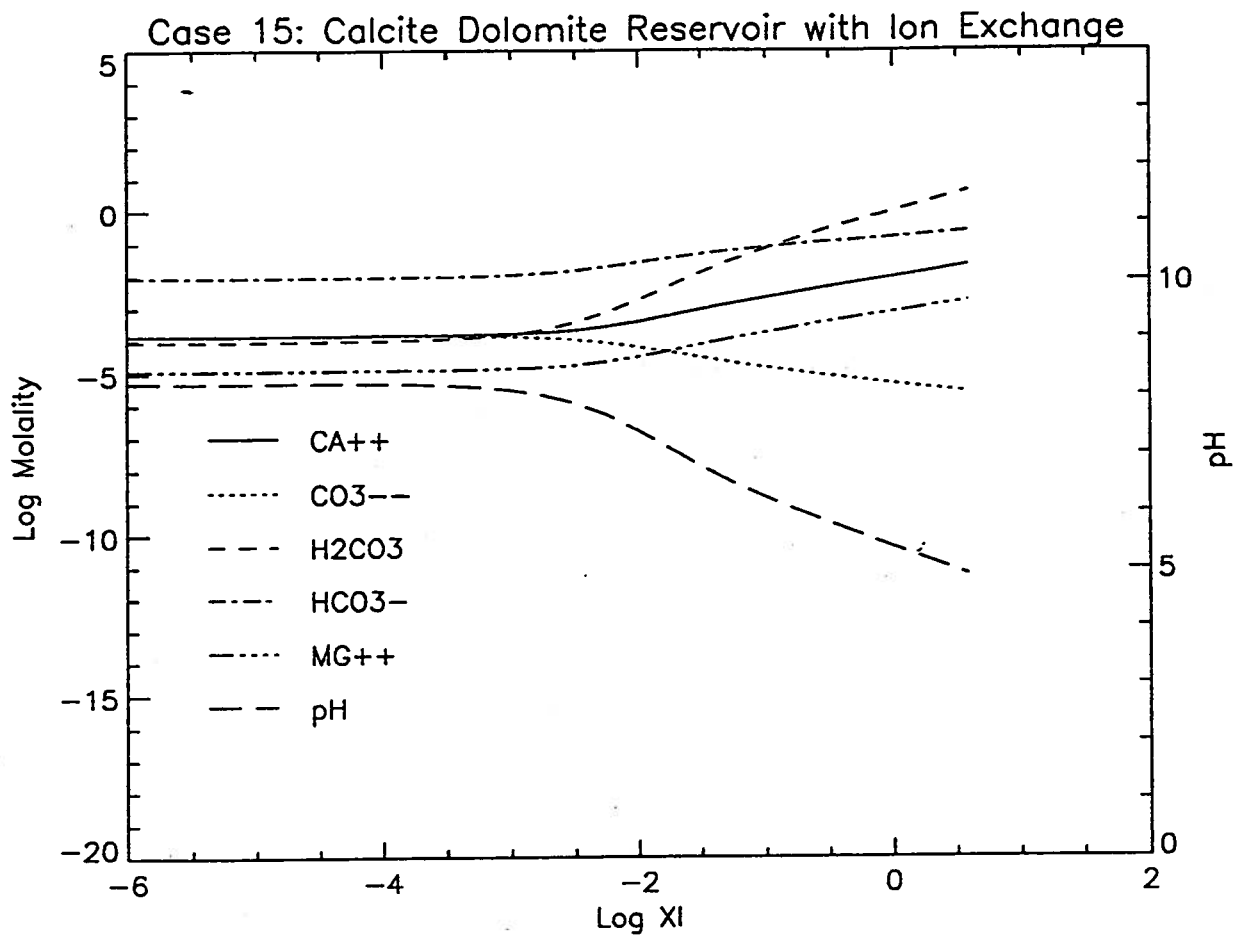


Figure 11.6c1



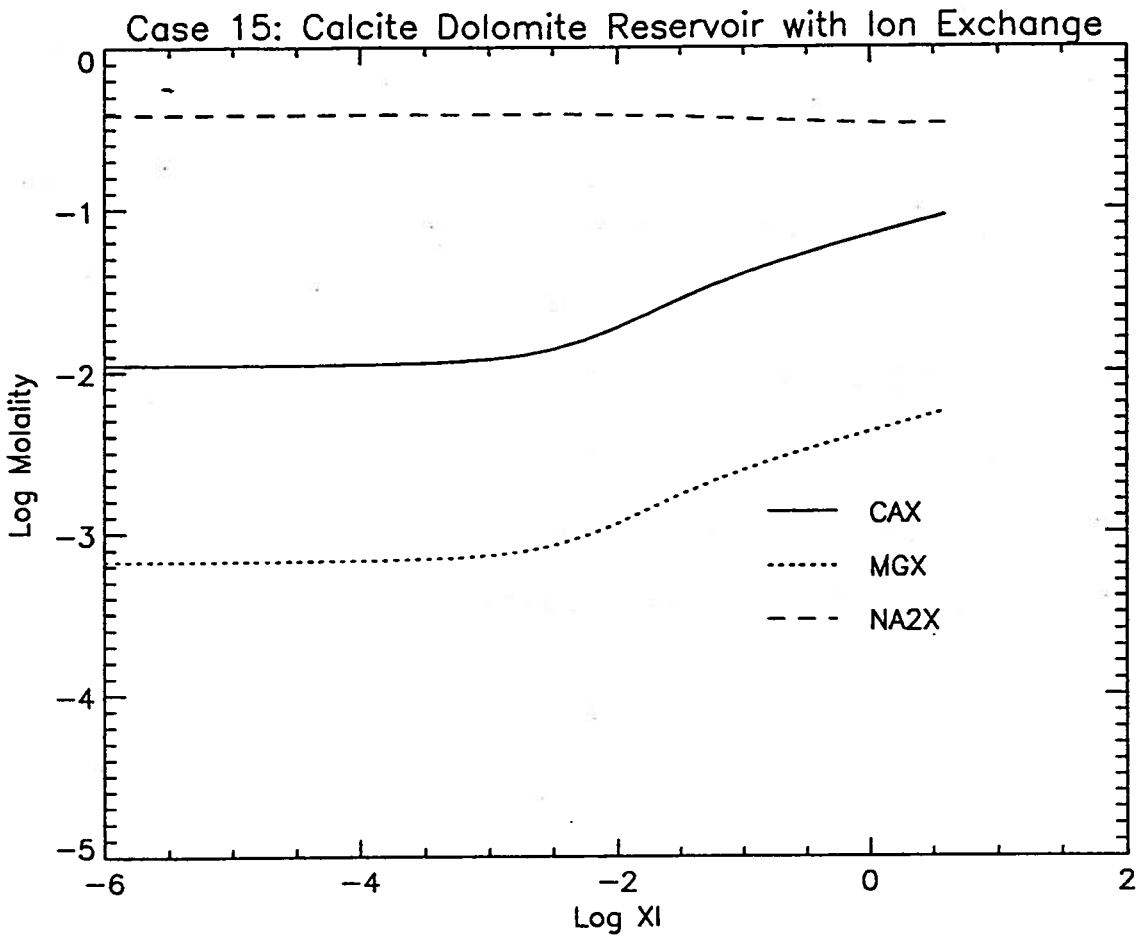


Figure 11.5.6c2

### **Figure 11.5.7**

**Reaction of Formation Water Brine with a calcite-dolomite-clay exchanger limestone aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').**

- a: Buildup of the partial pressure of CO<sub>2</sub> in bars.**
- b1: Molar amount of CO<sub>2</sub> injected into the aquifer.**
- b2: Change in the moles of mineral reactants.**
- c1: Change in the molality of the aqueous species.**
- c2: Change in the composition of the clay exchanger.**

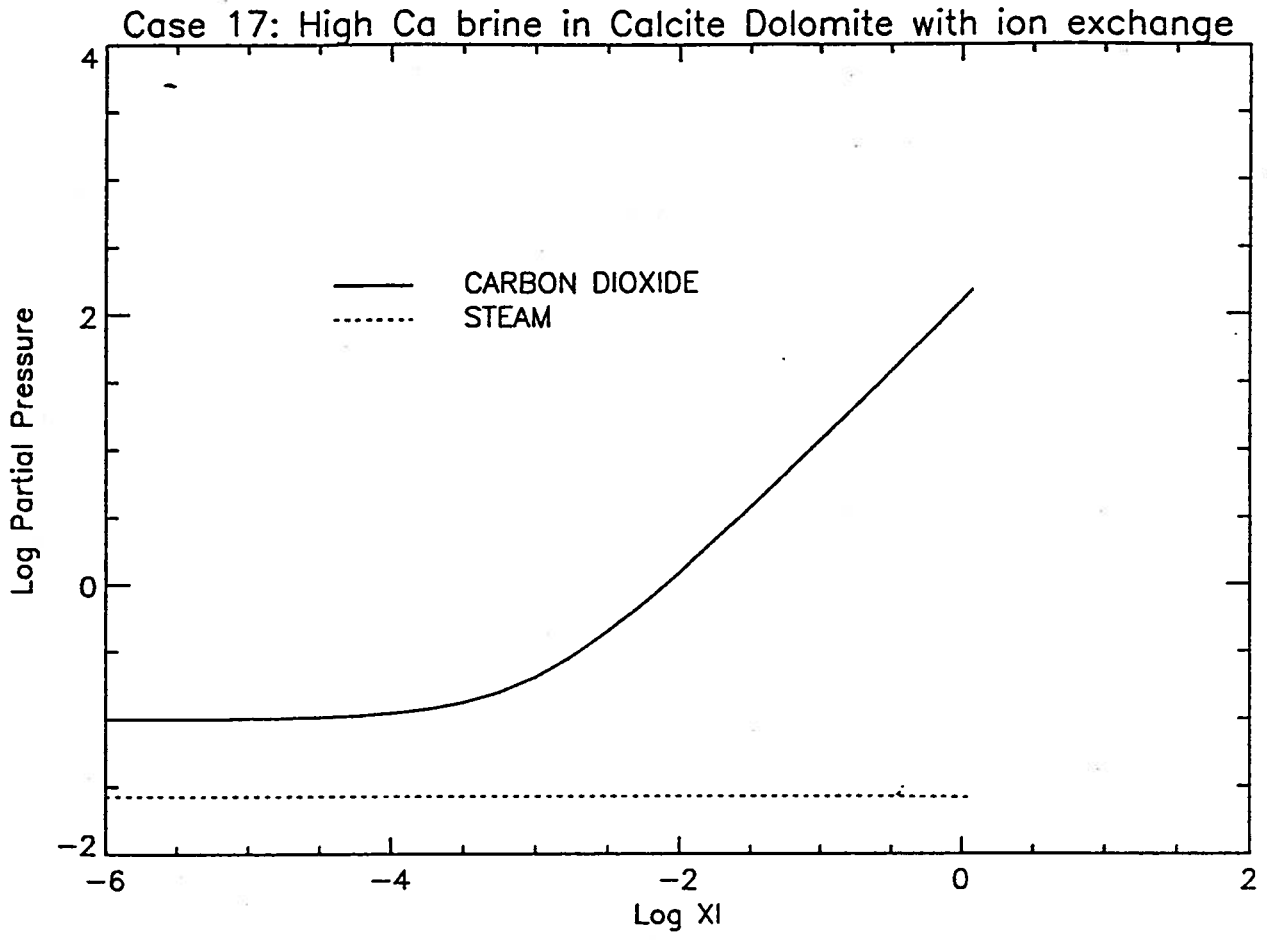


Figure 11.5.7a

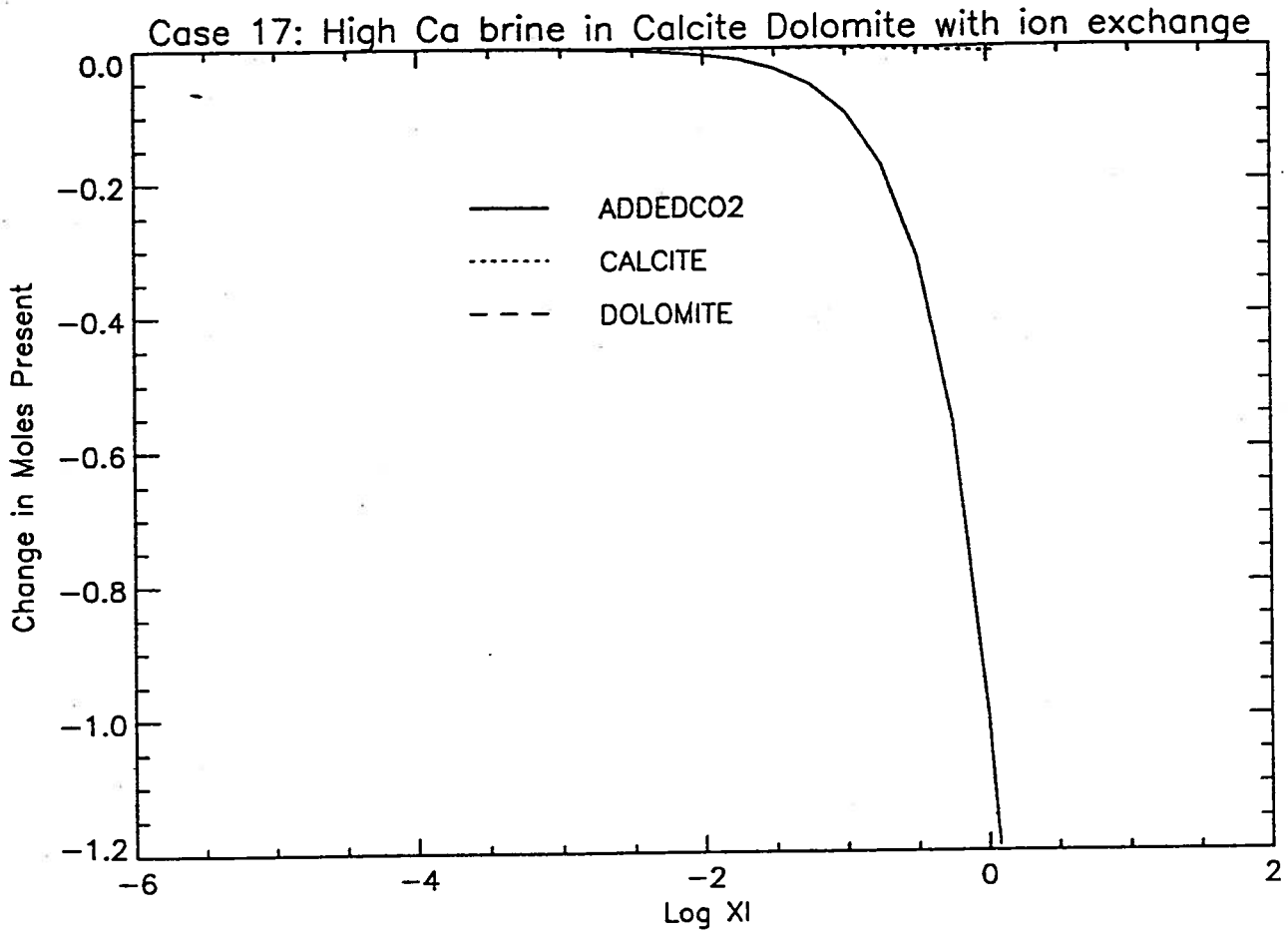


Figure 11.5.7b1

Case 17: High Ca brine in Calcite Dolomite with ion exchange

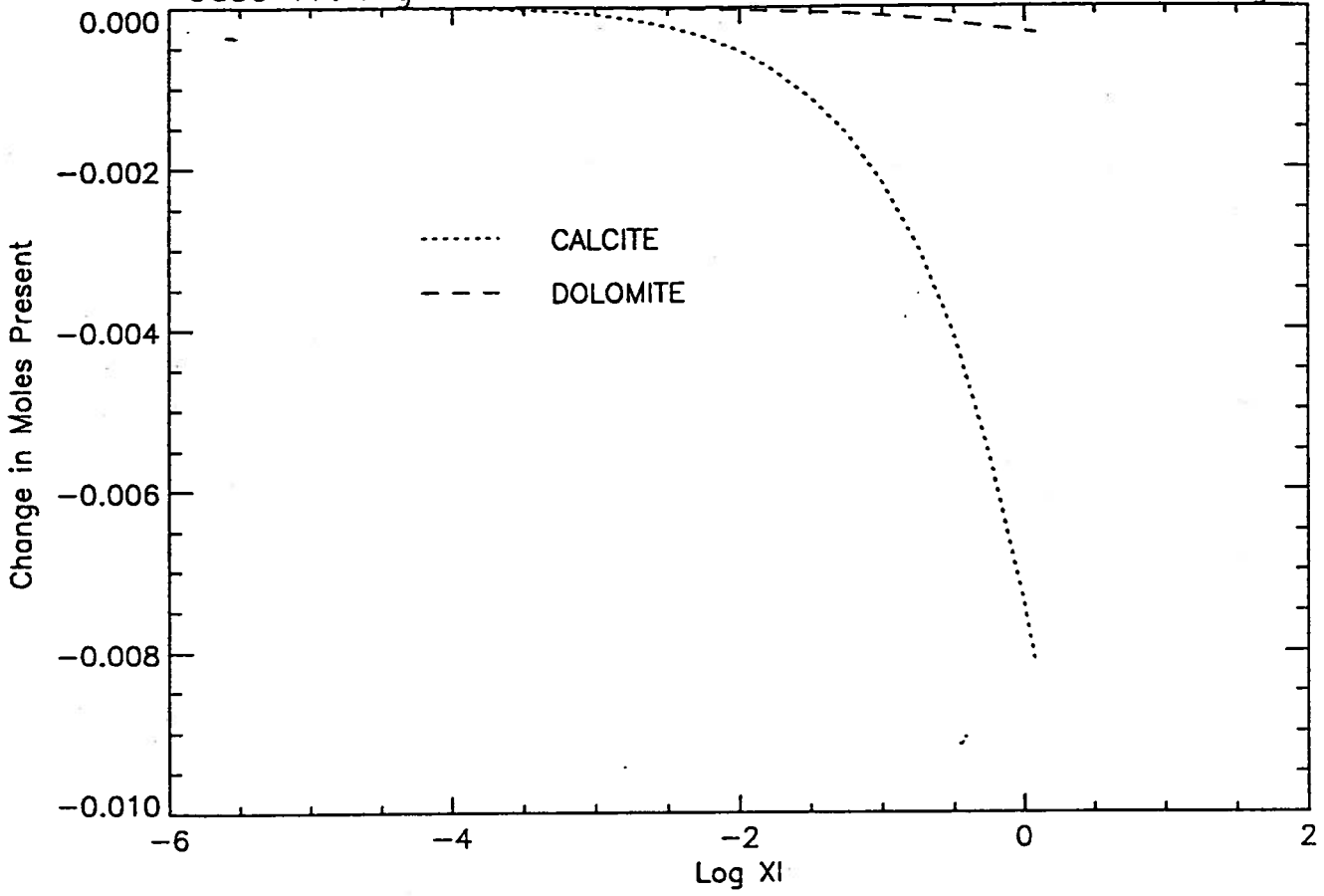


Figure 11.5.7b2

Case 17: High Ca brine in Calcite Dolomite with ion exchange

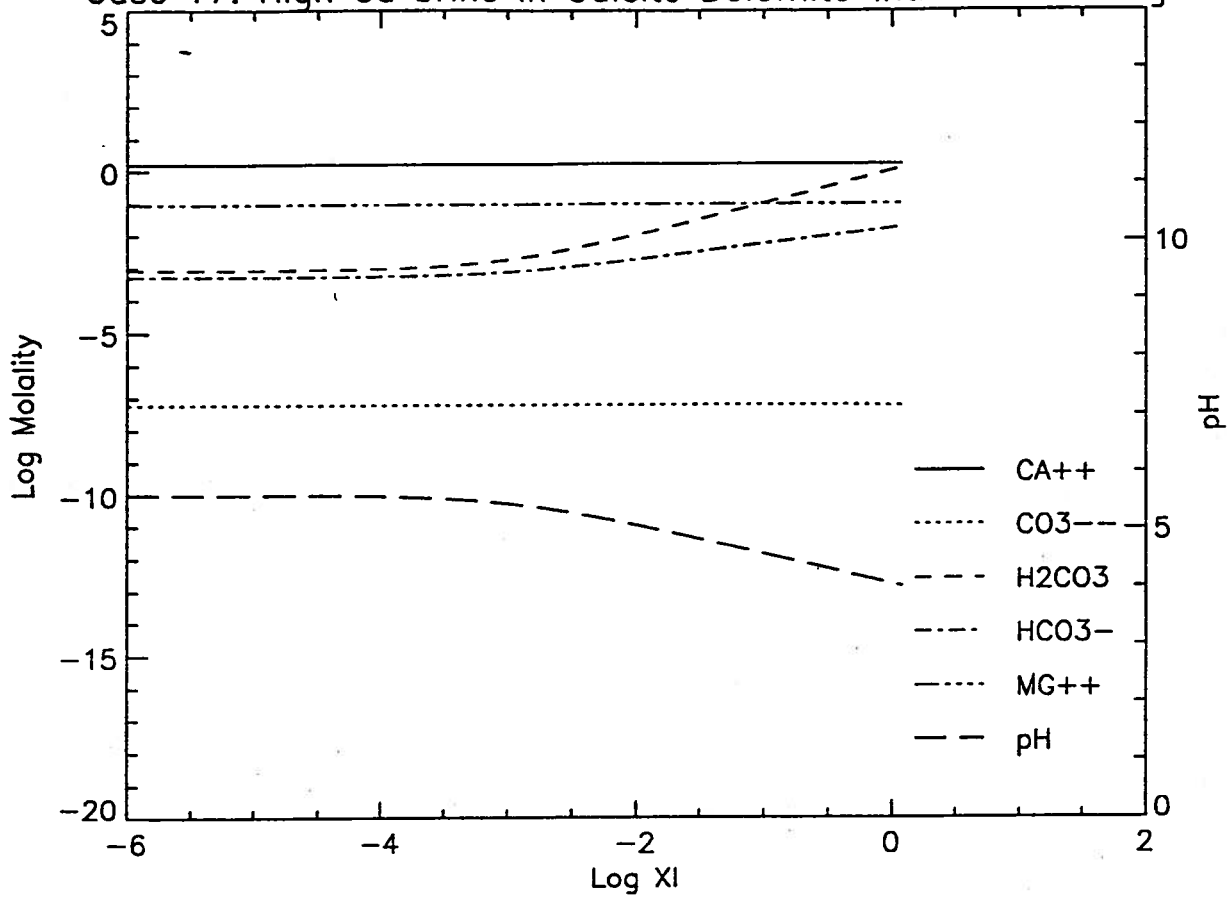


Figure 11.5.7c1

Case 17: High Ca brine in Calcite Dolomite with ion exchange

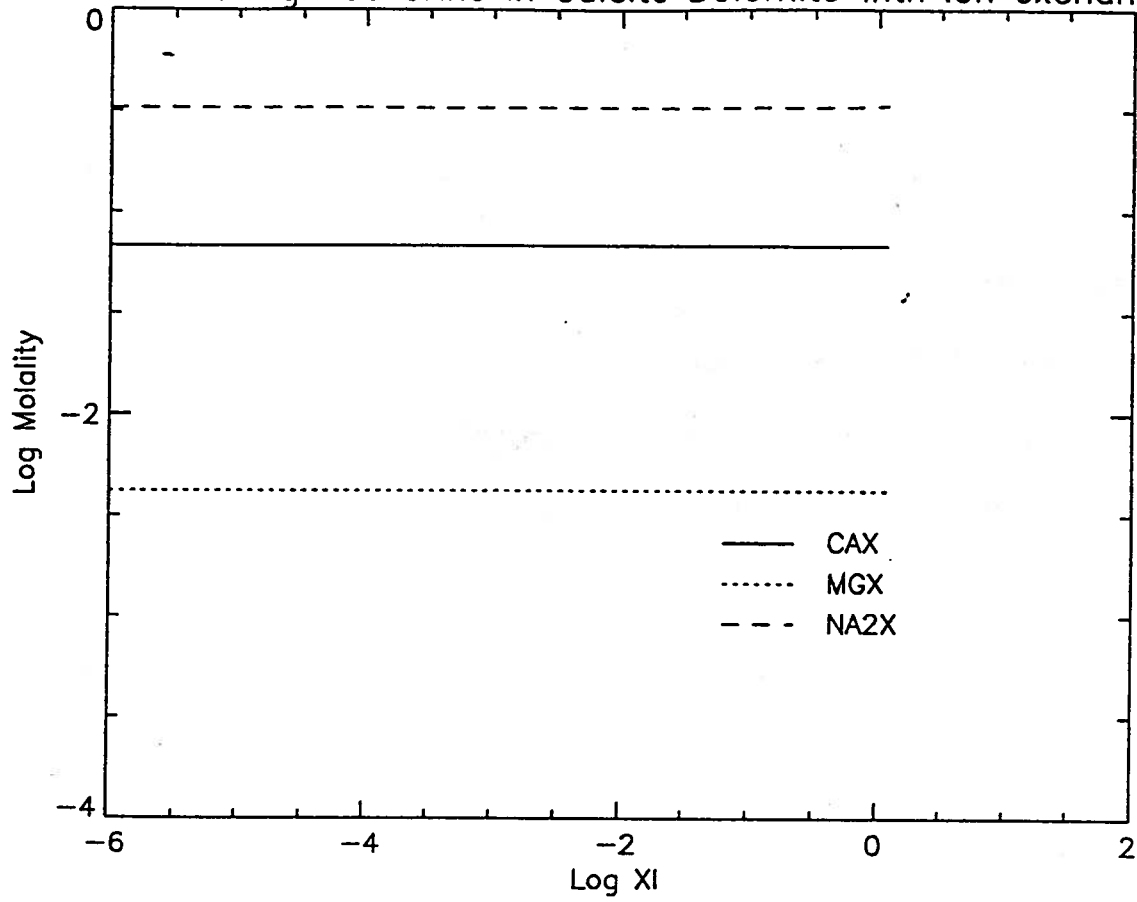


Figure 11.5.7c2

### Figure 11.5.8

Mineral Stability Fields in Aqueous Fluids plotted as a function of the thermodynamic concentrations or activities of the aqueous species in water.

- a: Activity ratio of  $(K^+/H^+)$  versus activity of  $(H_4SiO_4)$
- b: Activity ratio of  $(Na^+/H^+)$  versus activity of  $(H_4SiO_4)$
- c: Activity ratio of  $(Ca^{2+}/(H^+)^2)$  versus activity of  $(H_4SiO_4)$
- d: Activity ratio of  $(Mg^{2+}/(H^+)^2)$  versus activity of  $(H_4SiO_4)$



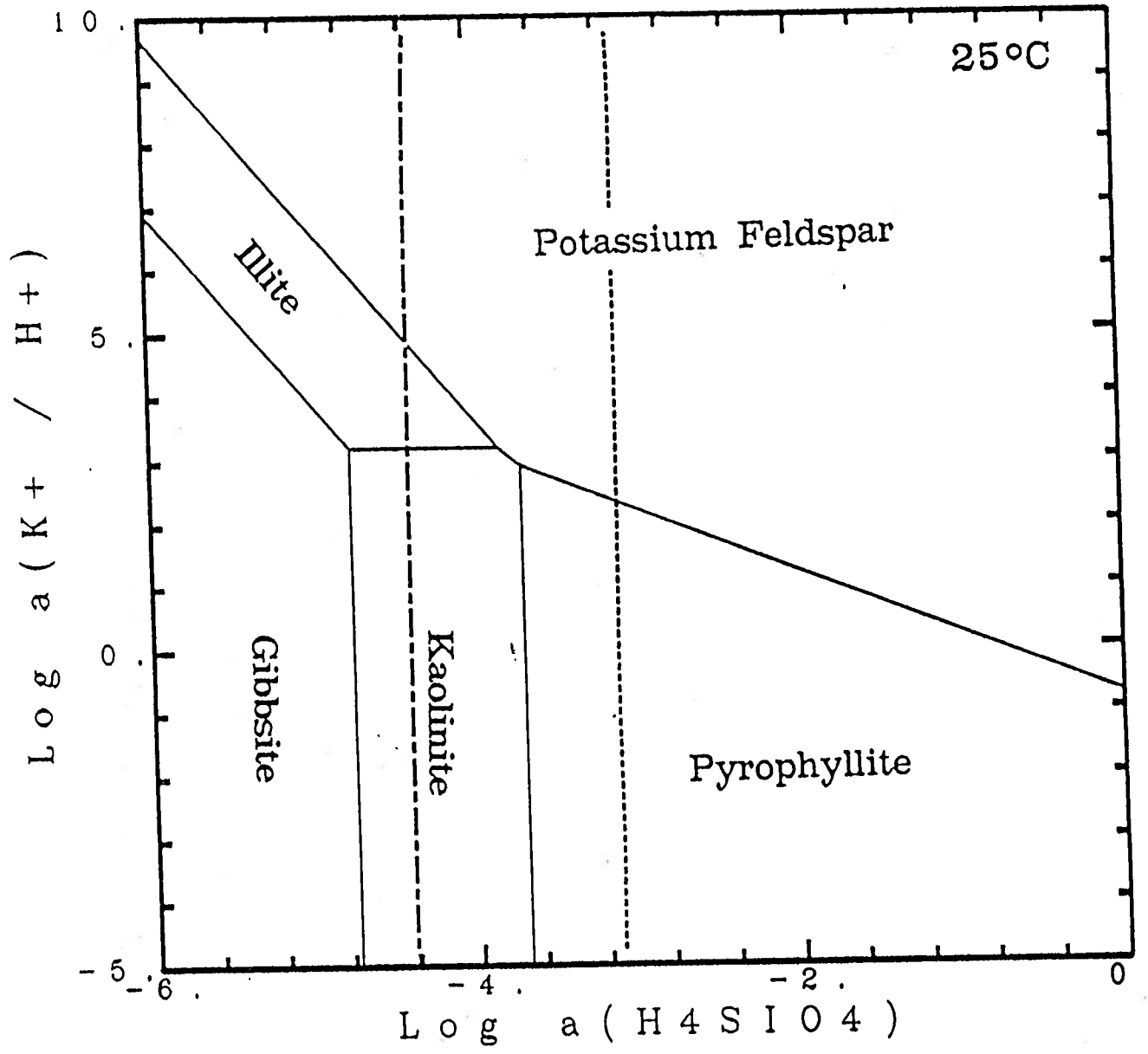


Figure 11.5.8a

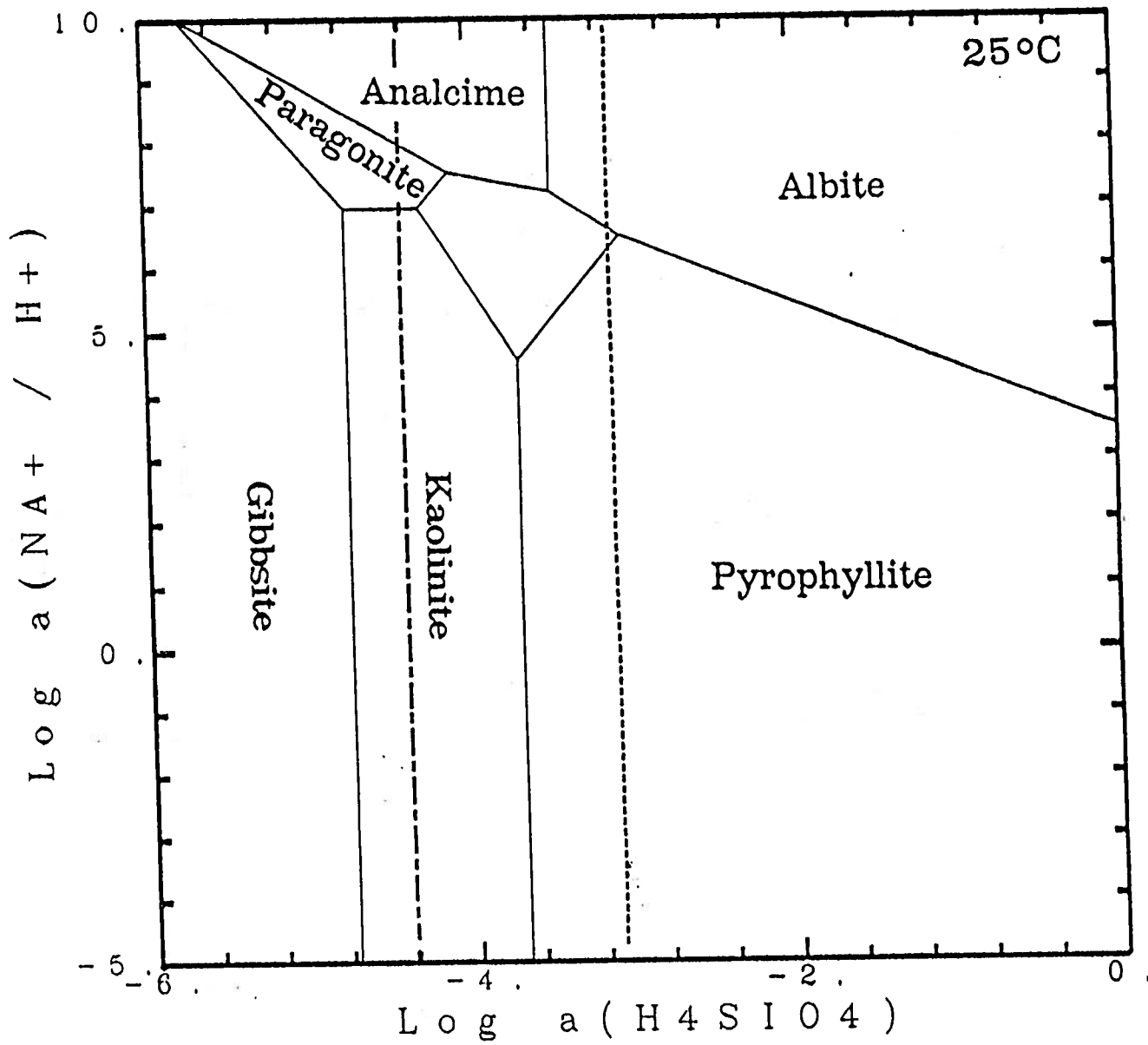


Figure 11.5.8b

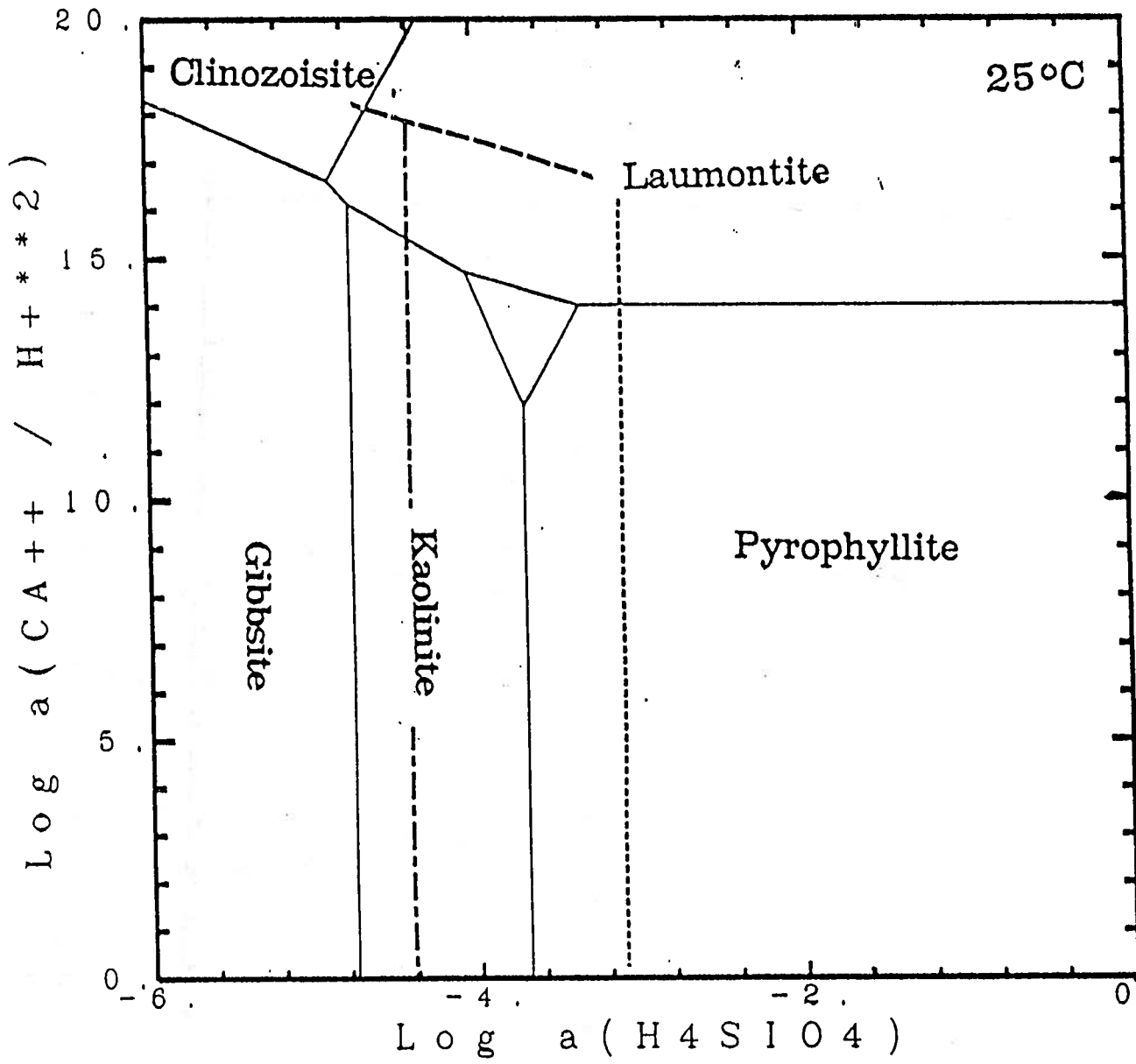


Figure 11.5.8c

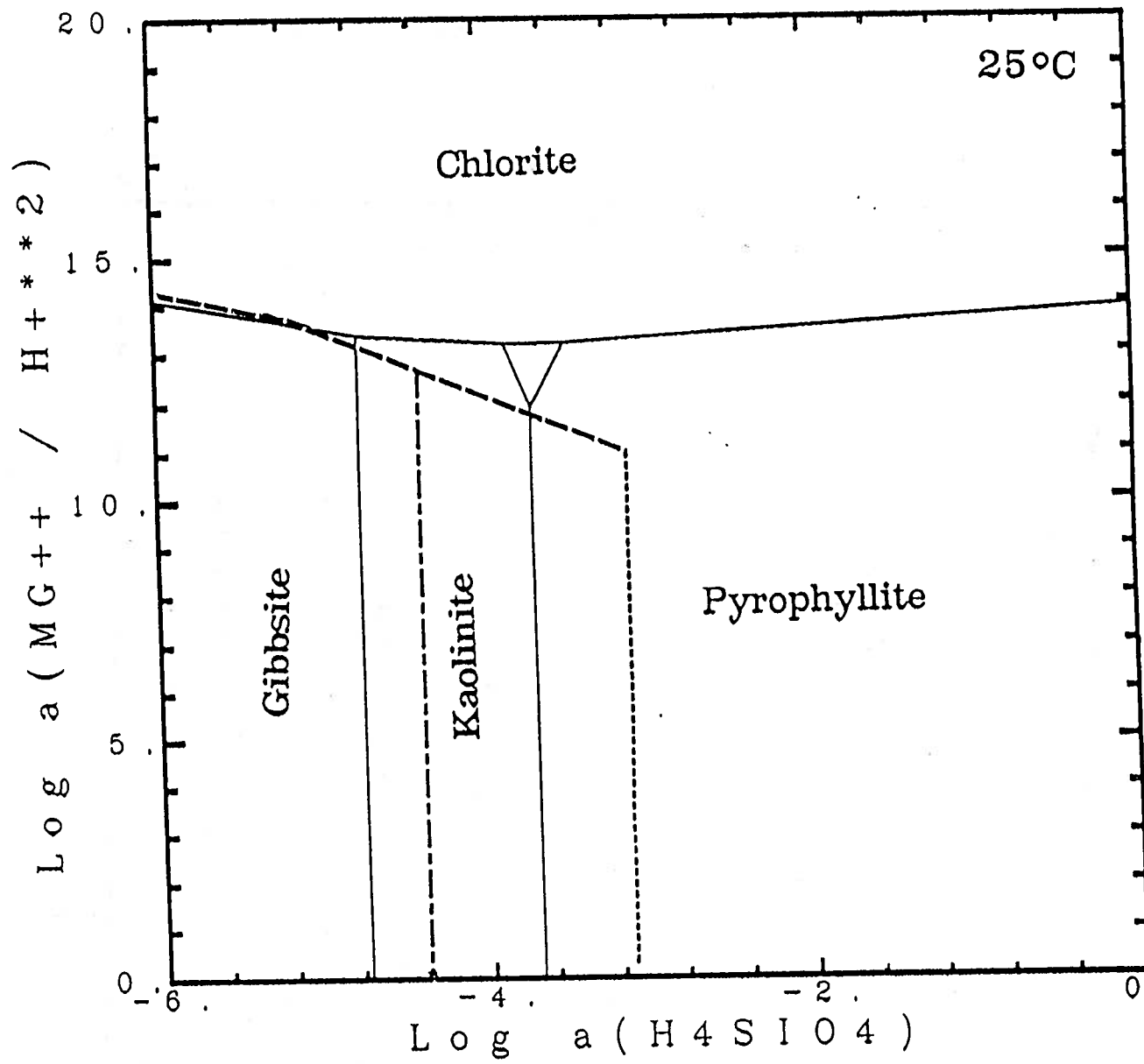


Figure 11.5.8d

### Figure 11.5.9

Reaction of a Brackish Formation Water with an anorthite-quartz-illite siliciclastic aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').

- a: Buildup of the partial pressure of CO<sub>2</sub> in bars.
- b1: Molar amount of CO<sub>2</sub> injected into the aquifer.
- b2: Change in the moles of mineral reactants.
- b3: Change in the moles of mineral products.
- c: Change in the molality of the aqueous species.

Case 10: Quartz, Anorthite, Muscovite/Illite Reservoir

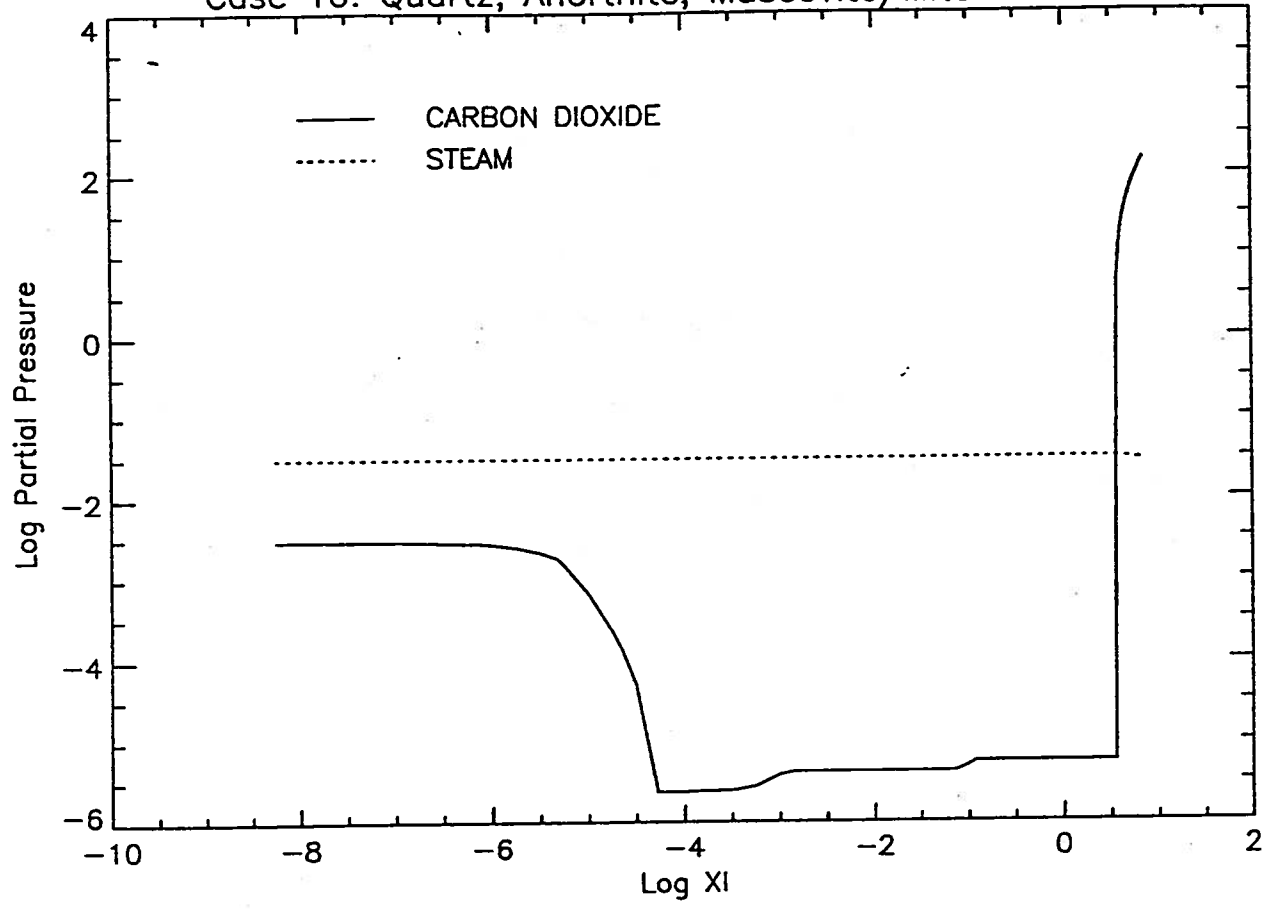


Figure 11.5.9a

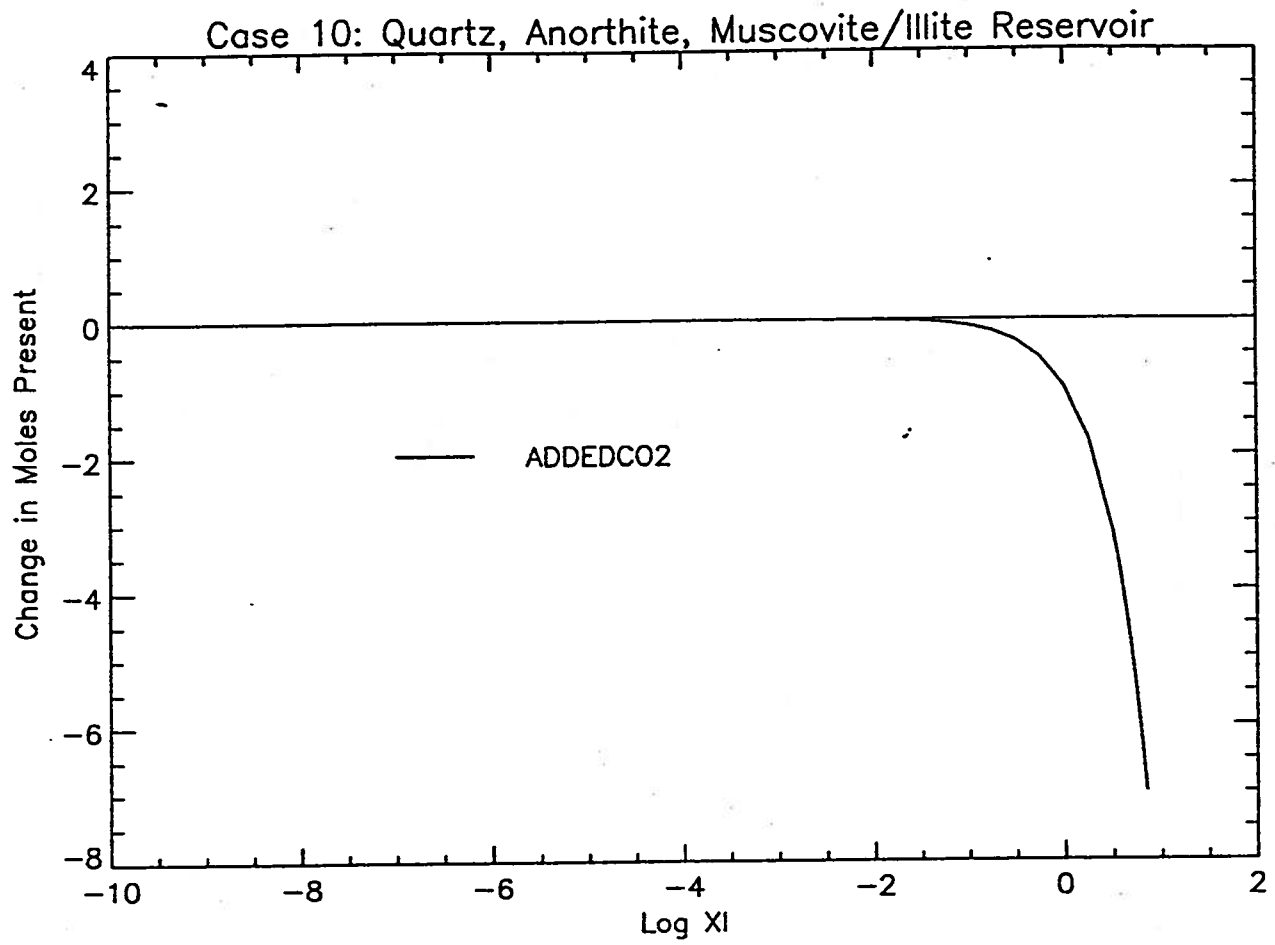


Figure 11.5.9b1

Case 10: Quartz, Anorthite, Muscovite/Illite Reservoir

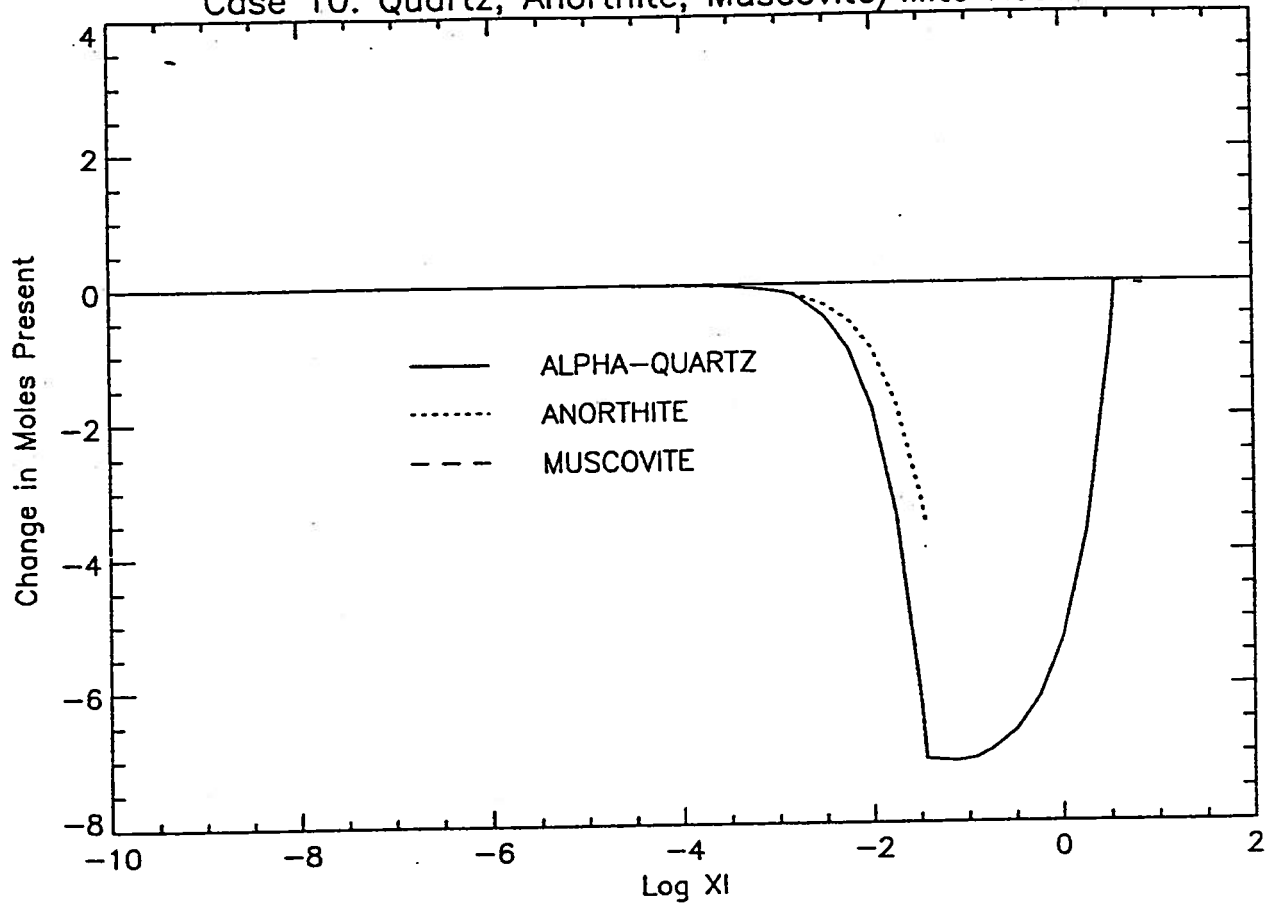


Figure 11.5.9b2



Case 10: Quartz, Anorthite, Muscovite/Illite Reservoir

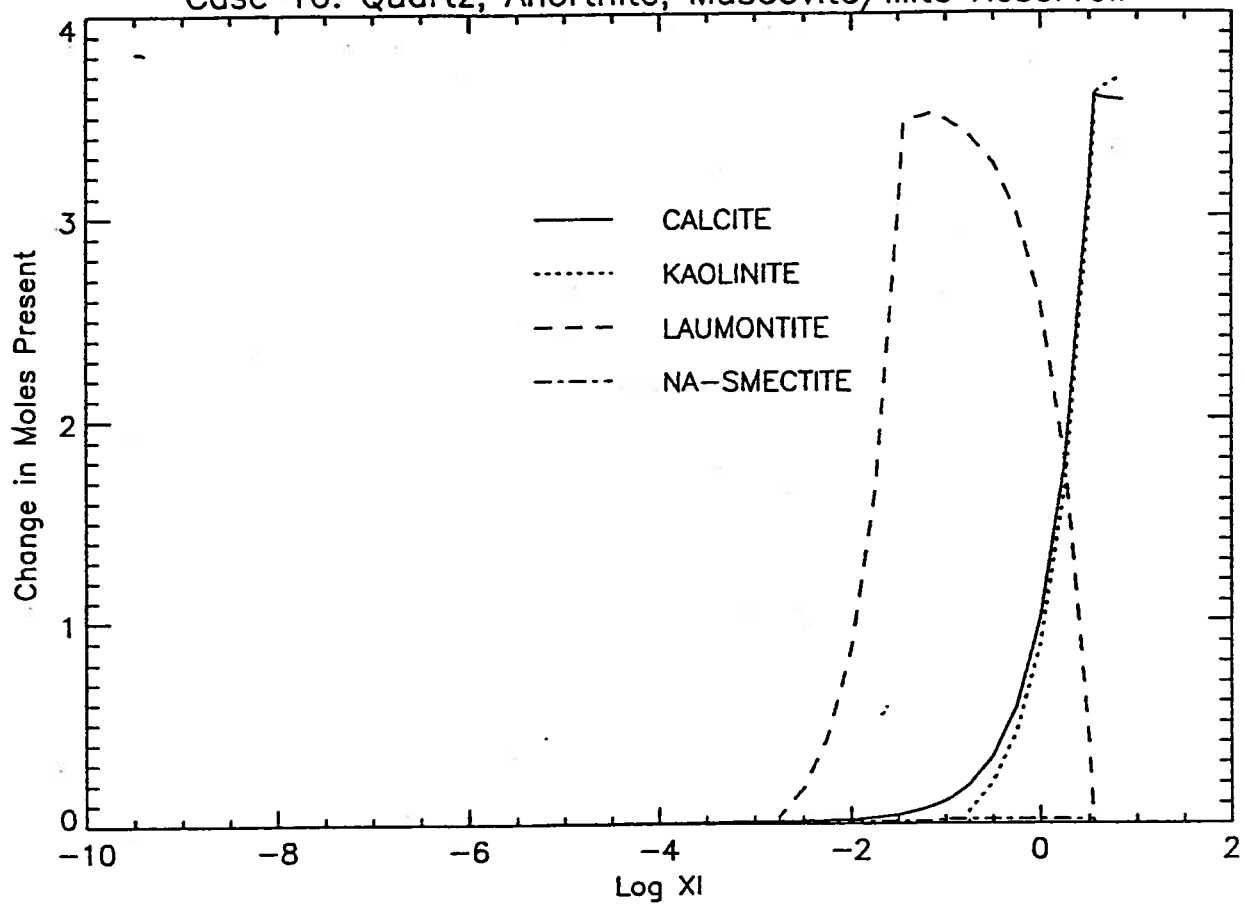


Figure 11.5.9b3

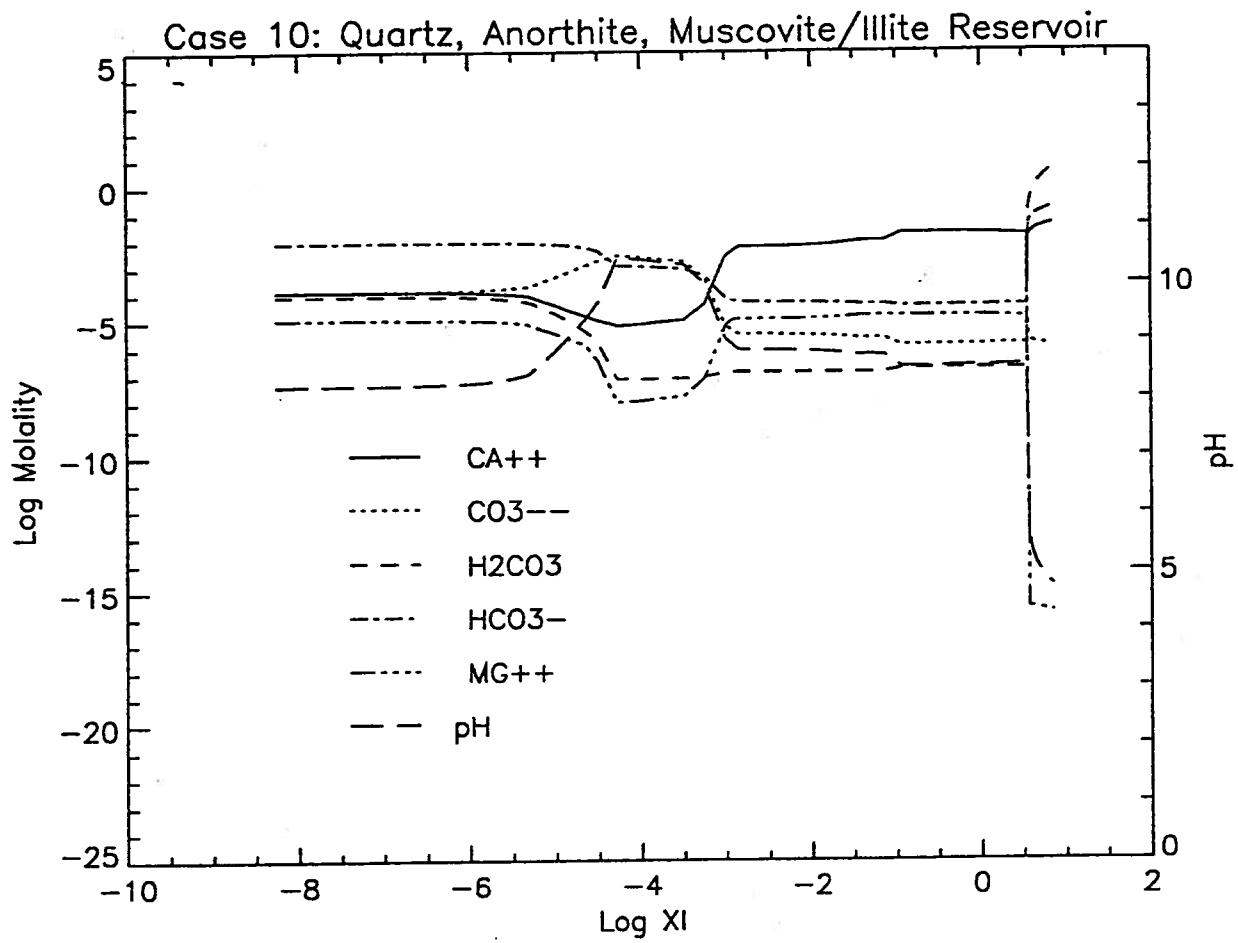


Figure 11.5.9c

### Figure 11.5.10

Reaction of a Formation Water Brine with an anorthite-quartz siliciclastic aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('XI').

a: Buildup of the partial pressure of CO<sub>2</sub> in bars.

b1: Molar amount of CO<sub>2</sub> injected into the aquifer & change in the moles of mineral reactants.

b2: Change in the moles of mineral products.

b3: Change in the moles of mineral products.

c: Change in the molality of the aqueous species.

Case 13: Concentrated brine reacting with a Anorthite Quartz Reservoir

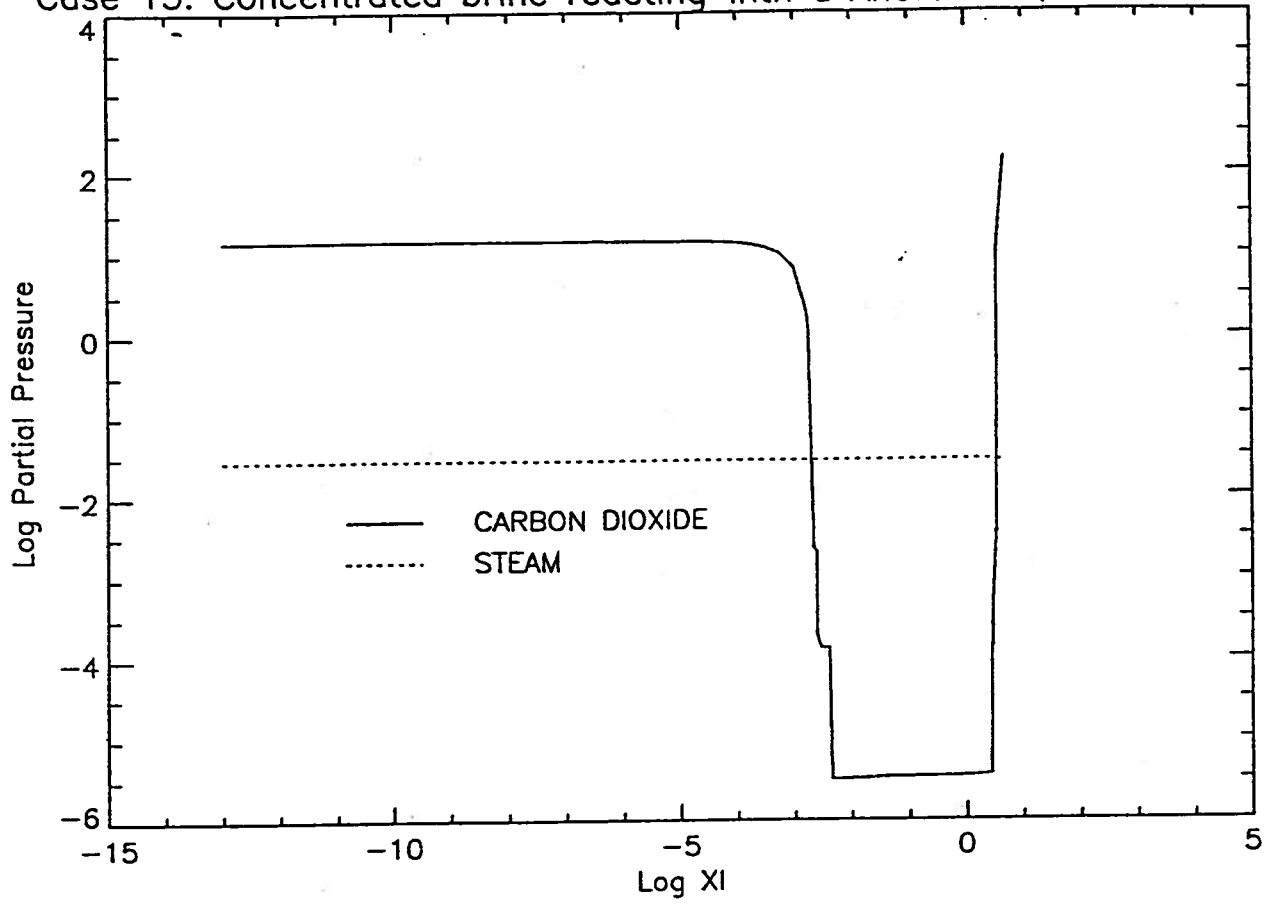


Figure 11.5.10a

Case 13: Concentrated brine reacting with a Anorthite Quartz Reservoir

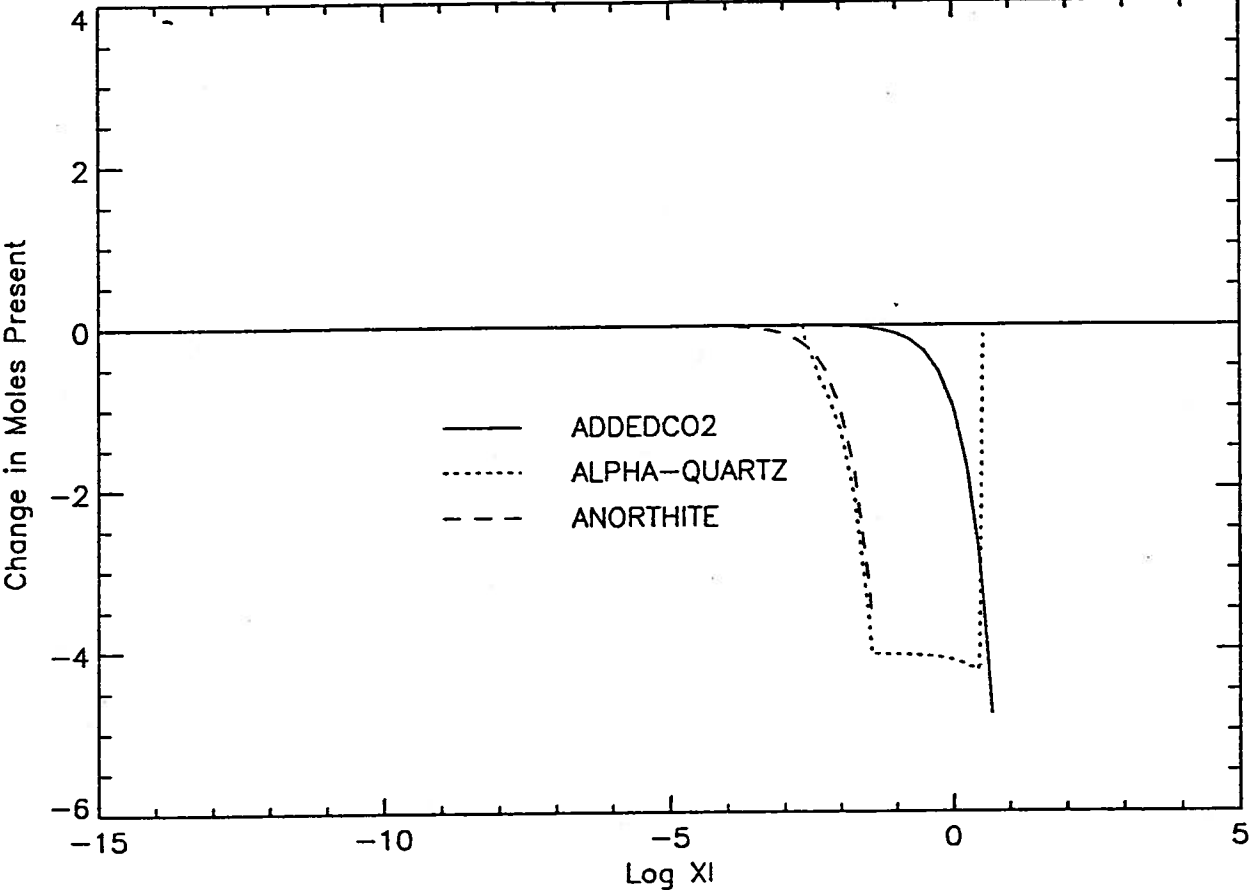


Figure 11.5.10b1

Case 13: Concentrated brine reacting with a Anorthite Quartz Reservoir

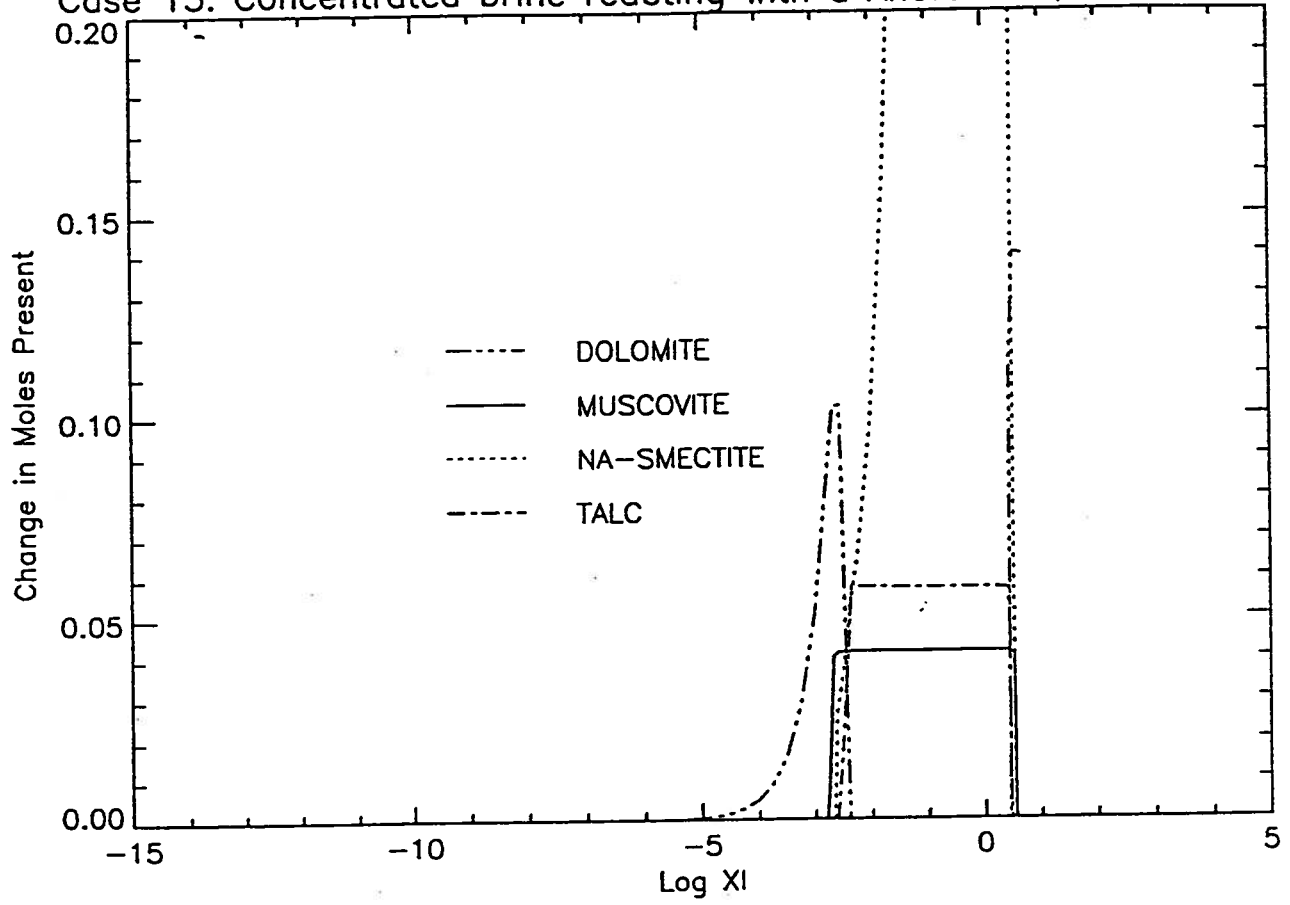


Figure 11.5.10b2

Case 13: Concentrated brine reacting with a Anorthite Quartz Reservoir

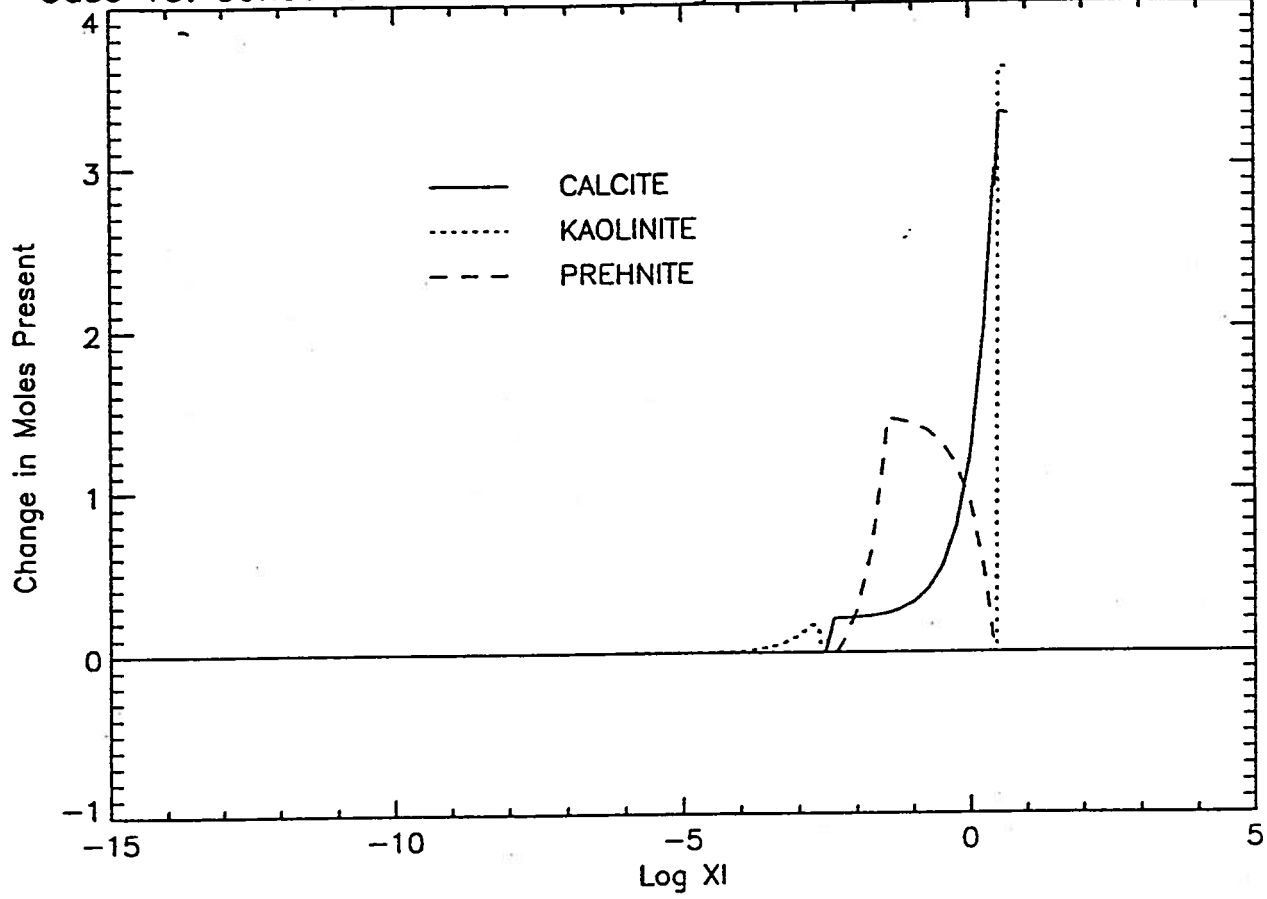


Figure 11.5.10b3

Case 13: Concentrated brine reacting with Anorthite Quartz Reservoir

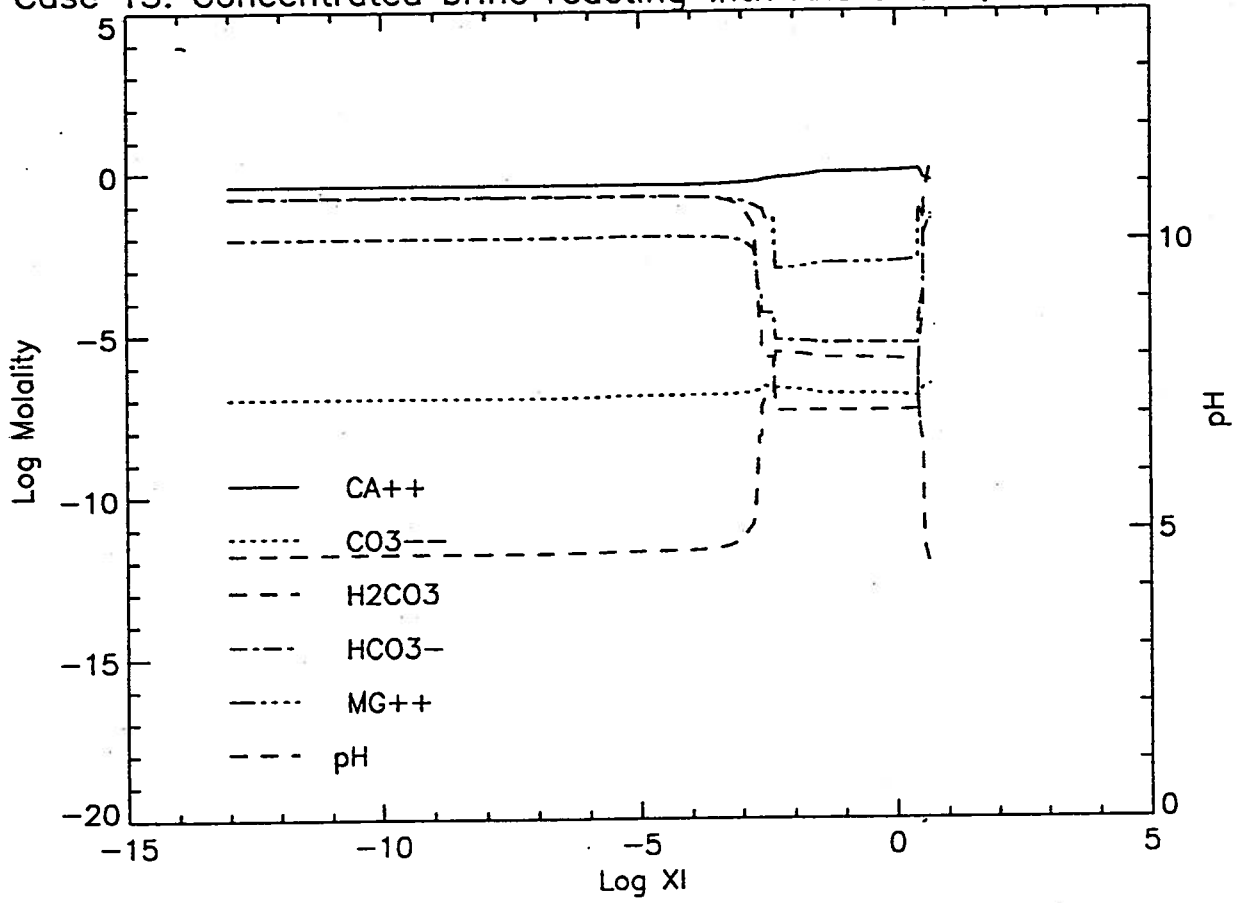


Figure 11.5.10c



### Figure 11.5.11

Reaction of a Formation Water Brine with an anorthite-quartz siliciclastic aquifer at 100°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').

a: Buildup of the partial pressure of CO<sub>2</sub> in bars.

b1: Molar amount of CO<sub>2</sub> injected into the aquifer & change in the moles of mineral reactants.

b2: Change in the moles of mineral products.

b3: Change in the moles of mineral products.

c: Change in the molality of the aqueous species.

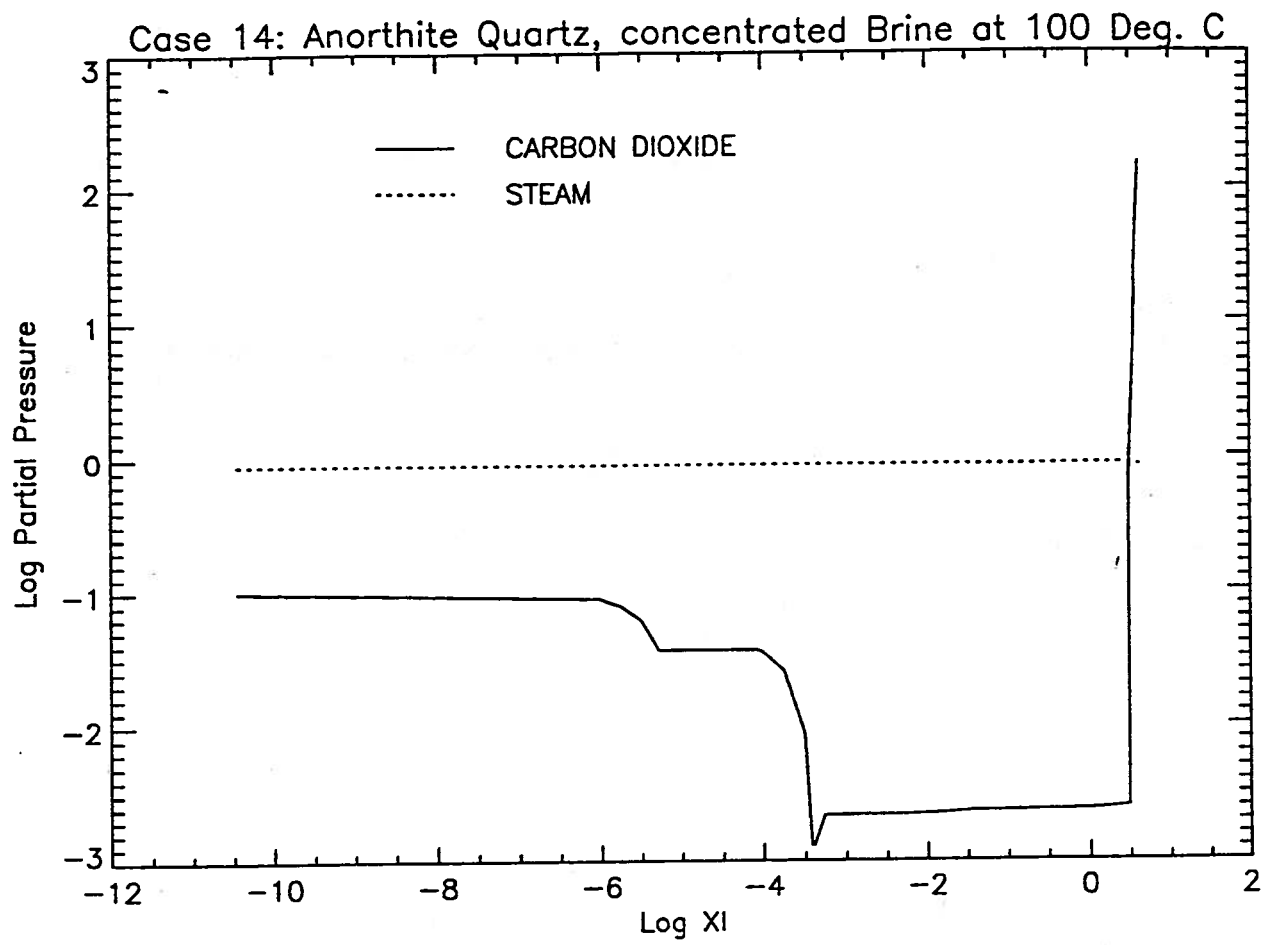


Figure 11.5.11a

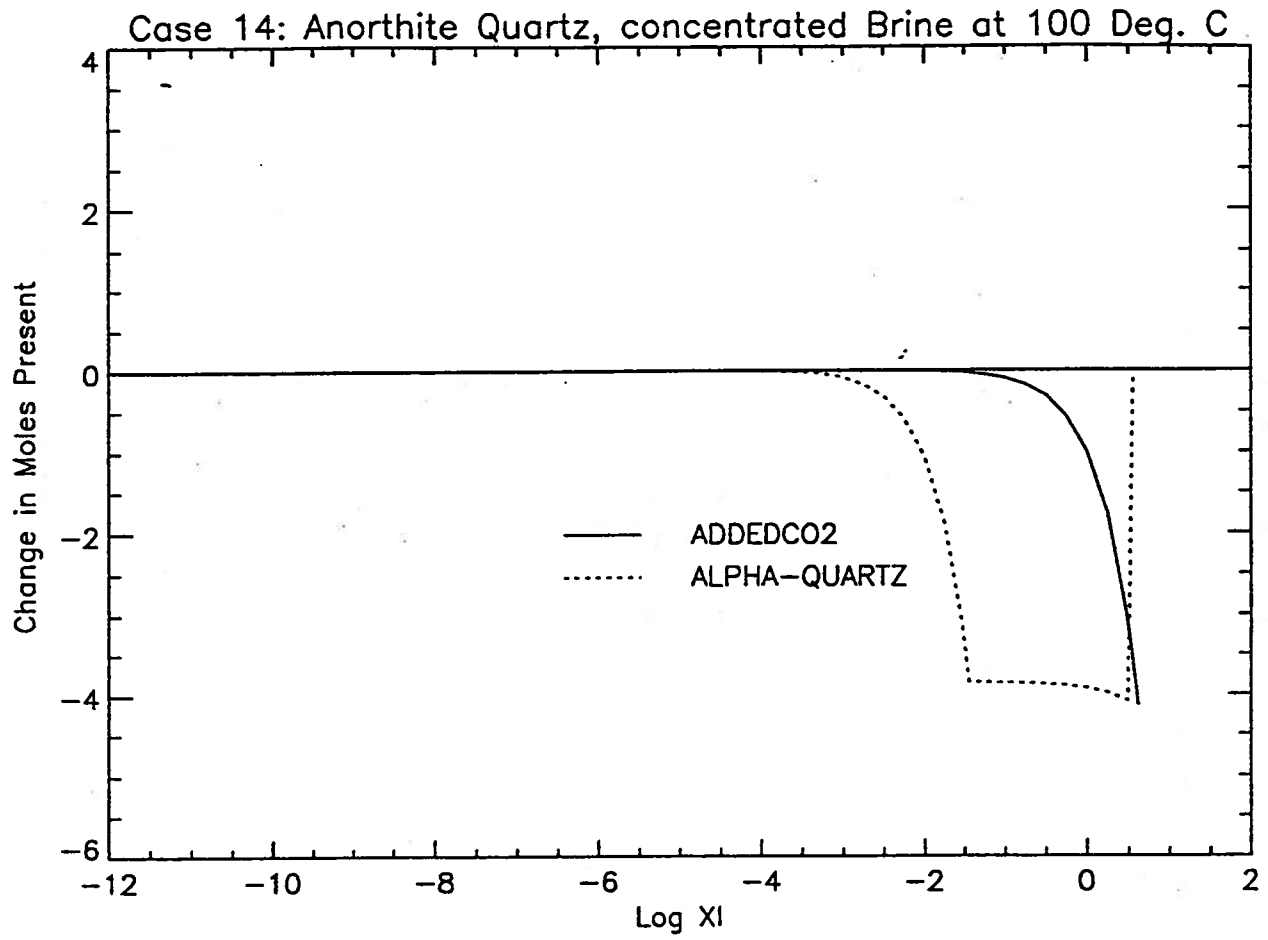


Figure 11.5.11b1

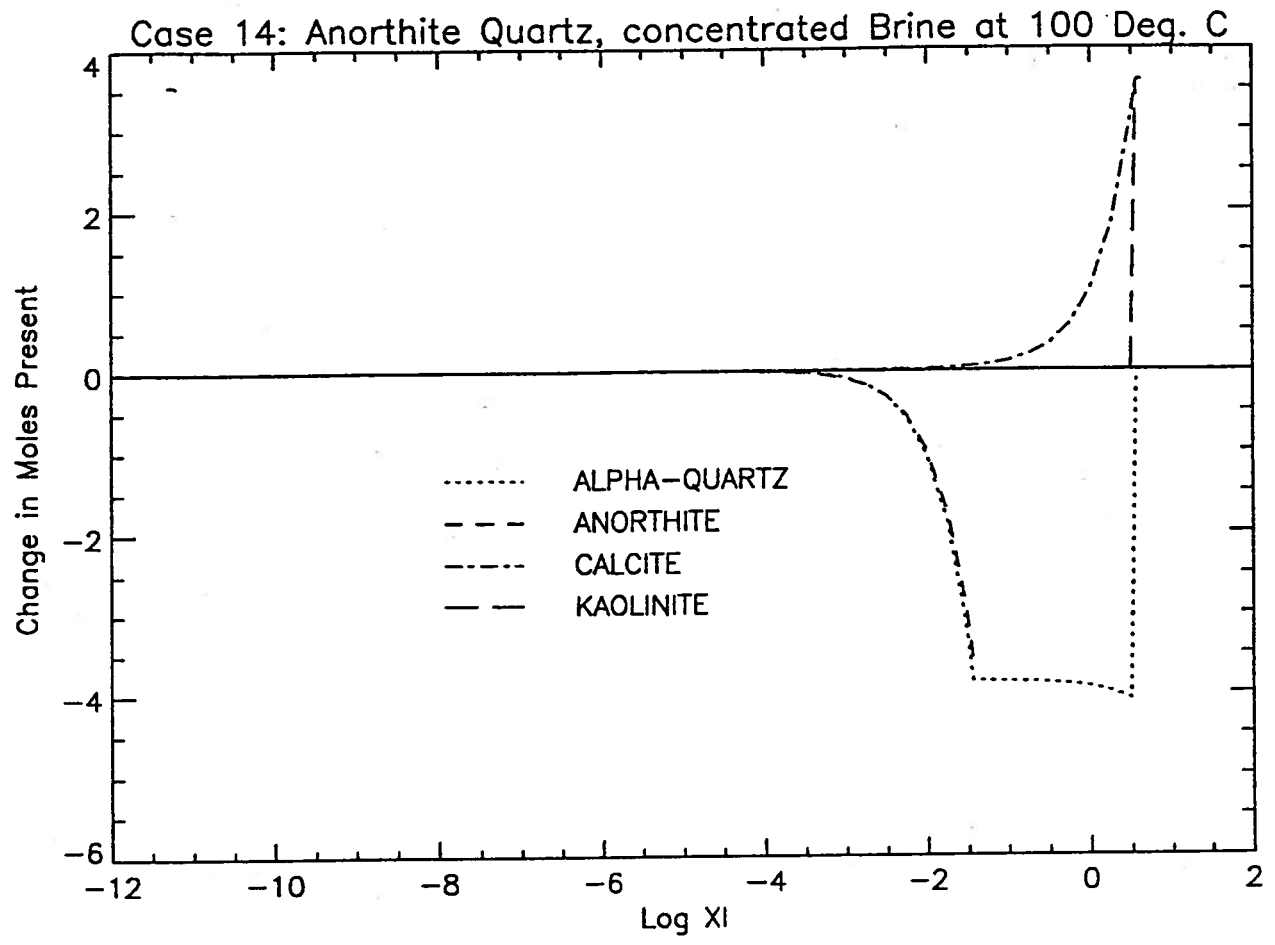


Figure 11.5.11b2

Case 14: Anorthite Quartz, concentrated Brine at 100 Deg. C

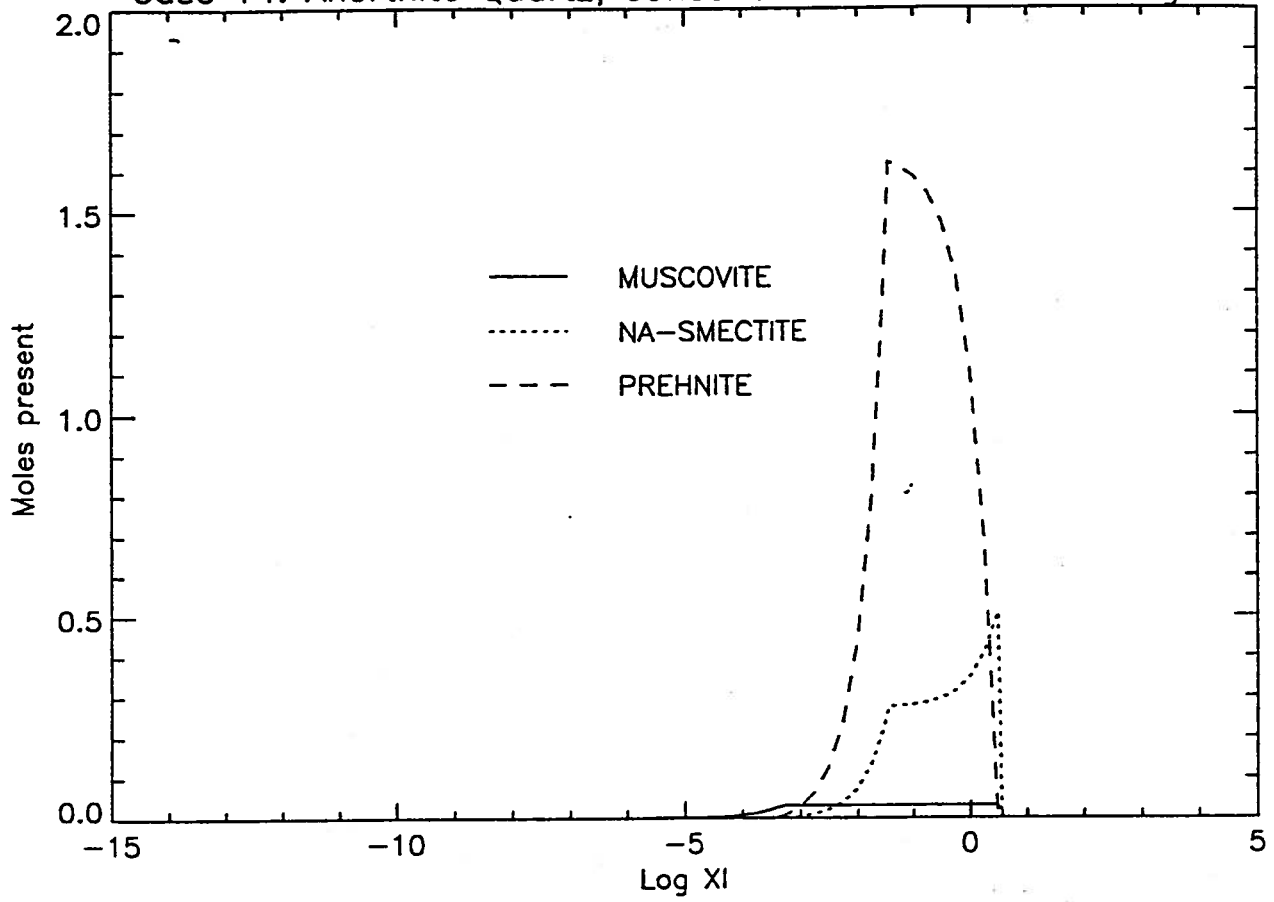


Figure 11.5.11b3

Case 14: Anorthite Quartz, concentrated Brine at 100 Deg. C

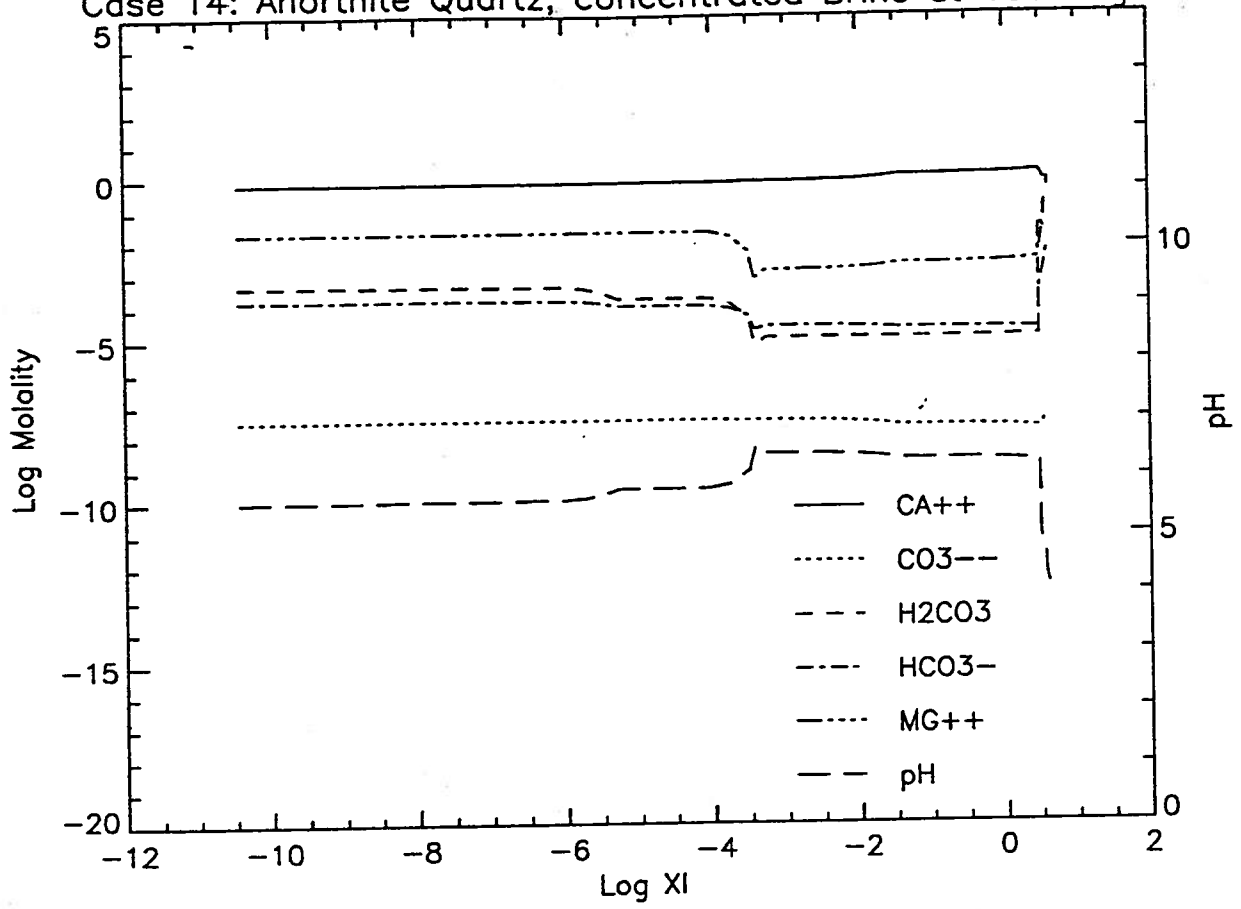


Figure 11.5.11c

### Figure 11.5.12

Reaction of a Formation Water Brine with an anorthite-Ca.smectite-quartz-illite siliciclastic aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').

- a: Buildup of the partial pressure of CO<sub>2</sub> in bars.
- b1: Molar amount of CO<sub>2</sub> injected into the aquifer.
- b2: Change in the moles of mineral reactants.
- b3: Change in the moles of mineral reactants and products.
- b4: Change in the moles of mineral products.
- b5: Change in the moles of mineral products.
- c: Change in the molality of the aqueous species.

Case 6. Formation water reacting with a complex silicate reservoir

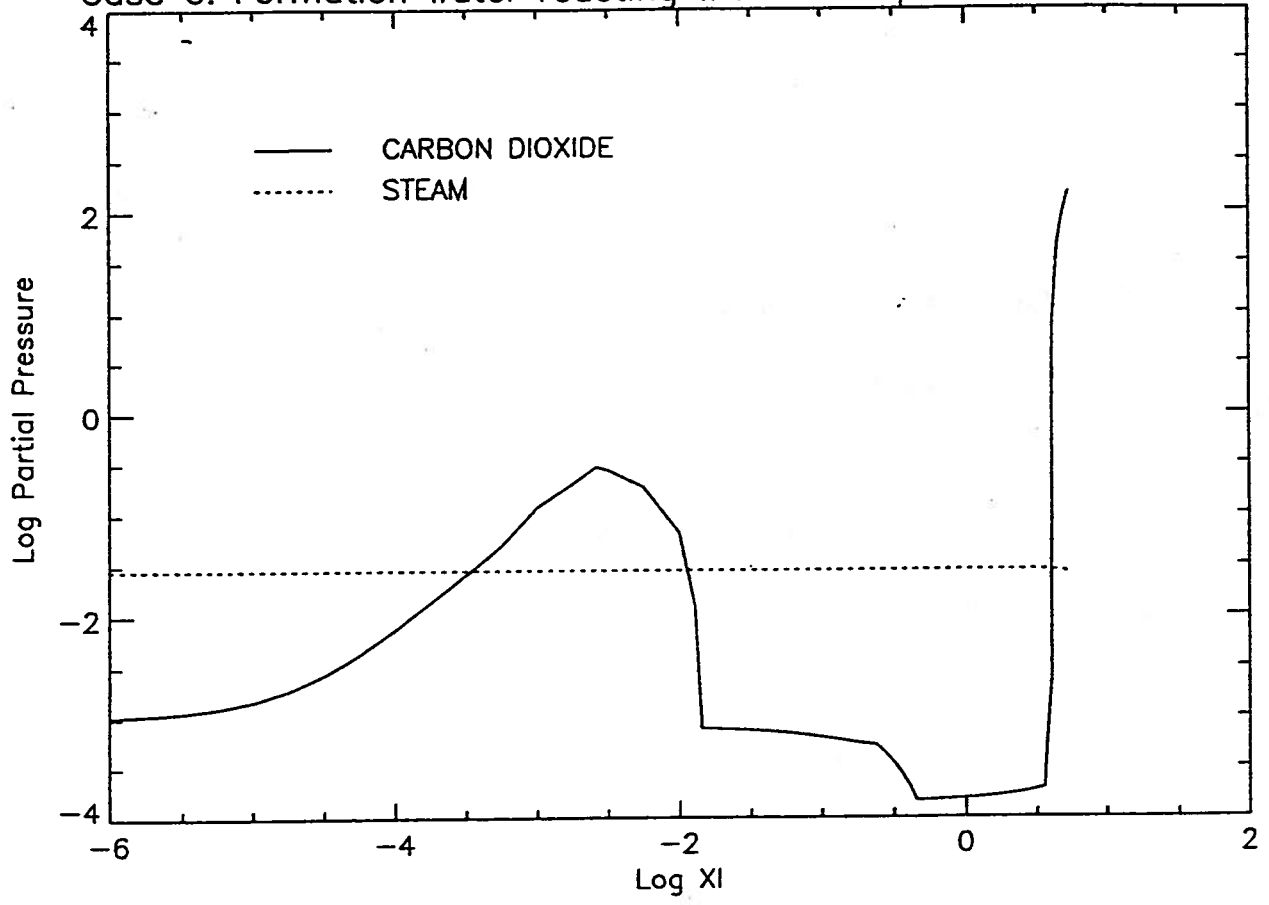


Figure 11.5.12a



Case 6. Formation water reacting with a complex silicate reservoir

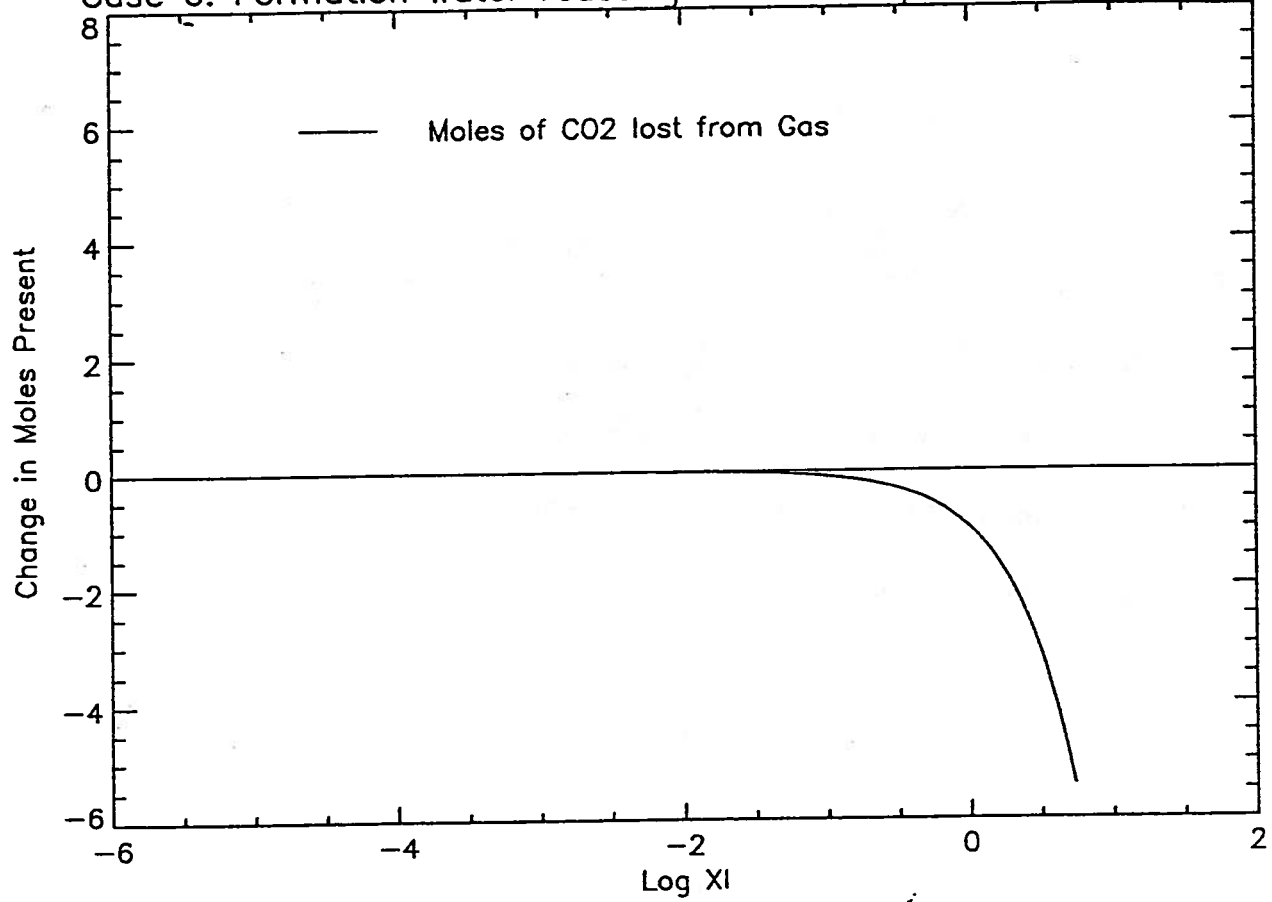


Figure 11.5.12b1

### **Figure 11.5.13**

Reaction of a Formation Water Brine with an anorthite-Ca-smectite-quartz-illite siliciclastic aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('XI'). The water/rock ratio has been increased by an order of magnitude.

- a: Buildup of the partial pressure of CO<sub>2</sub> in bars.
- b1: Molar amount of CO<sub>2</sub> injected into the aquifer.
- b2: Change in the moles of mineral reactants and products.
- b3: Change in the moles of mineral reactants and products.
- b4: Change in the moles of mineral products.
- c: Change in the molality of the aqueous species.

Case 3: Formation water in a complex silicate reservoir

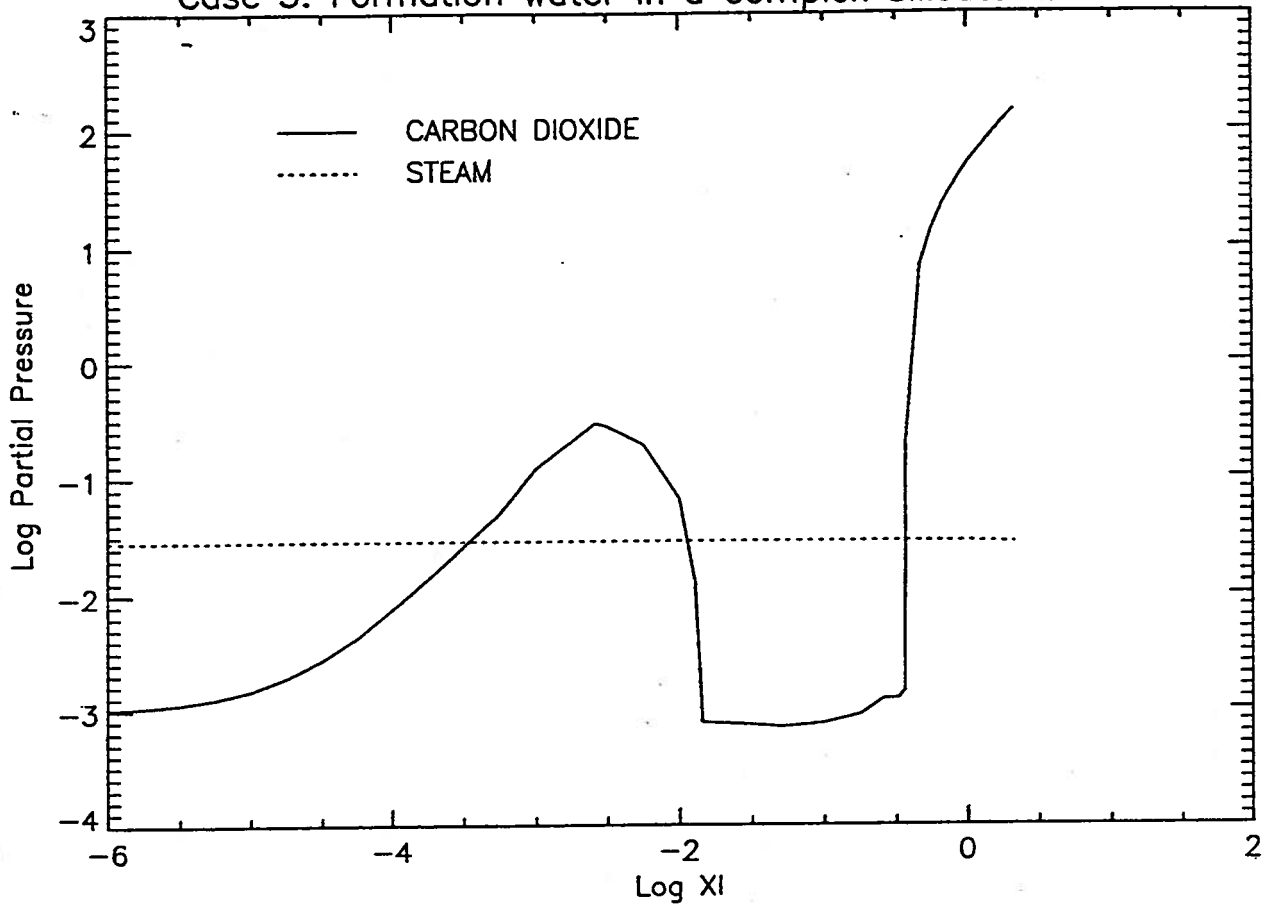


Figure 11.5.13a

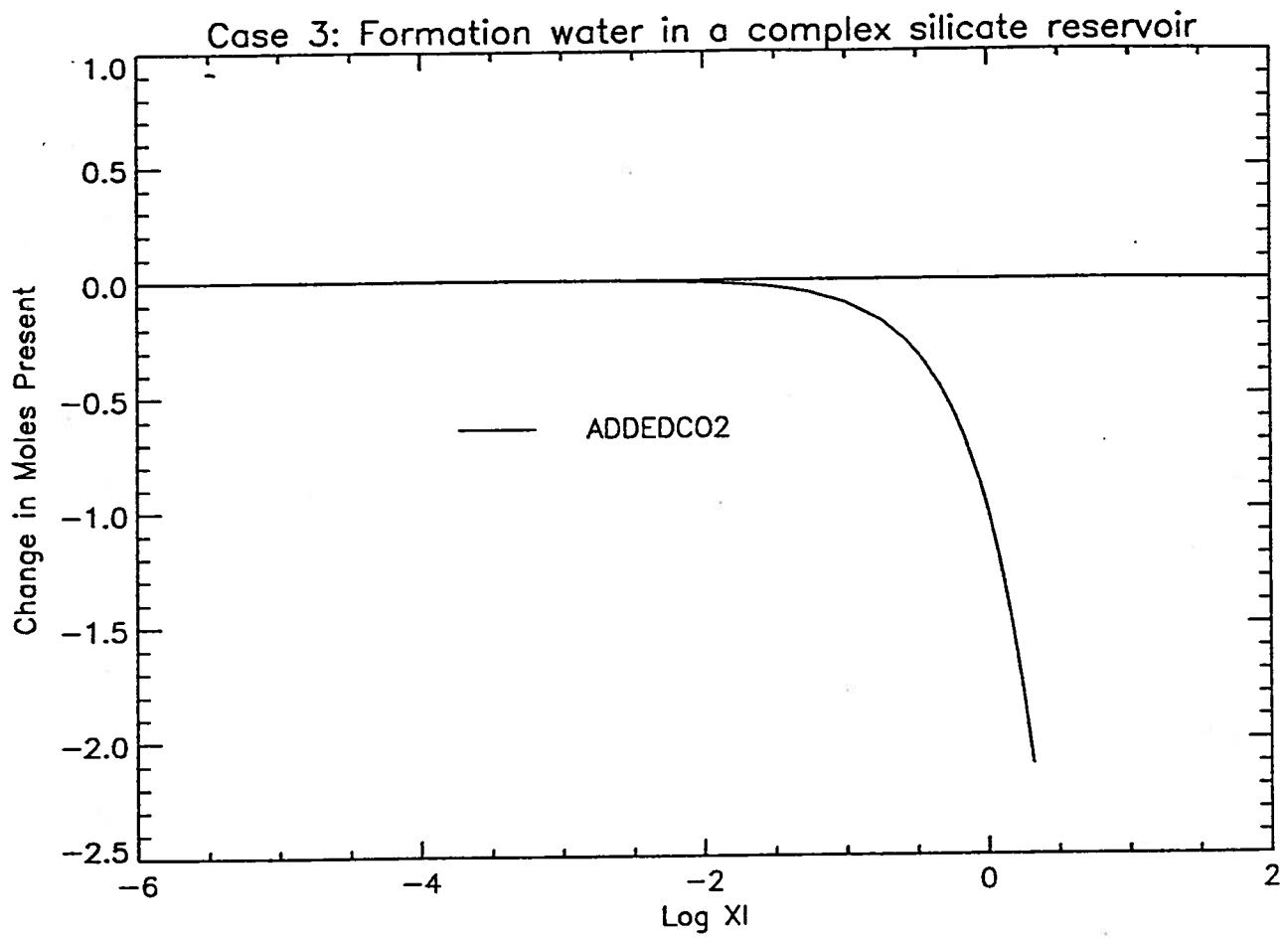


Figure 11.5.13b1

Case 3: Formation water in a complex silicate reservoir

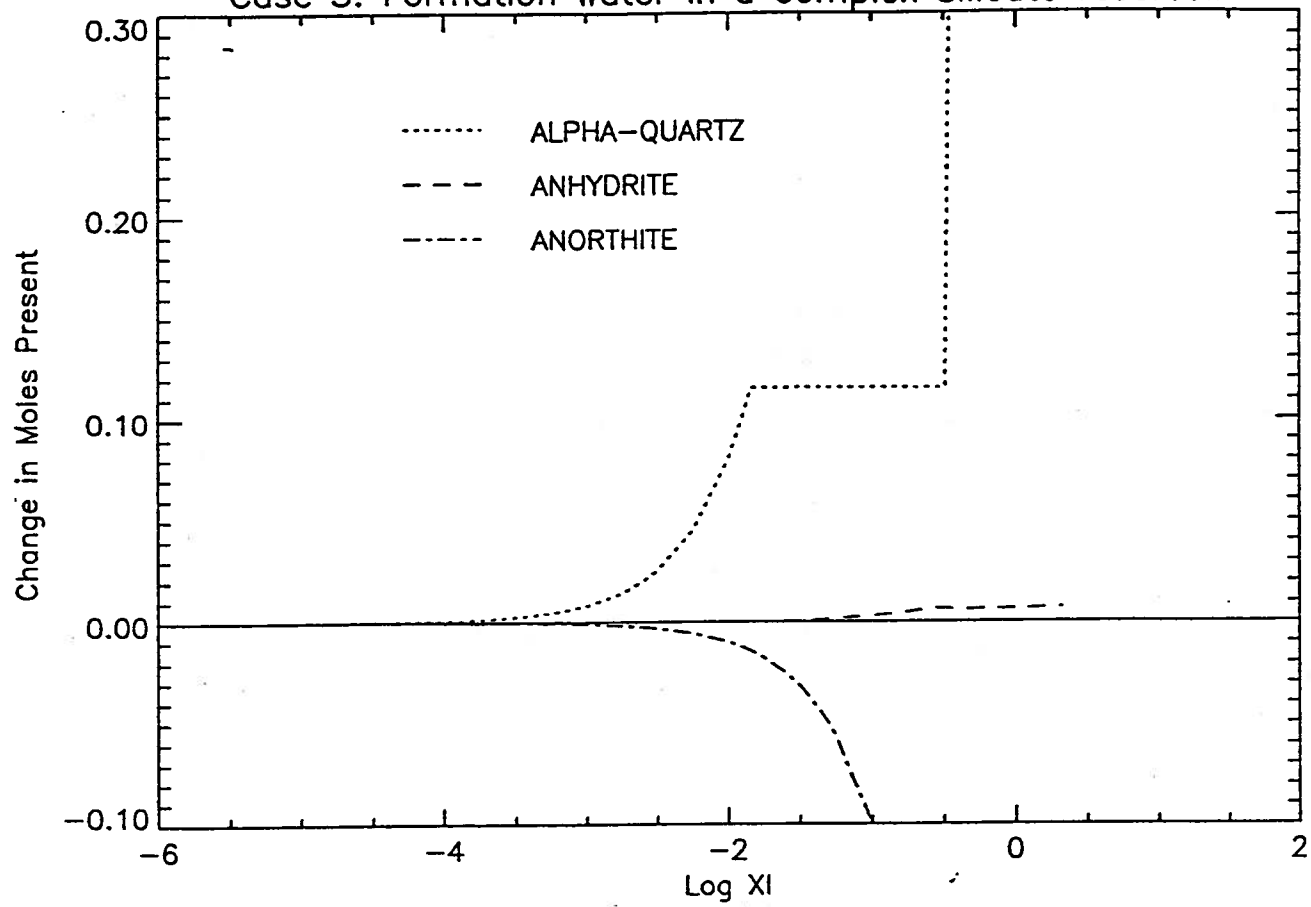


Figure 11.5.13b2

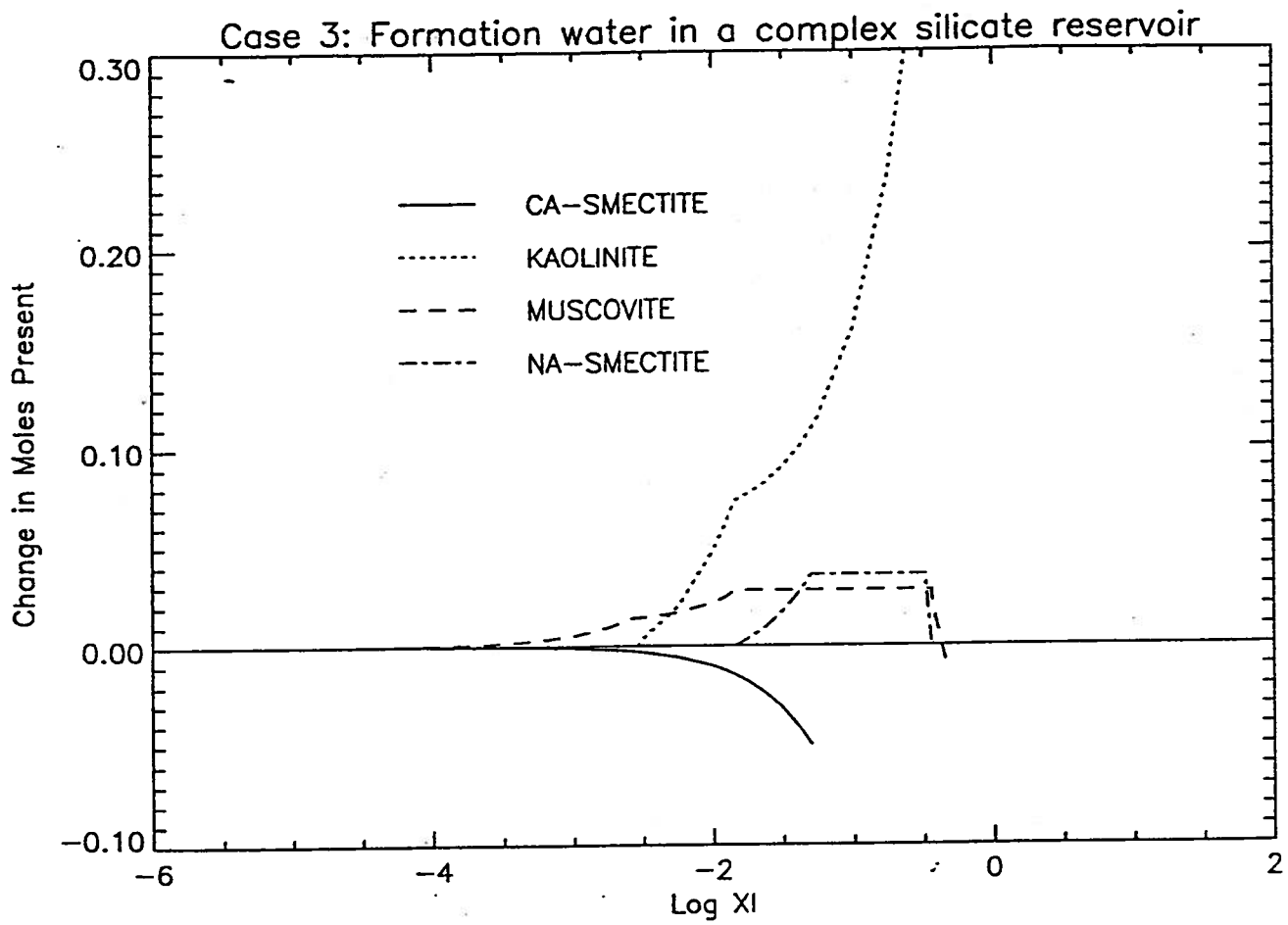


Figure 11.5.13b3

Case 3: Formation water in a complex silicate reservoir

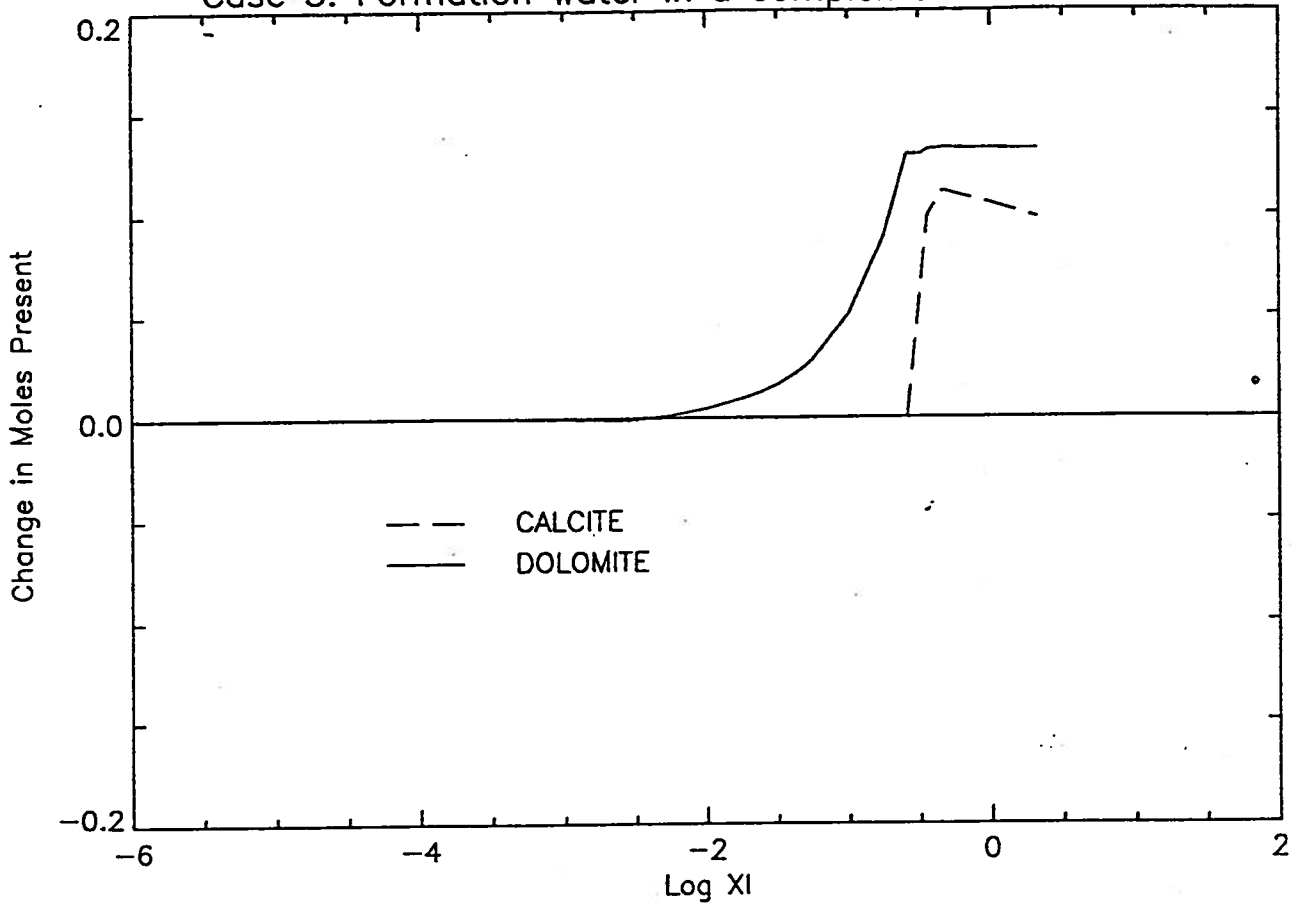


Figure 11.5.13b4

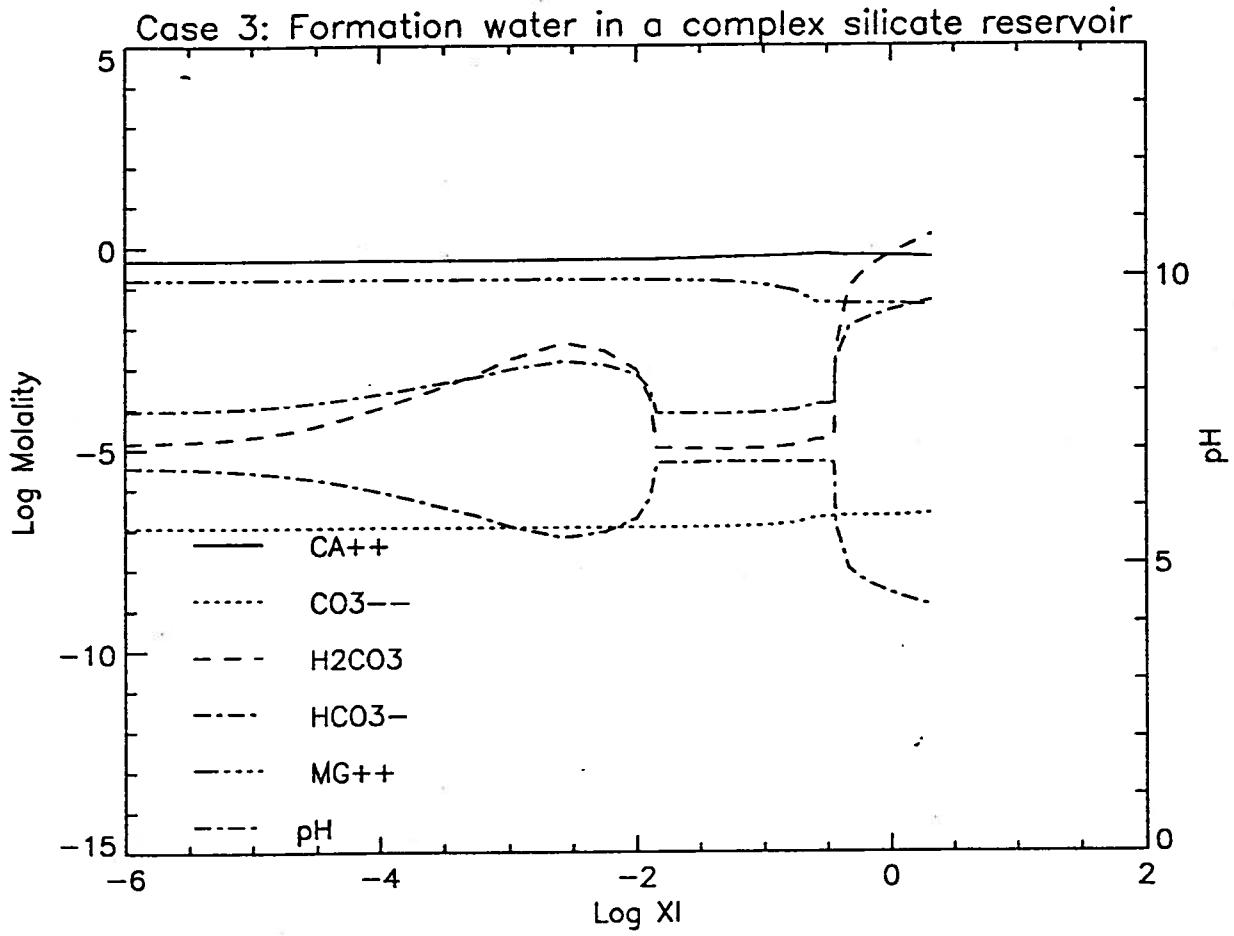


Figure 11.5.13c



### Figure 11.5.14

Reaction of a Brackish Formation Water with an clinochlore-quartz siliciclastic aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').

a: Buildup of the partial pressure of CO<sub>2</sub> in bars.

b1: Molar amount of CO<sub>2</sub> injected into the aquifer & change in the moles of mineral reactants and products.

b2: Change in the moles of mineral products.

c: Change in the molality of the aqueous species.

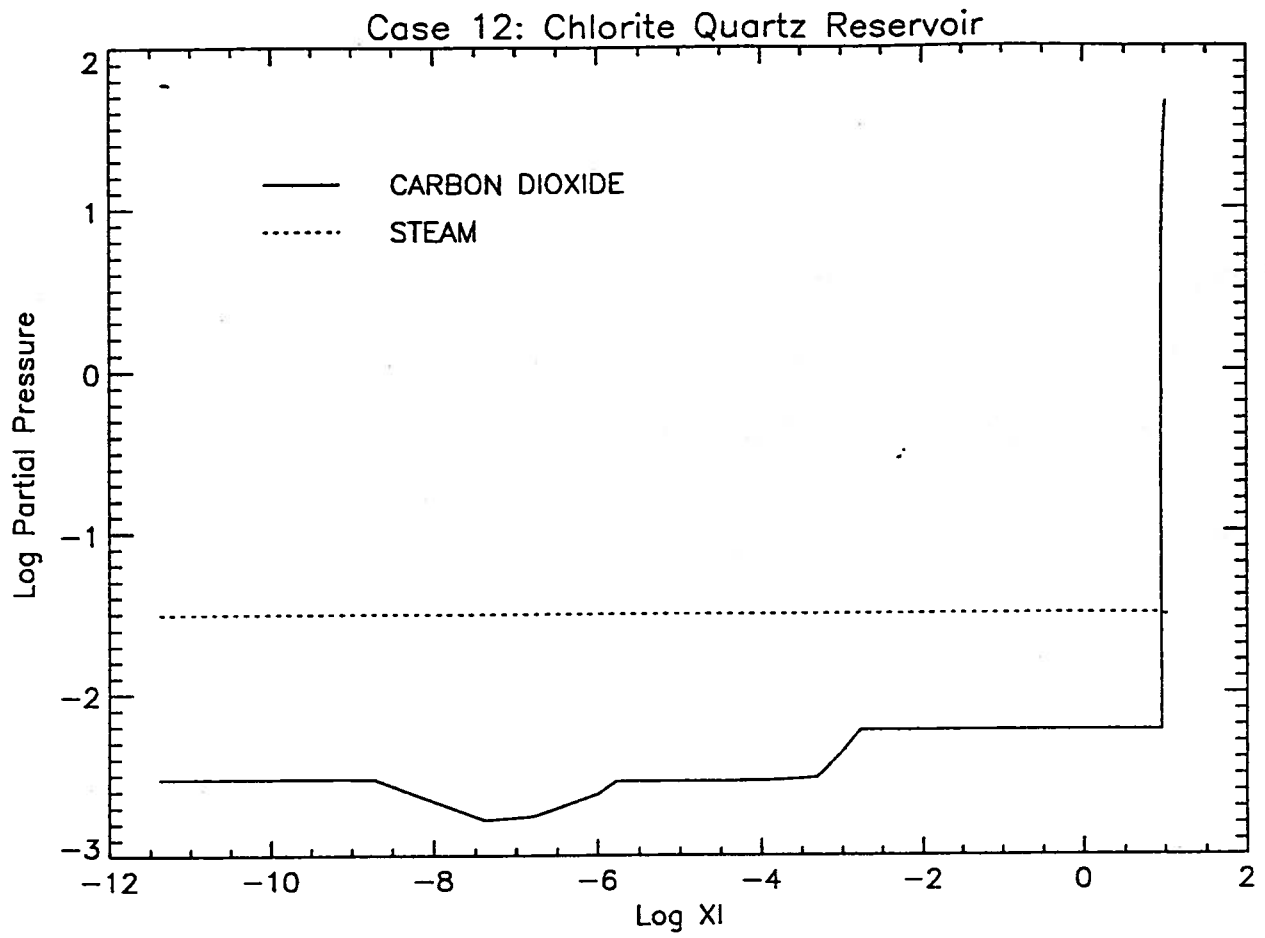


Figure 11.5.14a

Case 12: Chlorite Quartz Reservoir

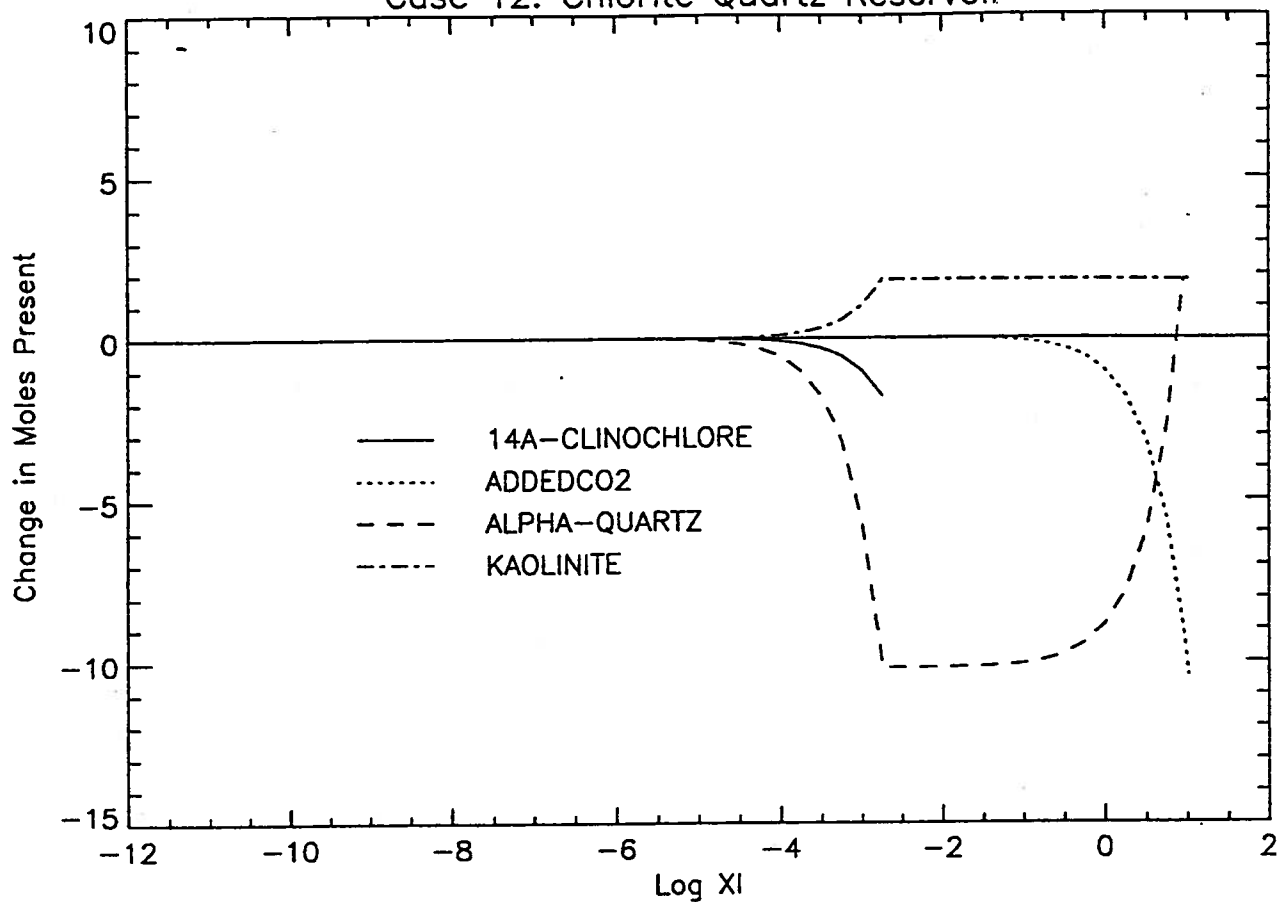


Figure 11.5.14b1

Case 12: Chlorite Quartz Reservoir

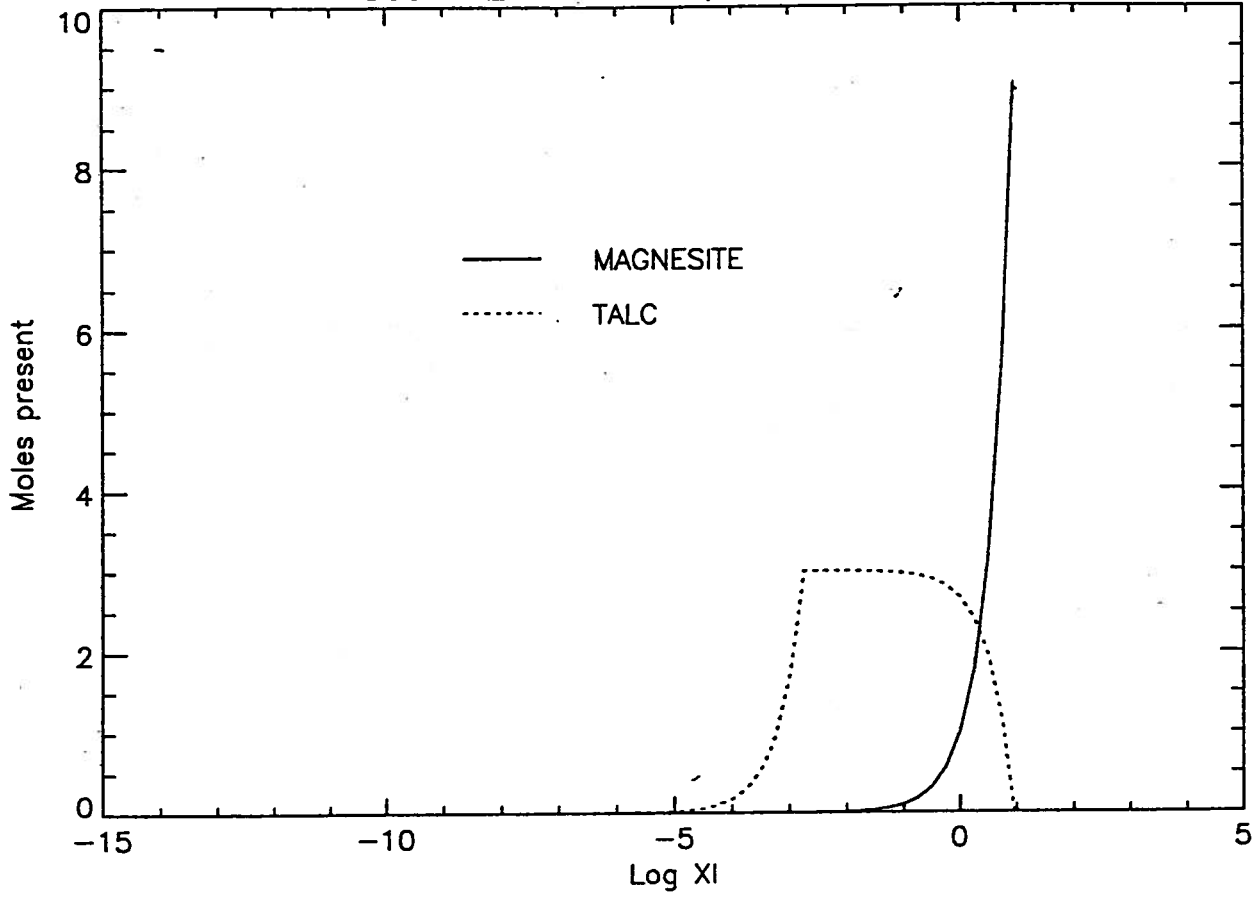


Figure 11.5.14b2

### Case 12: Chlorite Quartz Reservoir

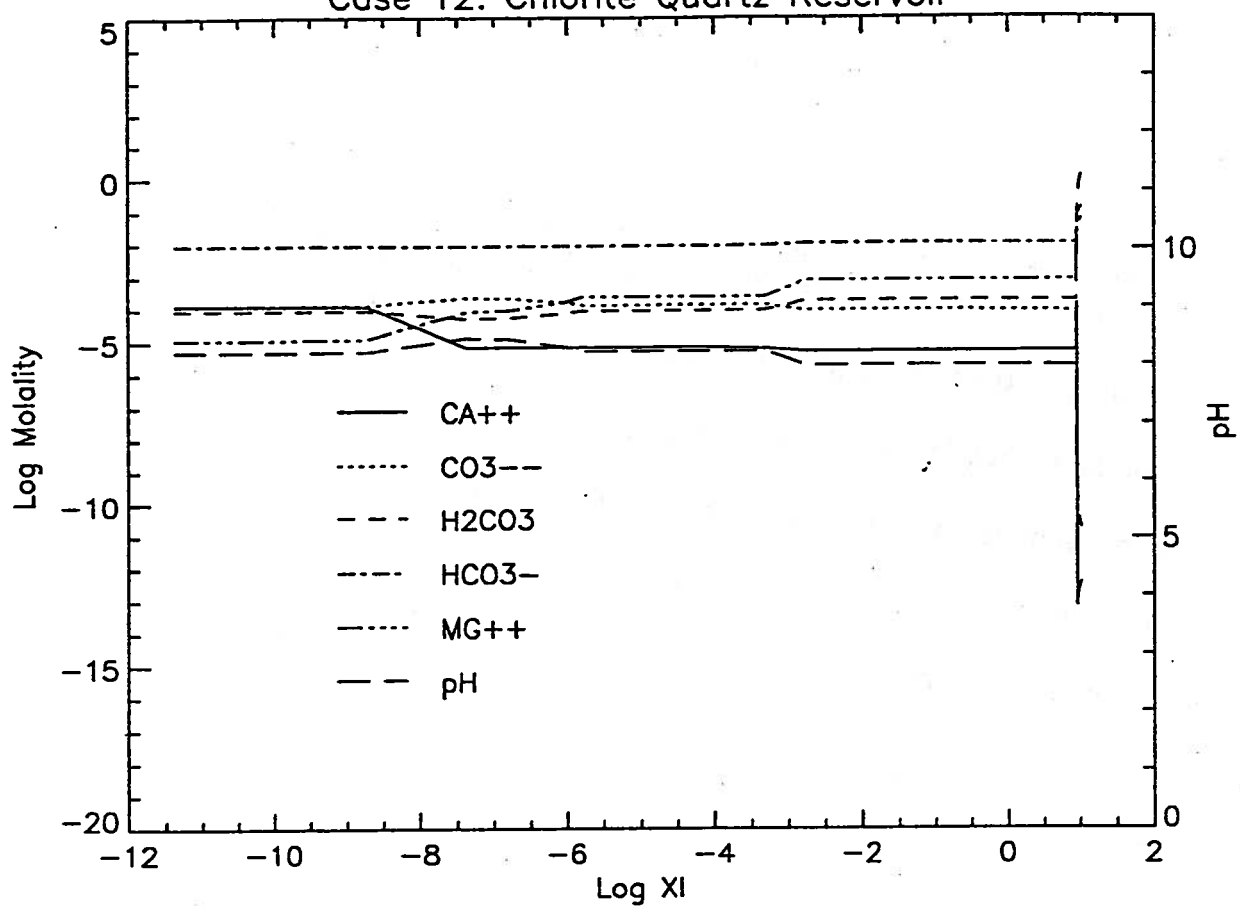


Figure 11.5.14c

**Figure 11.5.15**

Reaction of a Brackish Formation Water with an albite-quartz-illite siliciclastic aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').

a: Buildup of the partial pressure of CO<sub>2</sub> in bars.

b1: Molar amount of CO<sub>2</sub> injected into the aquifer.

b2: Change in the moles of mineral reactants and products.

b3: Change in the moles of mineral products.

c: Change in the molality of the aqueous species.

Case 11: Quartz, Albite, Illite Reservoir

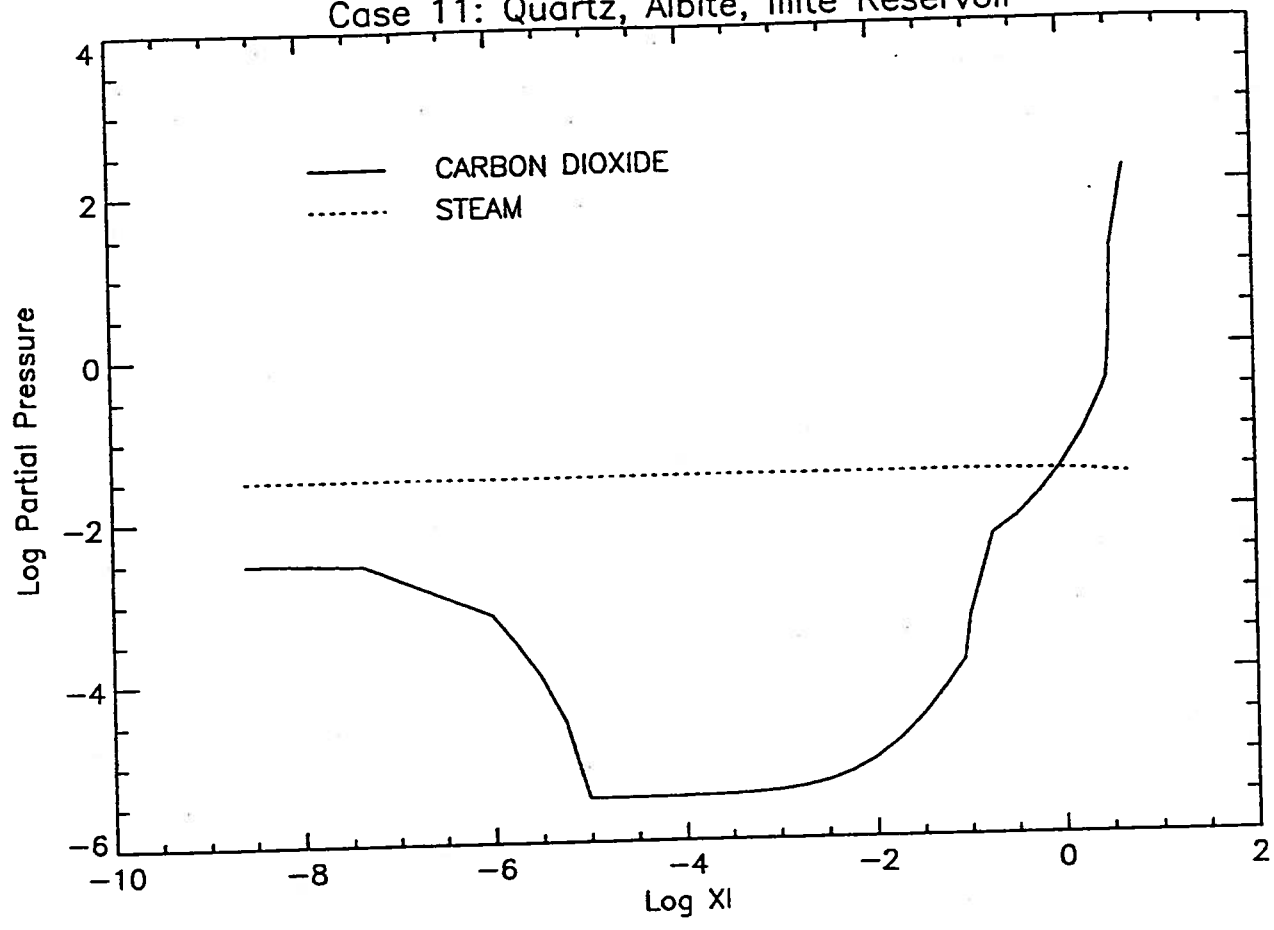


Figure 11.5.15a

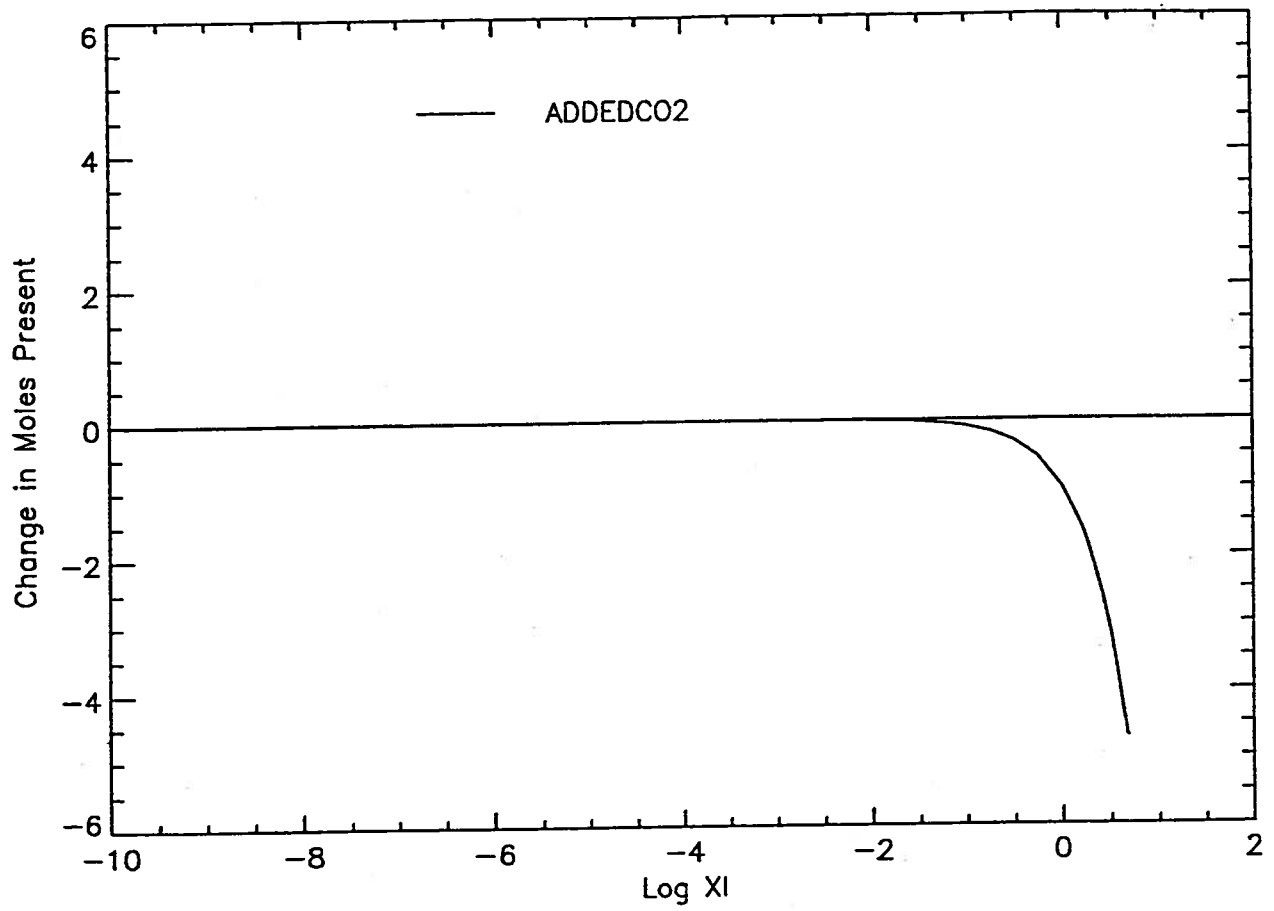


Figure 11.5.15b1



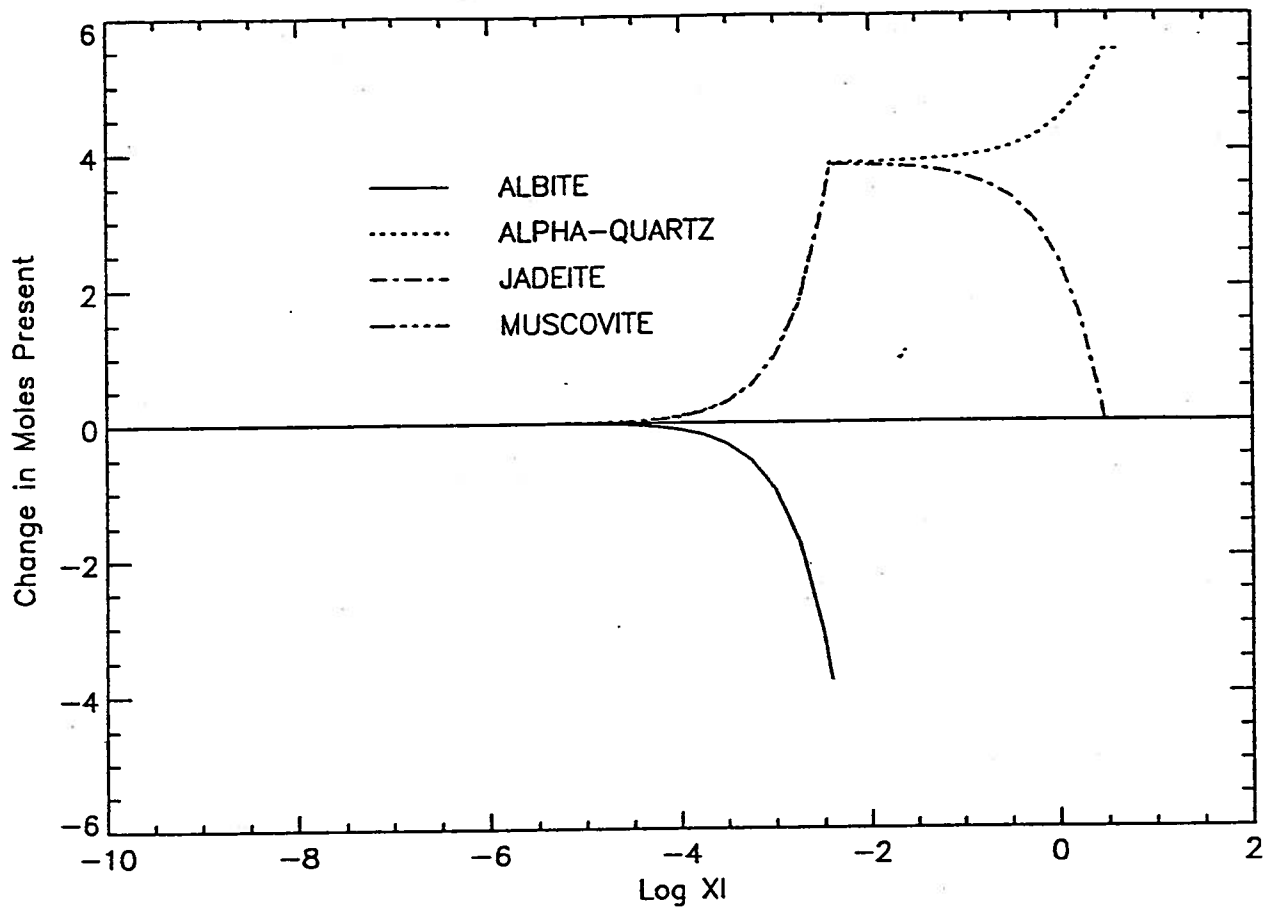


Figure 11.5.15b2

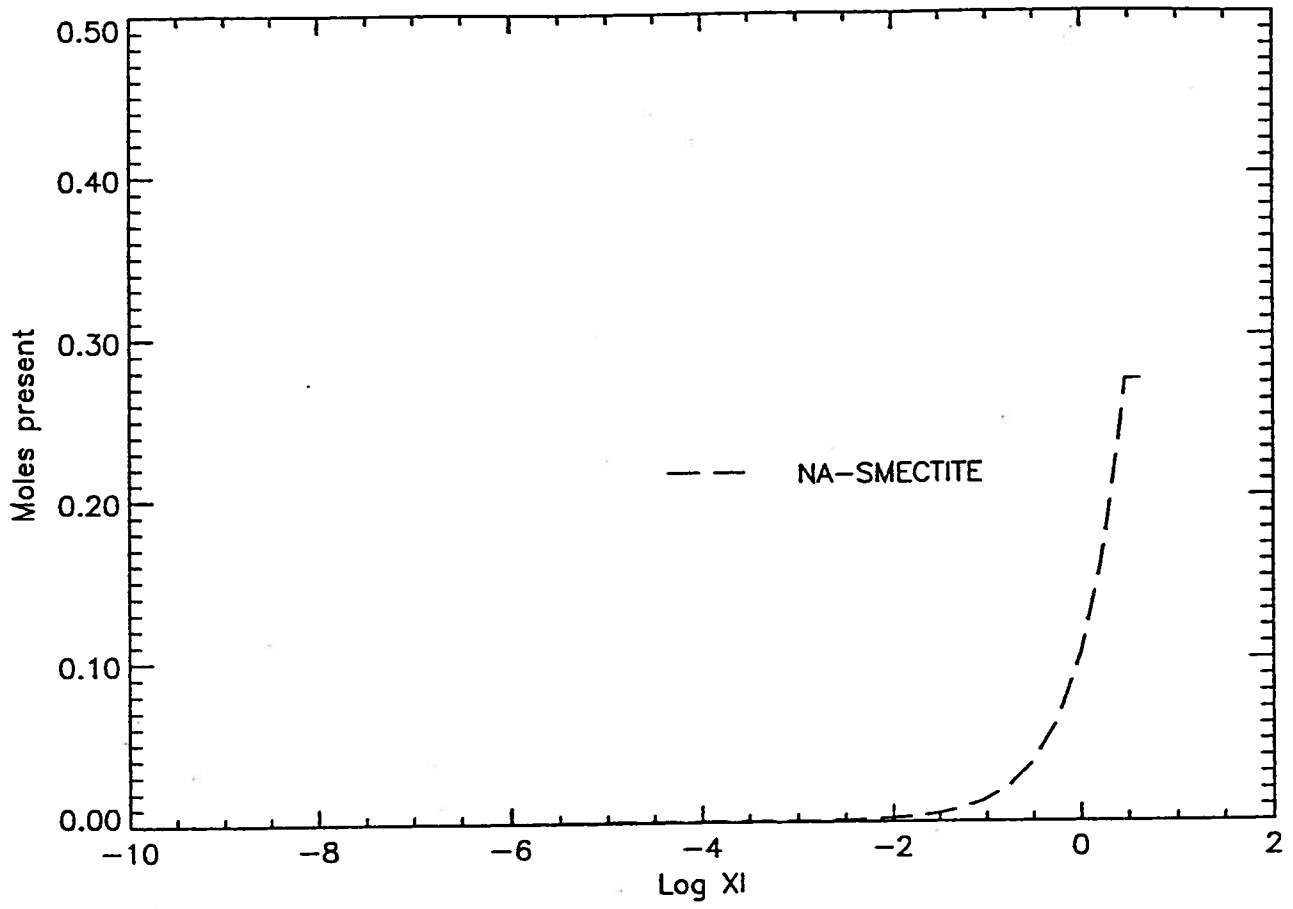


Figure 11.5.15b3

Case 11: Quartz, Albite, Illite Reservoir

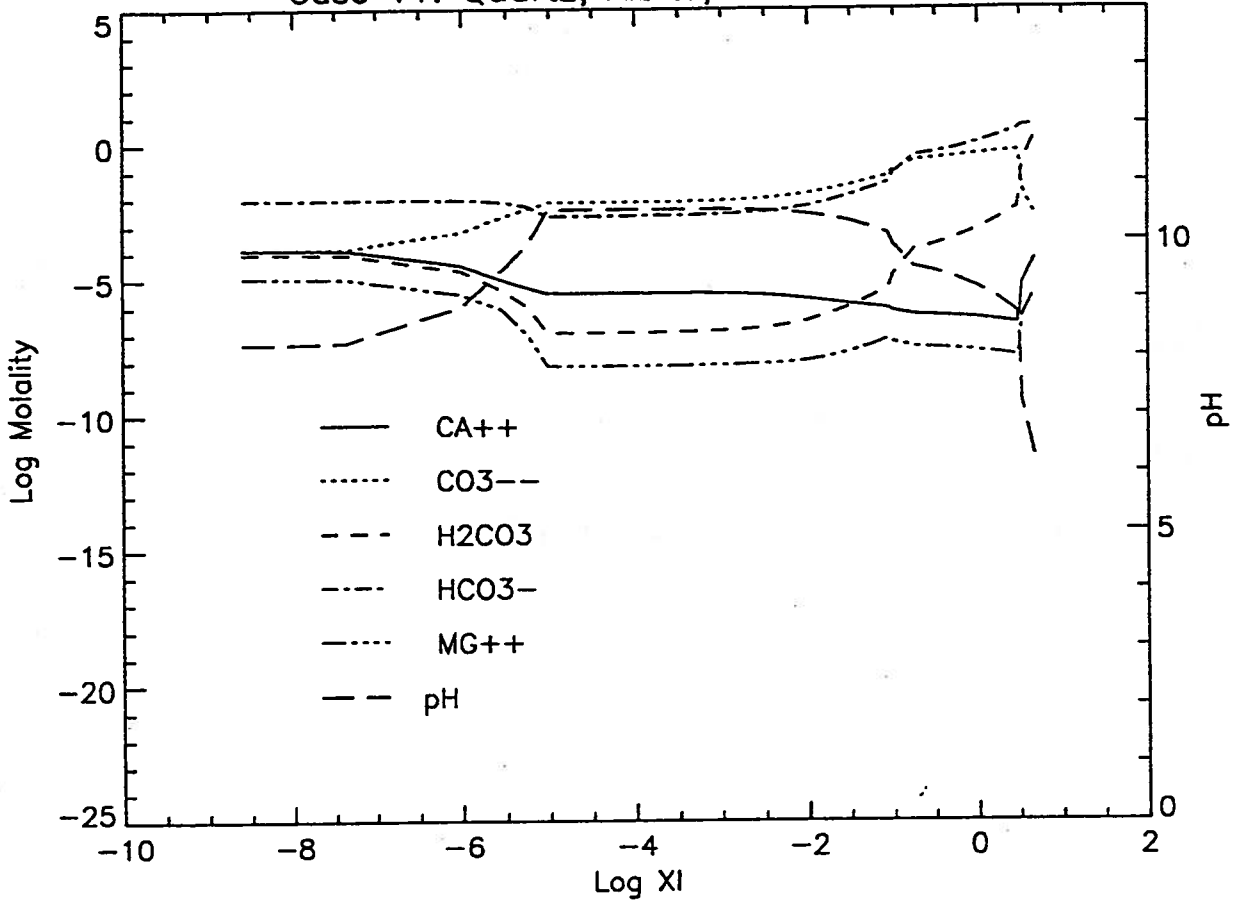


Figure 11.5.15c

### **Figure 11.5.16**

Reaction of a Brackish Formation Water with an K.feldspar-quartz-illite siliciclastic aquifer at 25°C as CO<sub>2</sub> is injected into the aquifer; plotted as a function of time ('X').

a: Buildup of the partial pressure of CO<sub>2</sub> in bars.

b: Molar amount of CO<sub>2</sub> injected into the aquifer & change in the moles of mineral reactants.

c: Change in the molality of the aqueous species.

Case 9: Quartz-Feldspar-Muscovite Reservoir

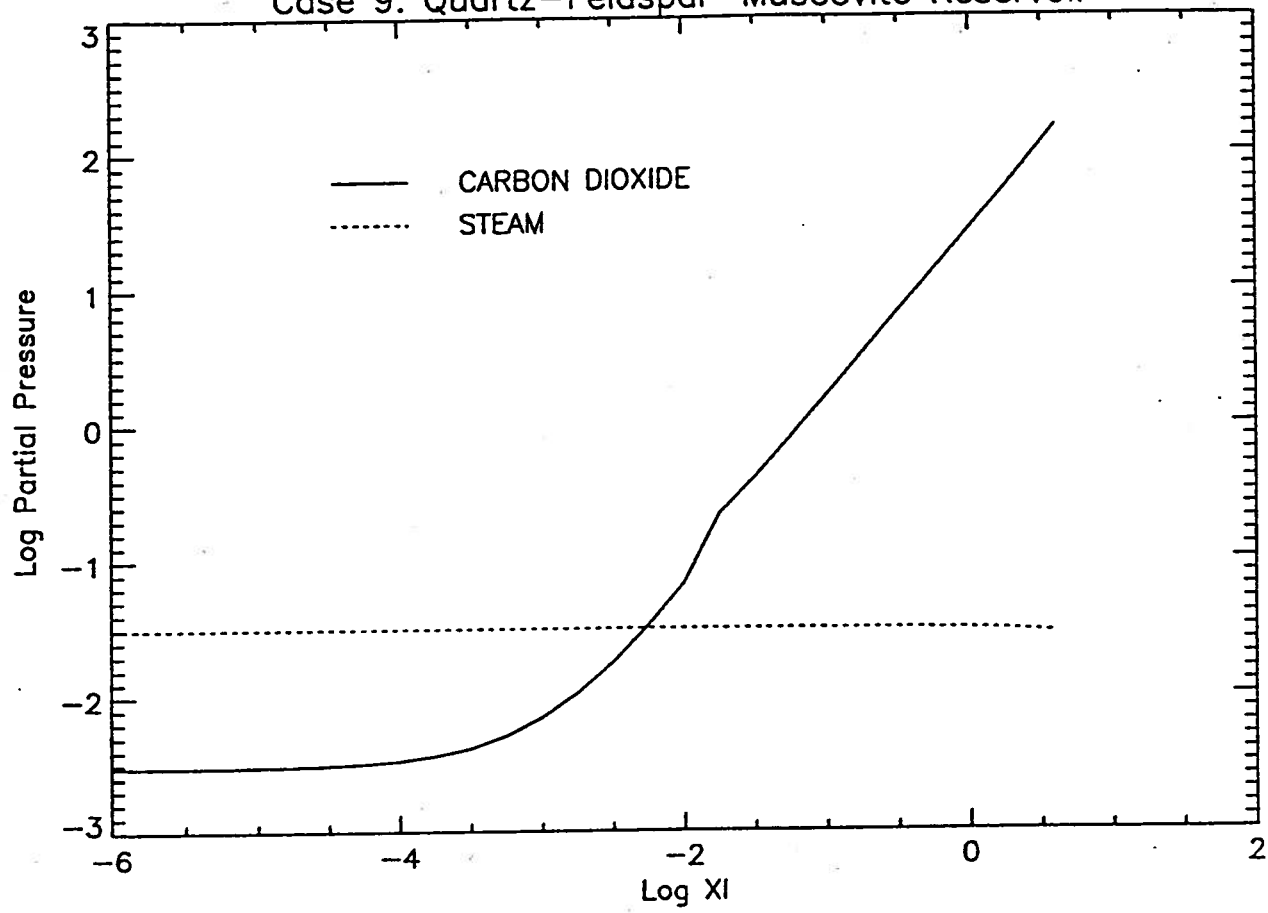


Figure 11.5.16a

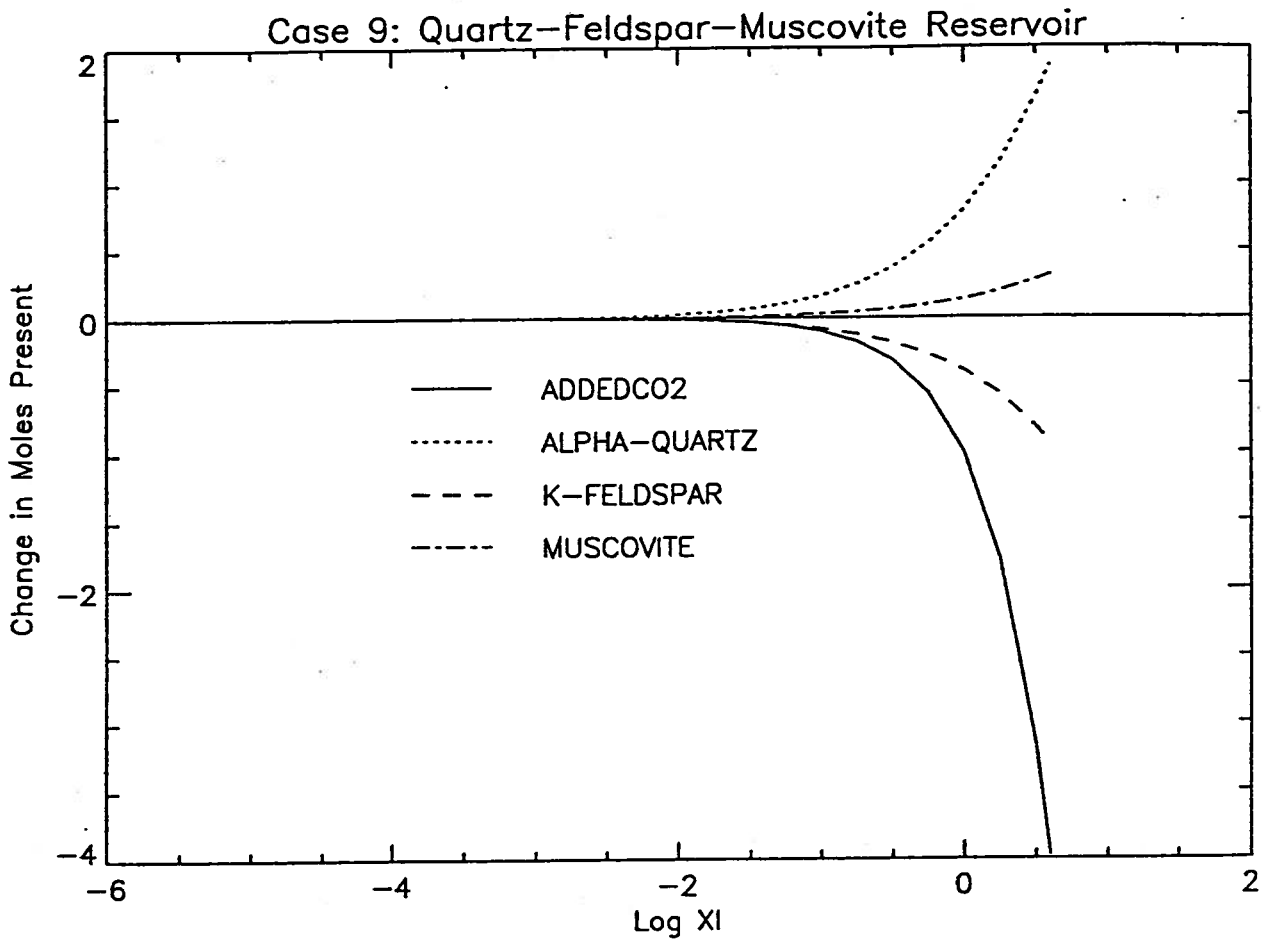


Figure 11.5.16b

Case 9: Quartz-Feldspar-Muscovite Reservoir

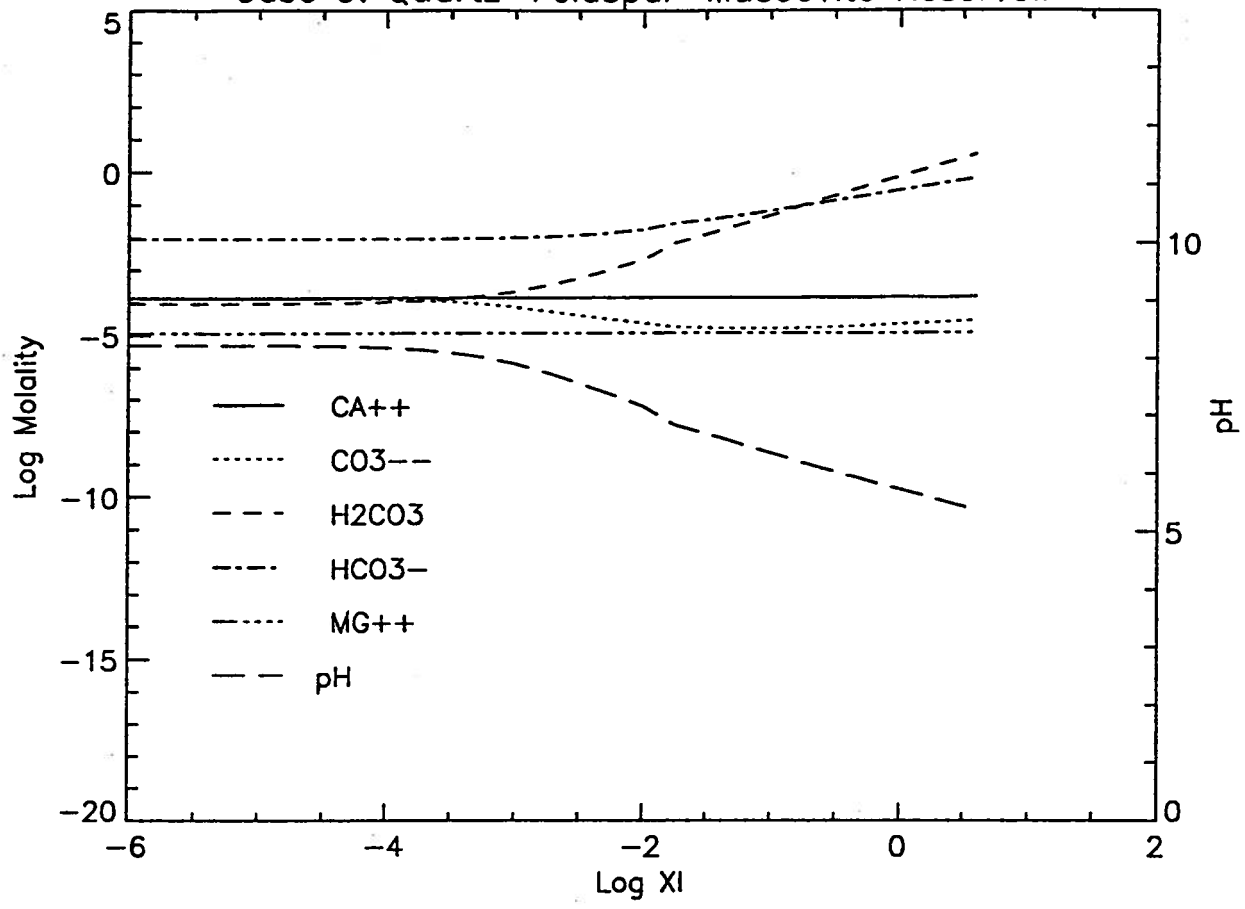


Figure 11.5.16c

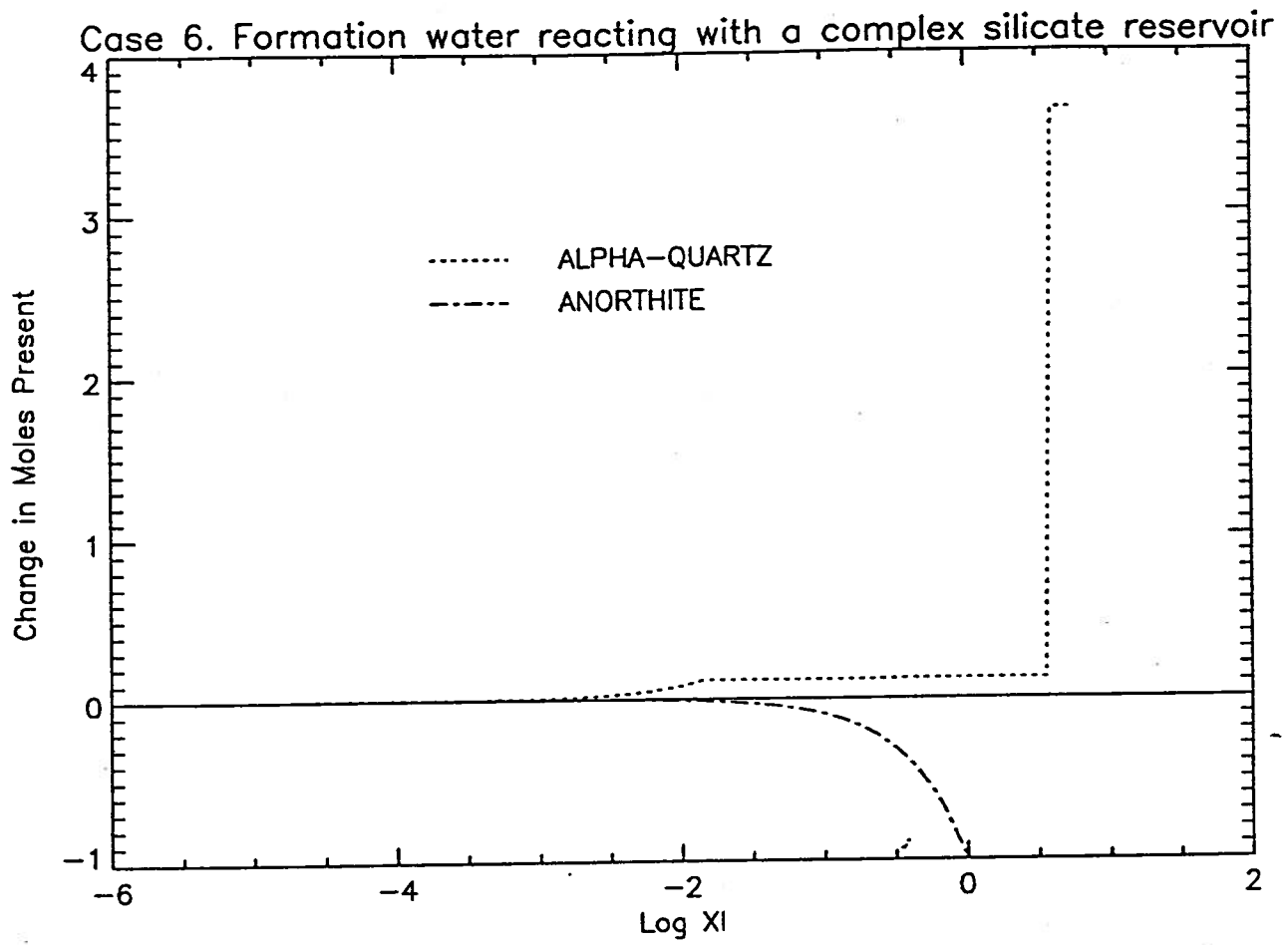


Figure 11.5.12b2



Case 6. Formation water reacting with a complex silicate reservoir

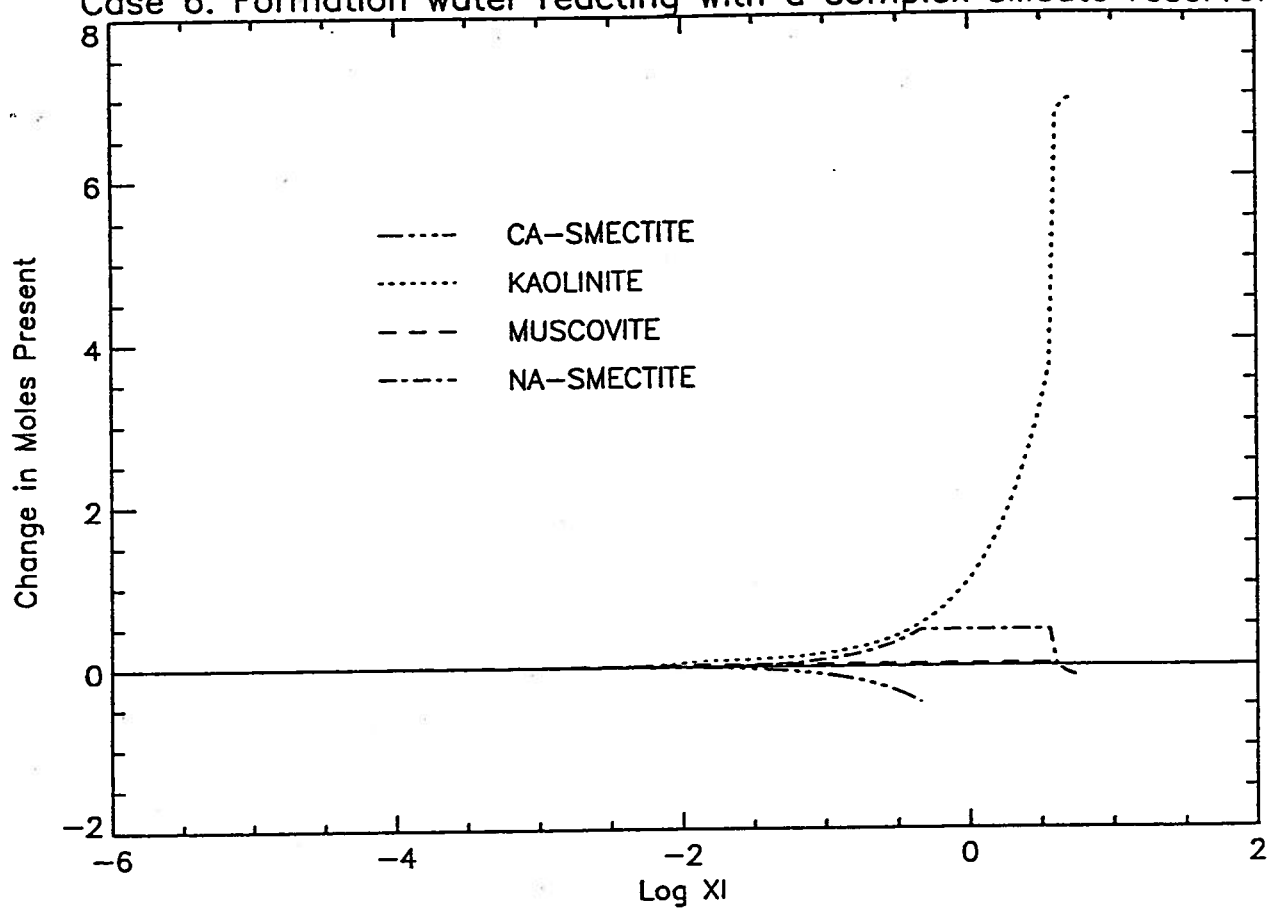


Figure 11.5.12b3

Case 6. Formation water reacting with a complex silicate reservoir

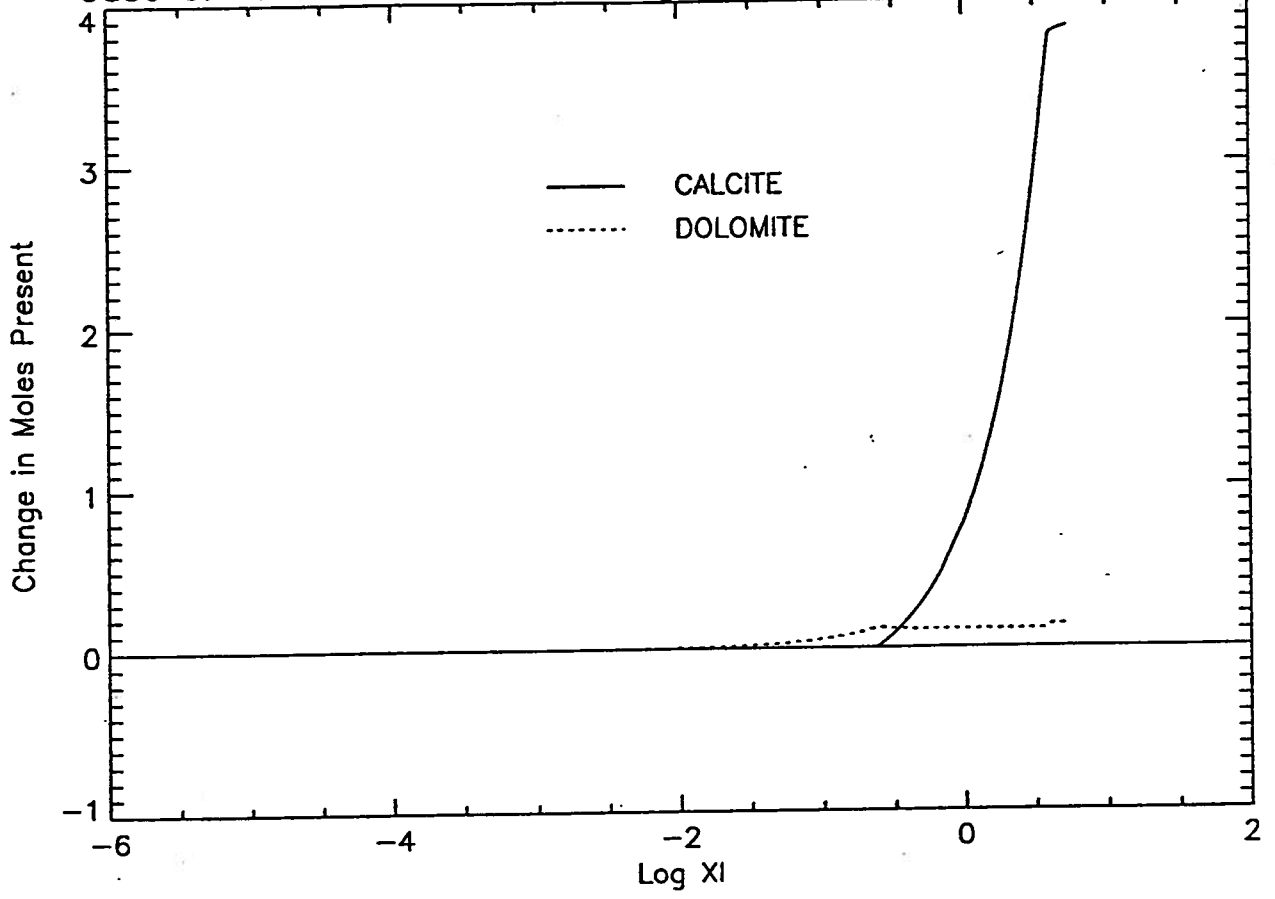


Figure 11.5.12b4

Case 6. Formation water reacting with a complex silicate reservoir

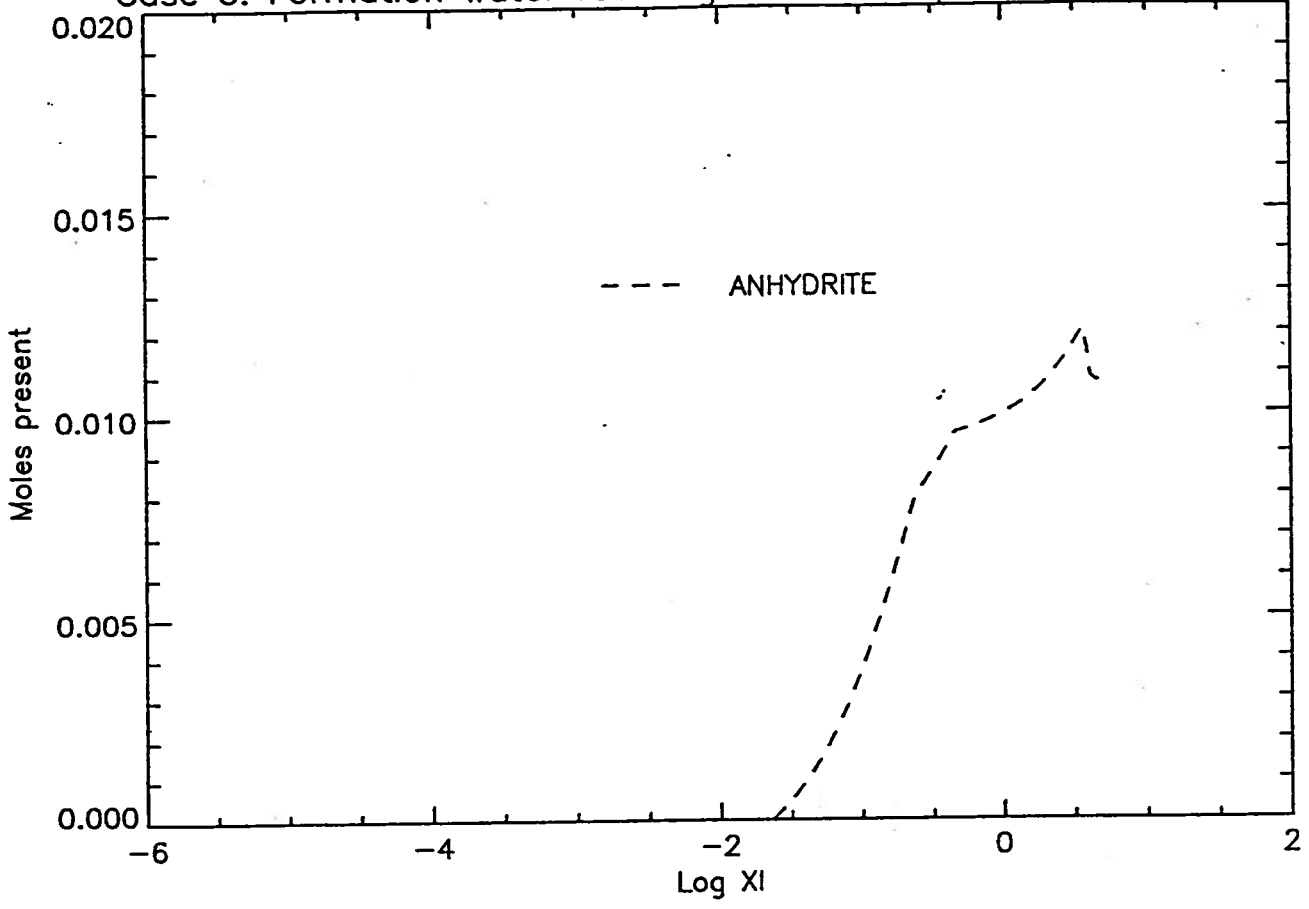


Figure 11.5.12b5

Case 6: Formation water reacting with a complex silicate reservoir

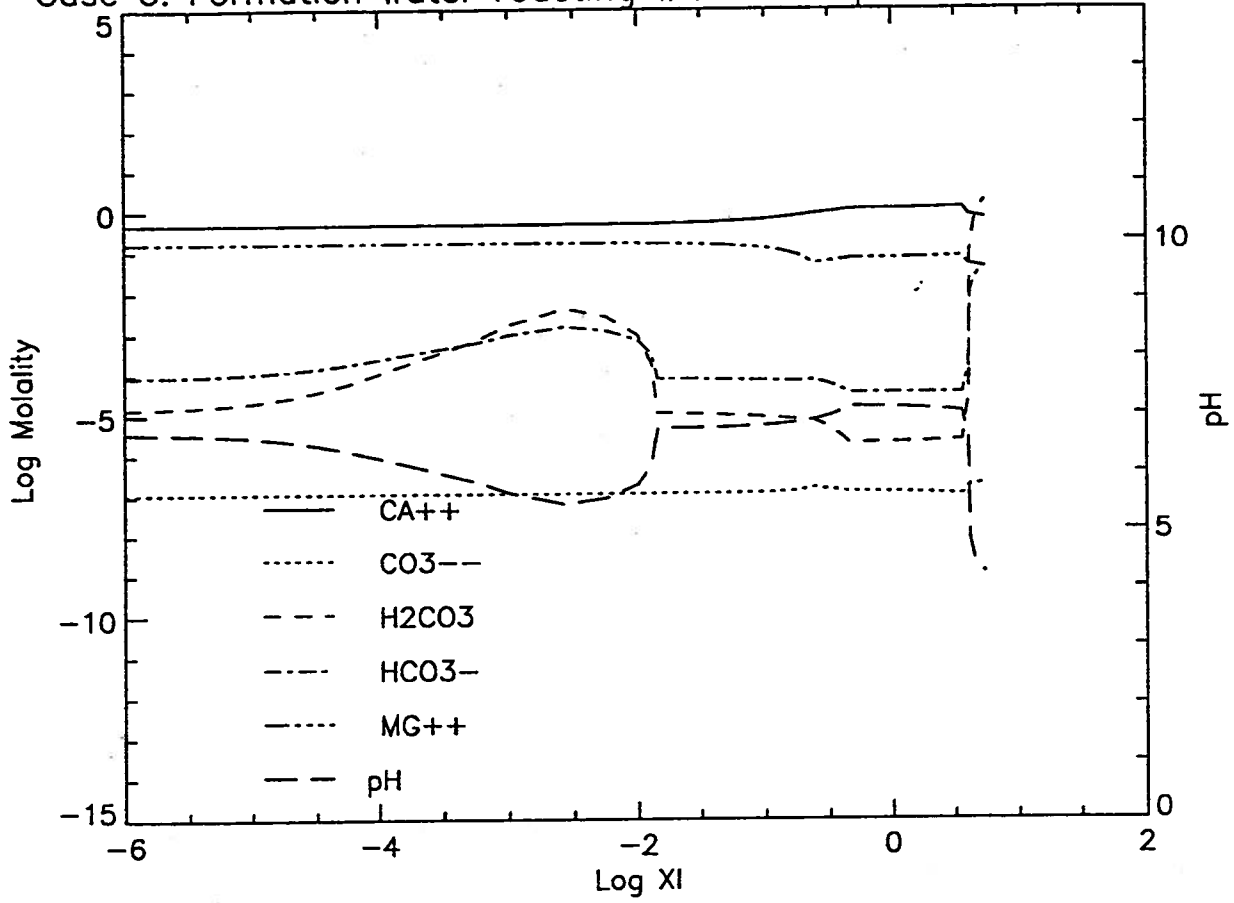


Figure 11.5.12c

**APPENDIX 11.5.b**

**Paper Presented at IEA Conference  
"Carbon Dioxide Disposal"**

- To appear in the Proceedings of the IEA Carbon Dioxide Disposal Symposium at Oxford, England, 29-31 March, 1993.

## AQUIFER DISPOSAL OF CO<sub>2</sub>-RICH GASES: REACTION DESIGN FOR ADDED CAPACITY

WILLIAM D. GUNTER & ERNEST H. PERKINS,  
Alberta Research Council, PO Box 8330, Edmonton, Alberta, Canada, T6H 5X2  
&  
TOM J. McCANN,  
Stanley Industrial Consultants Ltd., Calgary, Alberta, Canada, T2R 1M1

### ABSTRACT

Aquifer disposal of CO<sub>2</sub> is being investigated in a region between the Genesee and Sundance coal-fired power stations, west of Edmonton, Alberta, Canada. This study considers the changes to the mineralogy and water chemistry of both brackish and brine waters in carbonate and siliciclastic aquifers in this area as a result of the injection of CO<sub>2</sub>. The conclusions are general and may be applied to any aquifer.

Brines absorb less CO<sub>2</sub> due to the salting out effect. The reactions between CO<sub>2</sub>, water and aquifer solids in the carbonate aquifers can largely be described in two steps: dissolution of calcite and adsorption of dissolved calcium on clays. The dissolving CO<sub>2</sub> is neutralized to form bicarbonate ion due to the buffering action of the carbonate dissolution while the effect of ion exchange is to minimize the amount of dissolved calcium. In siliciclastic aquifers, the dissolving CO<sub>2</sub> is neutralized by reactions between basic aluminosilicate minerals (i.e. feldspars) and the resulting, more acid reaction products (i.e. kaolinite). Large amounts of carbonate minerals can precipitate during these reactions. The additional capture capacity of CO<sub>2</sub> due to this water-rock interaction has been found to be significant compared to that captured by simple solution of CO<sub>2</sub> in water. Reaction of aqueous CO<sub>2</sub> with calcium and magnesium bearing *basic* minerals in a siliciclastic aquifer can substantially increase the capacity of the aquifer for CO<sub>2</sub> disposal as compared to other aquifer mineralogies.

### KEYWORDS

Carbon dioxide; disposal; greenhouse gases; aquifers; water-rock reactions; mineral sinks.

### INTRODUCTION

There is currently considerable interest in using geological structures (salt domes, brines, coal beds, oil and gas reservoirs, or aquifers), the deep ocean or enhanced oil recovery as sinks for waste gas (particularly CO<sub>2</sub>) disposal. In the short term, enhanced recovery projects can utilize CO<sub>2</sub> if these projects are near the CO<sub>2</sub> source. However in the longer term, deep aquifers appear to offer the best promise for accepting large quantities of waste gases. Their global distribution and their large *disposal volume* are appealing for disposal of waste fluids or gases, particularly from point emission sources (Koide *et al*, 1992; van der Meer, 1992). Carbon dioxide is an ideal candidate for aquifer disposal because of its high density and high solubility in water at the relatively high pressures which may be imposed in aquifers.

Geological CO<sub>2</sub> sinks, depending upon the time scale, may be classified as reactive or inert. Clearly, reactive sinks are the most effective for permanent long term disposal. Injection into aquifers and the subsequent dissolution into the water increases the reactivity of CO<sub>2</sub> considerably. In addition, flow

through porous media in the crust promotes natural mixing and exposure of the dissolved CO<sub>2</sub> to additional grain surfaces where reactions can take place.

In this paper, the primary focus is on the generic documentation of the enhancement of CO<sub>2</sub> capture by reactive sinks through water-rock interaction, and builds from Dunsmore's (1992) suggestions for the use of calcium and magnesium brines. We distinguish three scenarios in the use of aquifers for the disposal of CO<sub>2</sub>: (1) The solution of CO<sub>2</sub> into a formation fluid in the absence of formation mineralogy; (2) The solution of CO<sub>2</sub> and reaction with the minerals present in a carbonate aquifer; (3) The solution of CO<sub>2</sub> and reaction with the minerals in a siliciclastic aquifer. These reaction scenarios are based on aquifers close to two coal fired power plants.

### AREA CHOSEN FOR STUDY

A region west of Edmonton, Alberta, Canada between the Sundance and Genesee power plants, covering a few townships (Township 49-52, Range 3-5, W5Mer) was selected as a desirable site for CO<sub>2</sub> disposal. Based on the general stratigraphy in the sedimentary strata in this area of the Alberta Basin (Porter *et al.*, 1982) regional siliciclastic and carbonate aquifers were identified at depths between 1400 and 2000 m. These aquifers are deep enough to be part of regional flow systems, isolated from the surface by extensive regional aquitards, yet relatively shallow in order to minimize drilling costs. The aquifers selected for evaluating CO<sub>2</sub> disposal are the carbonate Wabamun (Devonian) and the sandstone Lower Mannville (Cretaceous) Formations. Both aquifers have average permeabilities, porosities and thicknesses in the range of 2 md, 10% and 100 meters respectively. Based on these aquifer depths, an injection pressure of CO<sub>2</sub> in the order of 15MPa must be used to inject the CO<sub>2</sub>. At these pressures, CO<sub>2</sub> would be injected in a liquid or supercritical state.

### FORMATION WATER CHEMISTRY AND WATER-ROCK RATIO

Formation water analyses and cored intervals from the 754 wells within the area were extracted from the AGSWDB (Alberta Geological Survey well database). The formation water analyses were culled mechanically and then manually screened, resulting in 135 representative analyses from both carbonate and clastic stratigraphic units. From this dataset, two waters (brackish and a brine) were chosen as the basis for the modelling, representing extremes in TDS (i.e. approximately 4,000 versus 100,000 ppm). Sodium, potassium, calcium, magnesium and chloride are all more than an order of magnitude higher in the brine while sulphate is three times higher and bicarbonate is actually lower. The actual composition chosen for modelling depended on corrections applied to bring the formation water into equilibrium with the formation using the computer code SOLMINEQ.88 (Kharaka *et al.*, 1988; Perkins *et al.*, 1990) and simplification of the formation water chemistry pertinent to the end-member mineralogy being modeled.

The water-rock ratio in the aquifer is calculated from the porosity. Using an average porosity of 10% and an average rock density of 2.5, there are approximately 22,000 grams of rock per 1000 grams of water. Even if the porosity is doubled to 20%, the weight of rock would only be reduced to 10,000 grams. For the former case, the presence of 5 wt% of a mineral phase would account for 1000 grams of that phase being contacted by 1000 grams of water.

### MODELLING OF WATER-ROCK REACTIONS

Modelling of water-rock reactions was carried out at an aquifer temperature of 25°C on stoichiometric end-member mineralogies (i.e. quartz and pure Na-, K-, Ca-, Mg- minerals) using the mass transfer geochemical computer code PATH.ubc (Perkins, 1980) and GeoCalc (Brown *et al.*, 1989). PATH.ubc calculates the path of water-rock reaction for a given set of reactants as a function of the progress variable, 'XI' which is proportional to time. As 'XI' progresses, the reactants dissolve into the formation water, resulting in a different formation water composition. The change in formation water composition may be buffered by the precipitation (or dissolution) of the equilibrium phases or by the formation of new

equilibrium phases. Often an equilibrium phase is formed but later completely reacts out, and none is left in the system. PATH.ubc terminates when equilibrium has been achieved with all of the reactant phase(s) and/or when all of the reactant phase(s) have reacted out. Final equilibrium with the injected CO<sub>2</sub> is defined as when the partial pressure of CO<sub>2</sub> in equilibrium with the formation fluid has reached 15 MPa. This value was chosen as it is representative of the pressure of liquid CO<sub>2</sub> necessary for injection into the selected aquifers.

## CO<sub>2</sub> SOLUBILITY IN BRACKISH WATER OR IN BRINE

If carbon dioxide is dissolved into either a brine water (i.e. TDS is greater than 100,000 mg/l) or brackish water (i.e. TDS lies between 1000 and 10,000 mg/l) with no formation minerals present, no new minerals are precipitated. The water becomes more acidic and the amount of dissolved carbon dioxide is only a function of pressure and of fluid composition. A salting out effect occurs as the water becomes more concentrated. The basis for these results is shown through the following model simulations.

CO<sub>2</sub> was numerically dissolved stepwise into the brackish formation water of ionic strength 0.063 at 25°C. Fig. 1, curve a, shows the rise in CO<sub>2</sub> pressure as increments of CO<sub>2</sub> are added. A CO<sub>2</sub> pressure of 15MPa was reached after 4 moles of CO<sub>2</sub> had been added to each 1000 grams of water.

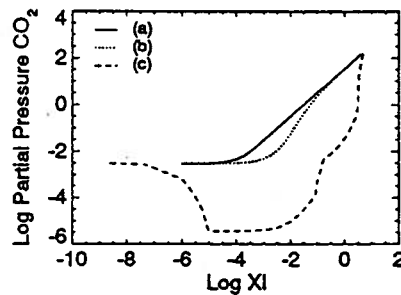


Fig. 1: Buildup of the partial pressure of CO<sub>2</sub> in bars as a function of time ('XI'): (a) in brackish formation water; (b) in brackish formation water in a calcite-dolomite aquifer with ion exchange; (c) in brackish formation water in an albitic (i.e. Na-rich) siliciclastic aquifer.

In contrast, the total CO<sub>2</sub> added to reach a CO<sub>2</sub> pressure of 15MPa is approximately 2 moles per 1000 grams of water for the brine formation water (ionic strength 4.00), just half of the amount added to the brackish formation water. This *salting out effect* is due to the increasing importance of hydration with salt content. As the ionic strength of the formation water increases to that of a brine, the activity coefficient of H<sub>2</sub>CO<sub>3</sub> increases from 1 to 2. Obviously to maximize CO<sub>2</sub> solubility, dilute formation waters are favoured.

## CO<sub>2</sub> UPTAKE IN CARBONATE AQUIFERS

If carbon dioxide is dissolved in a fluid in equilibrium with a carbonate formation (the formation mineralogy is comprised of calcite and/or dolomite, possibly with minor amounts of quartz present), the total amount of carbon dioxide dissolved into the fluid is greater than the previous case, but no new minerals are precipitated. In fact, the formation carbonate minerals dissolve into the fluid and partially neutralize the acid created by the addition of the carbon dioxide. The dominate reaction for calcite can be written as:





Two aquifer mineralogies were chosen to model this reaction: a pure dolomite-calcite aquifer and a dolomite-calcite-quartz aquifer. Both were reacted with the brackish formation water. The curves for the pure dolomite-calcite aquifer are almost identical to those of the pure formation water example (compare curve a, Fig. 1 to Fig. 2a) because only a small amount of calcite and dolomite have dissolved by the time equilibrium is reached (0.004 moles of dolomite and 0.05 moles of calcite; see Fig. 2c). This causes the concentration of bicarbonate ion to substantially increase (Fig. 2b) which results in an increase of approximately 1.5% or 0.06 moles of  $\text{CO}_2$  gas dissolved (Fig. 2d) when compared to the pure formation water case.

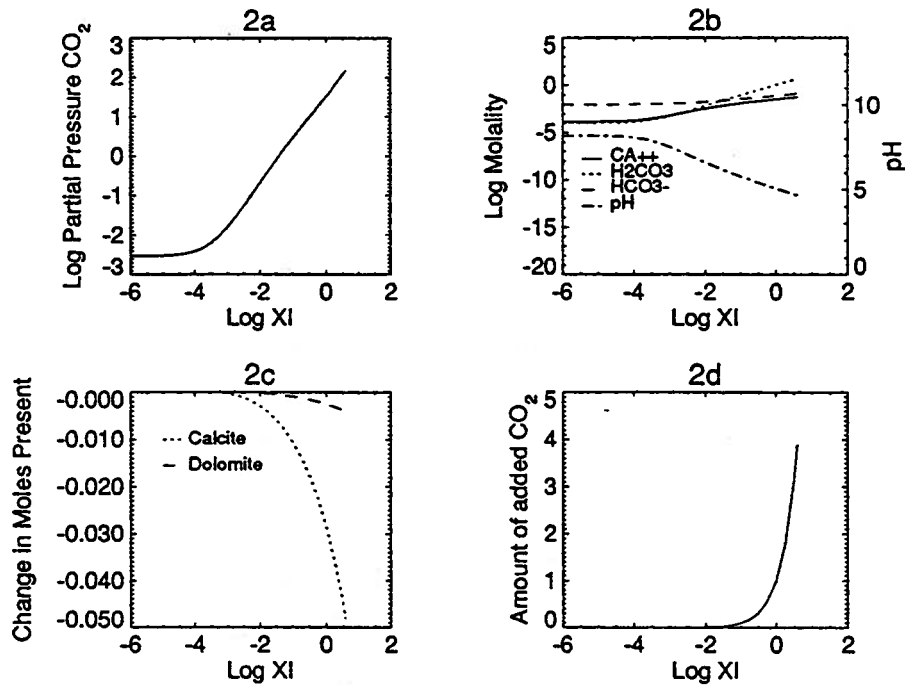
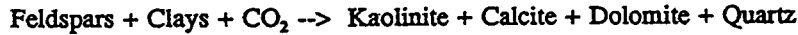


Fig. 2: Reaction of brackish formation water with a calcite-dolomite carbonate aquifer as  $\text{CO}_2$  is injected into the aquifer; plotted as a function of time ('Xi'): (a) buildup of the partial pressure of  $\text{CO}_2$  in bars; (b) change in the molality of the aqueous species; (c) change in the moles of mineral reactants; (d) molar amount of  $\text{CO}_2$  injected into the aquifer.

The amount of additional  $\text{CO}_2$  which can be added to a calcite-dolomite-quartz aquifer is identical to the calcite-dolomite aquifer. The quartz dissolves to saturation and is unaffected by the addition of the  $\text{CO}_2$ . No new phases are formed and the same amounts of calcite and dolomite are dissolved. In the case of a calcium-rich brine, the same conclusions hold except the amount of  $\text{CO}_2$  and calcite dissolved is less when compared to the brackish formation water. Consequently, depending upon the specific formation water chemistry, reaction of a carbonate formation can result in an increase of dissolved carbon dioxide by 1 to 4%. If clays are present with a high cation exchange capacity, they will buffer the calcium and magnesium in the formation water, allowing more calcite and dolomite to dissolve. This is shown by the depression of the  $\text{CO}_2$  - 'Xi' curve (curve b, Fig. 1). This effect is most pronounced for low ionic strength formation waters where the  $\text{CO}_2$  capture can be increased to 2 to 8%.

## $\text{CO}_2$ UPTAKE IN SILICICLASTIC AQUIFERS

Siliciclastic aquifers containing basic silicate minerals (i.e. anorthitic feldspar, chlorite, albitic feldspar and potassium feldspar) can absorb more  $\text{CO}_2$  (see Gunter and Bird, 1988, for an explanation) than other aquifers through a complex set of water-rock reactions. These reactions can be summarized in a general sense by the reaction of feldspar and clay silicate minerals with  $\text{CO}_2$ :



The reactant clays are comprised of both illites, chlorites and smectites. The final ratio and the respective amounts of calcite and dolomite is dependent upon the initial formation mineralogy and formation water composition. The more feldspars and clays initially present, the more carbonate minerals produced as reaction products and the more carbon dioxide trapped in the formation. Generally, we have chosen to take a simple approach to modelling the effect of the four end-member basic silicates on  $\text{CO}_2$  uptake. We have represented the aquifer solids as a three phase mixture; excess quartz (representing the dominant phase in the aquifer solids) and 1000 grams (i.e. 5 wt%) of each of the basic end-member silicate (i.e. anorthite, chlorite, albite and potassium feldspar) and other clays (note that we used muscovite as a proxy for the clay mineral illite).

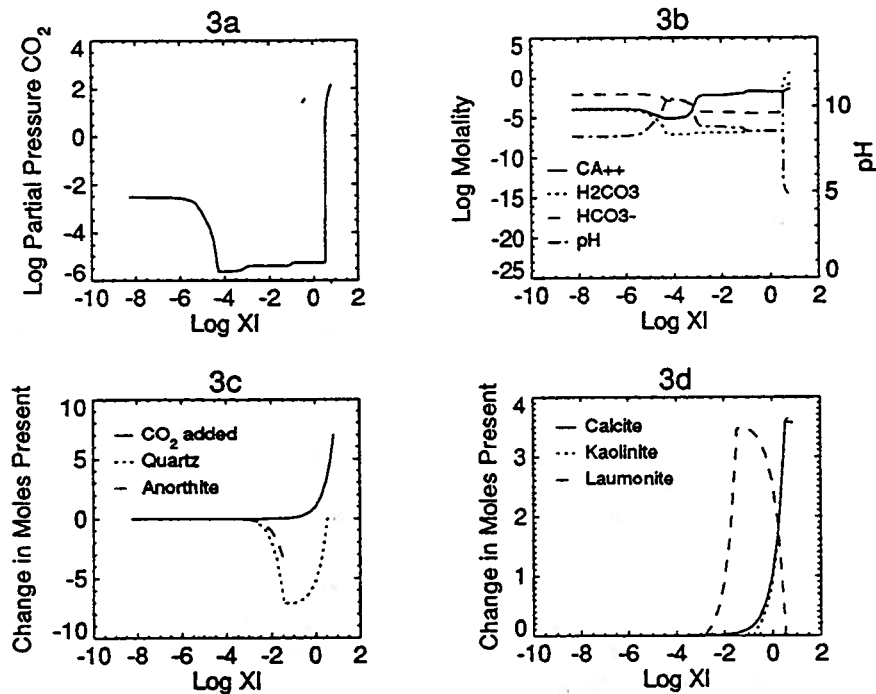


Fig. 3: Reaction of brackish formation water with an anorthite-muscovite-quartz siliciclastic aquifer as  $\text{CO}_2$  is injected into the aquifer; plotted as a function of time ('XI'): (a) buildup of the partial pressure of  $\text{CO}_2$  in bars; (b) change in the molality of the aqueous species; (c) change in the moles of the initial formation mineralogy and the amount of  $\text{CO}_2$  injected into the aquifer; (d) change in the moles of mineral products.

To model the effects of  $\text{CO}_2$  addition to a formation mineralogy rich in calcium, the three phase assemblage, anorthite, muscovite and quartz, was allowed to react with  $\text{CO}_2$  in a brackish formation water. The calculated reaction paths are complex with anorthite and quartz initially reacting to form laumontite (Fig. 3c & d). Muscovite is stable and little reaction occurs. Once all of the anorthite has reacted out, the laumontite then breaks down to form kaolinite, calcite and quartz. The reaction progress can be followed by monitoring the partial pressure of  $\text{CO}_2$  in Fig. 3a or the change in the aquifer water chemistry in Fig. 3b. The first part of the curve is similar to that for no water-rock reaction; flat. However instead of a steep rise, the  $\text{CO}_2$  sharply drops to a flat minimum, as first the pH is buffered to more basic conditions and then as calcite precipitates. Each plateau in the minimum of the  $\text{CO}_2$  curve marks the loss or precipitation of a new phase. The  $\text{CO}_2$  pressure starts to rise sharply to the final imposed pressure only after all the laumontite has reacted out. At this point there is no source of calcium left to form calcite,

thus allowing the level of carbonate (dissolved CO<sub>2</sub>) in solution to increase rapidly. In addition, a small amount of calcite will dissolve as the CO<sub>2</sub> pressure builds up to 15 MPa. Approximately four moles of CO<sub>2</sub> have precipitated as calcite (Fig. 3d). The amount of CO<sub>2</sub> locked up in the aquifer has doubled when compared to the non-reactive or to the carbonate aquifer cases. If the mass of available anorthite had been increased, more CO<sub>2</sub> could have been trapped by the continued precipitation of calcite. Although not shown here, modelling the effect of temperature, a formation brine and/or a complex calcium-rich mineral assemblage support these conclusions.

The magnesium-rich siliciclastic aquifers were modelled as a mixture of clinocllore (i.e. chlorite) and quartz. The results are similar to the calcium-rich ones, except that magnesium-rich silicate minerals form and breakdown; the magnesium released finally combining with CO<sub>2</sub> to form magnesite. The final assemblage is quartz, magnesite and kaolinite. Over 9 moles of CO<sub>2</sub> have been trapped by the precipitation of magnesite. This emphasizes the earlier results that the actual amount of CO<sub>2</sub> locked up by precipitation of carbonate minerals is limited only by the amount of basic calcium and magnesium silicate minerals present in the aquifer solid assemblage.

The sodium-rich siliciclastic aquifers were modelled as a mixture of 5 wt% of albite and muscovite in the presence of excess quartz. As was observed in previous simulations, the muscovite behaved inertly. The final equilibrium assemblage is muscovite, quartz and sodium smectite. The kaolinite stability field was never reached because the large sodium build up in the formation fluid stabilized smectite. The CO<sub>2</sub> pressure curve (Fig. 1, curve c) rises from the minimum much earlier than for the Ca- or Mg- cases (Fig. 3a) because no carbonate phases precipitate. Final CO<sub>2</sub> takeup is 5 moles, of which 4.4 moles is present in the form of bicarbonate ion and 1.6 moles as dissolved CO<sub>2</sub>. Even though the initial formation water was a brackish formation water, the buildup of the bicarbonate ion increases the ionic strength from 0.063 to 4.41. This results in a significant salting out effect for the dissolved CO<sub>2</sub>. The observed concentration of bicarbonate is more than an order of magnitude higher than calculated for the calcium- or magnesium-rich siliciclastic aquifers. The buildup of bicarbonate cannot occur for the calcium or magnesium cases because of early saturation with calcite, magnesite and/or dolomite.

The effects of CO<sub>2</sub> addition to a dilute formation water in a potassium-rich siliciclastic reservoir were modelled using a formation composed of 5 wt% of each potassium feldspar and muscovite, in the presence of excess quartz. Under these conditions, the potassium feldspar reacted to form muscovite and quartz, both of which remained in equilibrium with the fluid during the addition of CO<sub>2</sub>. The pressure of CO<sub>2</sub> climbed steadily similar to the carbonate aquifer case (Fig. 1, curve b) as it was not affected significantly by the mineral reactions. The potassium subsystem is by far the least reactive of all of the siliciclastic systems considered under high CO<sub>2</sub> pressures; the final bicarbonate ion concentration reaches only 0.6 molal. Although this is considerably higher than its calcium and magnesium counterparts, it is only a fraction of the concentrations reached by the sodium analogue simulation. Consequently, siliciclastic aquifers dominated by potassium accessory phases would not enhance the CO<sub>2</sub> uptake significantly above the 4 moles dissolved in the inert (mineral absent) aquifer case.

## SUMMARY AND CONCLUSIONS

The modelling results indicate that brackish and dilute formation waters in aquifers can take up more CO<sub>2</sub> than brine formation waters; thus brackish or dilute formation waters are favoured for CO<sub>2</sub> capture. The maximum solubility of CO<sub>2</sub> is limited in brines due to the salting-out effect at higher ionic strengths.

The reaction of the mineralogy and formation water for a carbonate aquifer with injected CO<sub>2</sub> does not significantly increase the CO<sub>2</sub> uptake. However, if the carbonate aquifer contains significant amounts of clays with a large cation exchange capacity, the final CO<sub>2</sub> capture capacity will be a little greater than for a clay-absent carbonate aquifer.

The maximum amount of CO<sub>2</sub> can be trapped in a siliciclastic aquifer containing a brackish formation water. The amount of trapped CO<sub>2</sub> is dependent upon the amount of and type of basic minerals (feldspars and clays) present in the formation. Magnesium- and calcium-rich siliciclastic aquifers

are favoured for neutralization and trapping of the injected CO<sub>2</sub> through the precipitation of calcite (calcium carbonate), dolomite (calcium magnesium carbonate) or magnesite (magnesium carbonate). The amount of CO<sub>2</sub> captured can be increased through formation of aqueous complexes and precipitation by more than a factor of two over solubility in a brackish formation water. The exact amount depends upon the amount of available calcium and/or magnesium in the formation minerals and the pressure of CO<sub>2</sub>. Sodium-rich siliciclastic aquifers will absorb CO<sub>2</sub>, neutralizing it to form bicarbonate ions and thus converting the brackish chloride formation water to a bicarbonate brine. The increase in CO<sub>2</sub> solubility due to formation of bicarbonate is only partially balanced by the salting out effect due to the increased ionic strength. Thus a sodium rich formation mineralogy may be favoured as a disposal site when the precipitation of carbonate minerals must be avoided. Potassium-rich siliciclastic aquifers equilibrate more rapidly than their sodium counterparts and only limited amounts of bicarbonate ion are formed. Thus CO<sub>2</sub> capture is not enhanced significantly for potassium-rich siliciclastic aquifers.

One concern which has not been addressed in this paper is that the most efficient capture mechanism (i.e. carbonate mineral precipitation) may reduce the permeability of the reservoir. Detailed examination of permeability changes are beyond the scope of this paper as they depend upon the permeability and the porosity of the aquifer, the amount and surface area of the reactive minerals available, the kinetics of the reactions and on the attachment sites of the mineral products. This is not the case for carbonate aquifers because only dissolution occurs. Thus the porosity and permeability must increase in these reservoirs as CO<sub>2</sub> is injected. The net change in porosity can be calculated for siliciclastic aquifers but not the permeability. However, in the early stage of reaction in the siliciclastic reservoirs, dissolution is the predominate mechanism. From this, we can conclude that in the near well region of a CO<sub>2</sub> injection well, permeability and porosity should increase. Resolution of the permeability changes in a siliciclastic reservoir can only be addressed by physical simulation using core plugs under the actual conditions of aquifer disposal; where CO<sub>2</sub>-charged water would be flowed through an aquifer core at different rates and the permeability changes monitored as a function of time.

The reactions considered in this paper have been numerically simulated using a closed system reaction type of geochemical model in which the calculation is normalized to one liter of water. These calculations are limited because they assume a closed environment of reaction. In reality, CO<sub>2</sub> disposal should be modelled in the context of the hydrodynamics of a sedimentary basin. In a sedimentary basin, deep groundwater moves on the order of one centimeter to one meter a year. The basins are typically hundreds of kilometers across, so basinal water movement is measured in thousands of years. During that time, the CO<sub>2</sub>-charged formation waters will be exposed to a much larger mass of solids than assumed for the modelling carried out here. Consequently, over periods of thousands of years, the reaction between the *basic* minerals in the aquifers will be responsible for capture of more CO<sub>2</sub> than predicted by our model calculations. This will limit the mobility of the CO<sub>2</sub> to a smaller radius than would otherwise be expected. These effects of an open system should be evaluated and included as part of any aquifer model used for assessing the long term effects of CO<sub>2</sub> aquifer disposal.

The CO<sub>2</sub> capture potential and the geochemical reactions discussed in this report are part of a preliminary engineering feasibility study to examine the fixation of CO<sub>2</sub> in carbonate and siliciclastic aquifers. In parallel, scoping experiments in autoclaves are being undertaken to verify the results of the numerical modelling reported here. The experiments are the subject of a separate communication. The feasibility of injection, the sustainable injection rates and the long term pressure effects on a model Alberta aquifer in the area of the Genesee and Sundance power plants have already been determined. Based on these results, preliminary designs and conceptual cost estimates to implement aquifer disposal of CO<sub>2</sub> are being undertaken.

#### ACKNOWLEDGEMENTS

Ian Webster, IEA, was a great help in identifying and helping with sources of potential funding for this project. Wayne Nesbitt, University of Western Ontario, helped us with the analysis of the effect of a clay exchanger. Stefan Bachu, ARC, provided us with the aquifer data in the Sundance and Genesee power plant areas. Finally we would like to thank our sponsors and their representatives on the management

committee - Alberta Energy (D.E. Macdonald), Environment Canada (V.R. Marwaha), CANMET (F.M. Mourits), TransAlta (M.M. McDonald) and Edmonton Power (Doug Heaton). The conclusions reached in this paper do not necessarily reflect the view of the sponsors.

#### REFERENCES

Brown, T.H., R.G. Berman and E.H. Perkins (1989). PTA-SYSTEM: A GeoCalc software package for the calculation and display of activity-temperature-pressure phase diagrams. *Amer. Min.*, 74, 485-487.

Dunsmore, H.E. (1992). A geological perspective on global warming and the possibility of carbon dioxide removal as calcium carbonate mineral. *Energy Convers. Mgmt.*, 33, 565-572.

Gunter, W.D. and G.W. Bird (1988). CO<sub>2</sub> production in tar sands reservoirs under in situ steam temperatures: reactive calcite dissolution. *Chemical Geology*, 70, 301-311.

Kharaka, Y.K., W.D. Gunter, P.K. Aggarwal, E.H. Perkins and J.D. DeBraal (1988). SOLMINEQ.88: A computer program for geochemical modelling of water-rock reactions. U.S. Geol. Surv. Water-Resources Investigations Report 88-4227, Menlo Park.

Koide, H., Y. Tazaki, Y. Noguchi, S. Nakayama, M. Iijima, K. Ito and Y. Shindo (1992). Subterranean containment and long-term storage of carbon dioxide in unused aquifers and in depleted natural gas reservoirs. *Energy Convers. Mgmt.*, 33, 619-626.

Perkins, E.H. (1980). *A reinvestigation of the theoretical basis for the calculation of mass transfer in geochemical processes involving aqueous solutions*. MSc Thesis, University of British Columbia, Vancouver.

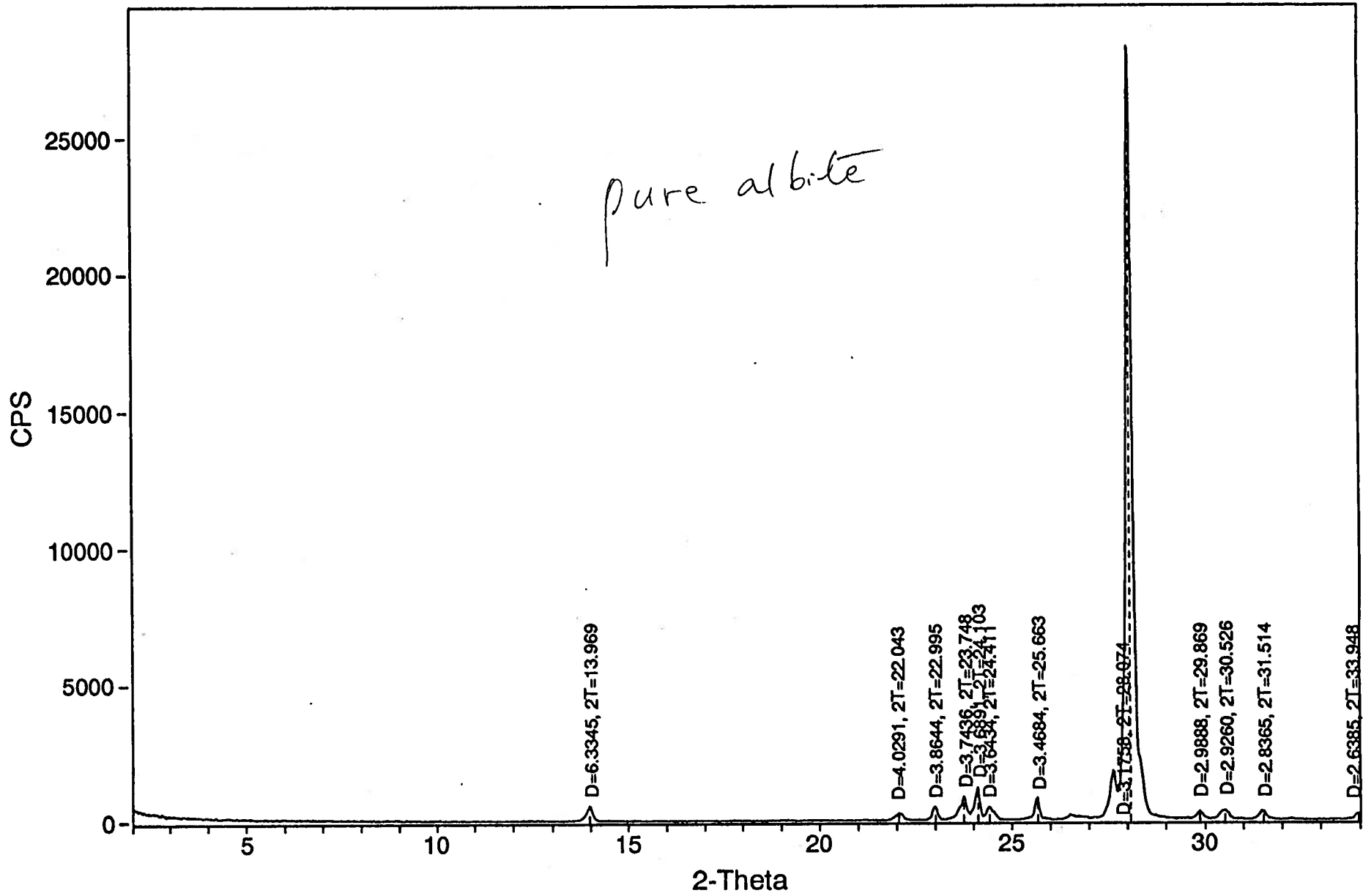
Perkins, E.H., Y.K. Kharaka, W.D. Gunter and J.D. DeBraal (1990). Geochemical modelling of water-rock interactions using SOLMINEQ.88. In: *Chemical Modelling of Aqueous Systems II* (eds. D.C. Melchior and R.L. Bassett), Chap. 9, pp. 117-127, ACS symposium series 416, Washington, D.C.

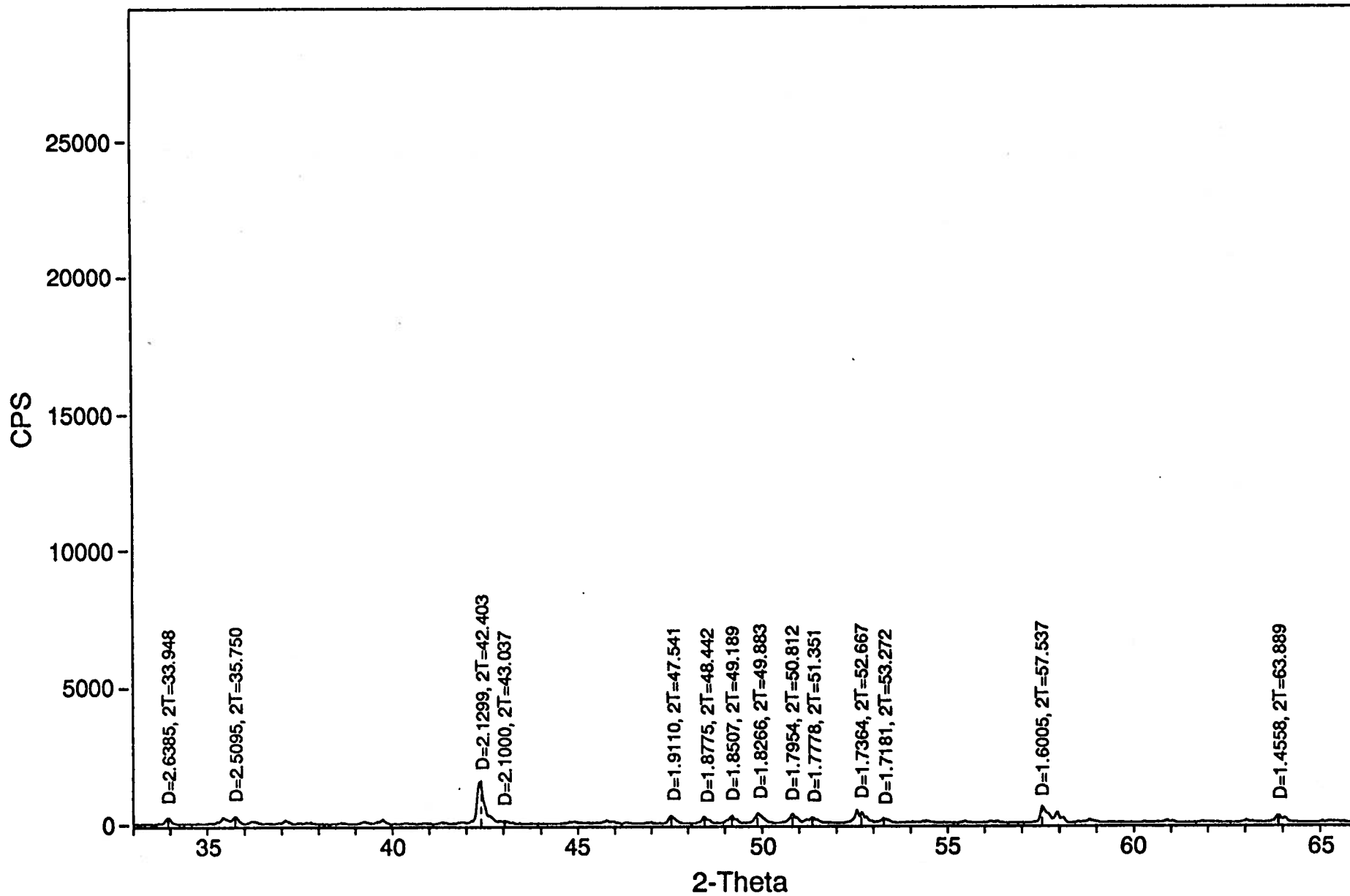
Porter, J.E., J.A. Price and R.G. McCrossan (1982). The western Canada sedimentary basin. *Philosophical Transactions of the Royal Society of London, Series A*, 305, 169-192.

van der Meer, L.G.H. (1992). Investigations regarding the storage of Carbon Dioxide in Aquifers in the Netherlands. *Energy Convers. Mgmt.*, 33, 611-618.

## **APPENDIX 11.6.1**

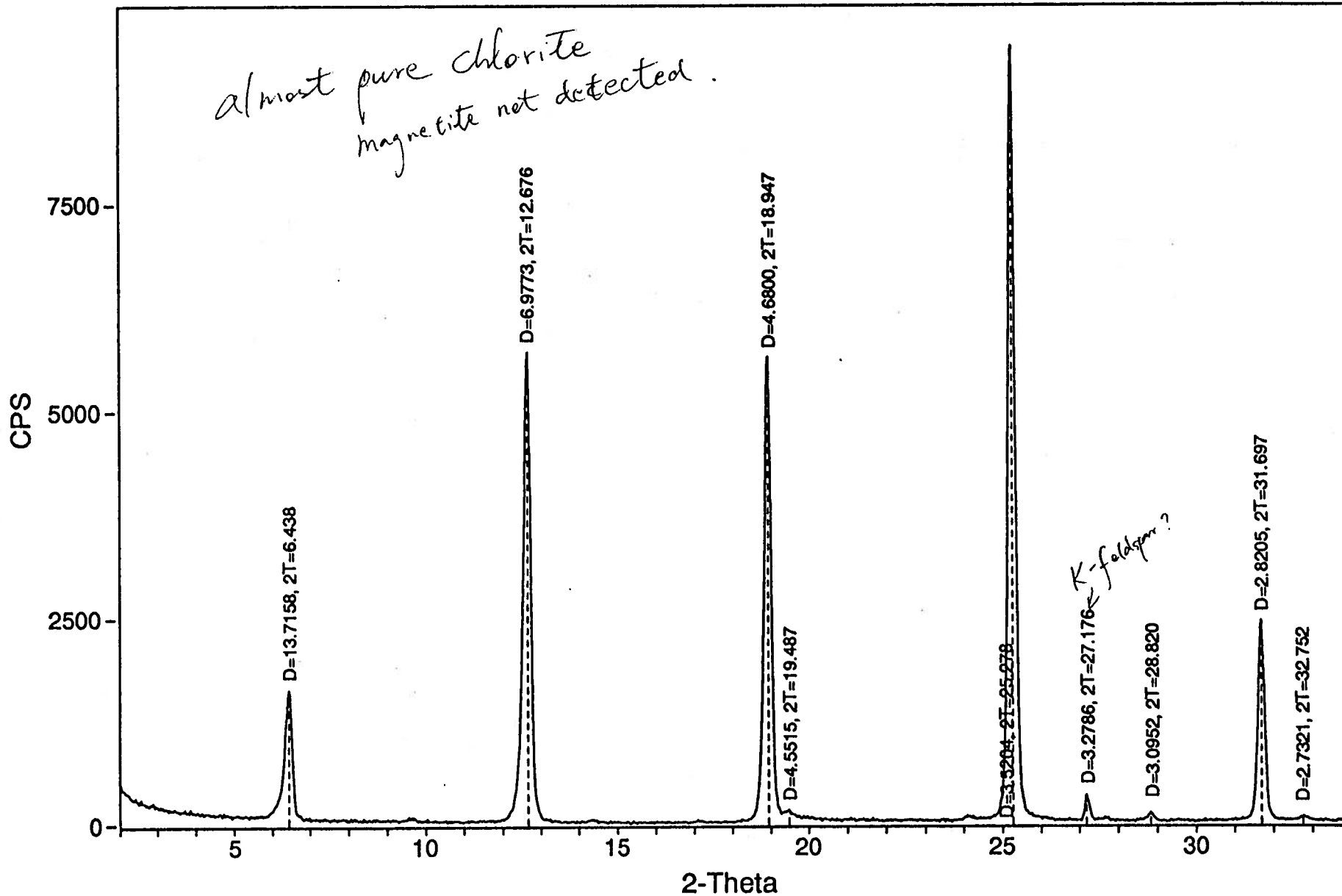
### **X-Ray Diffractograms of Mineral Reactants**







*almost pure chlorite  
magnetite not detected.*

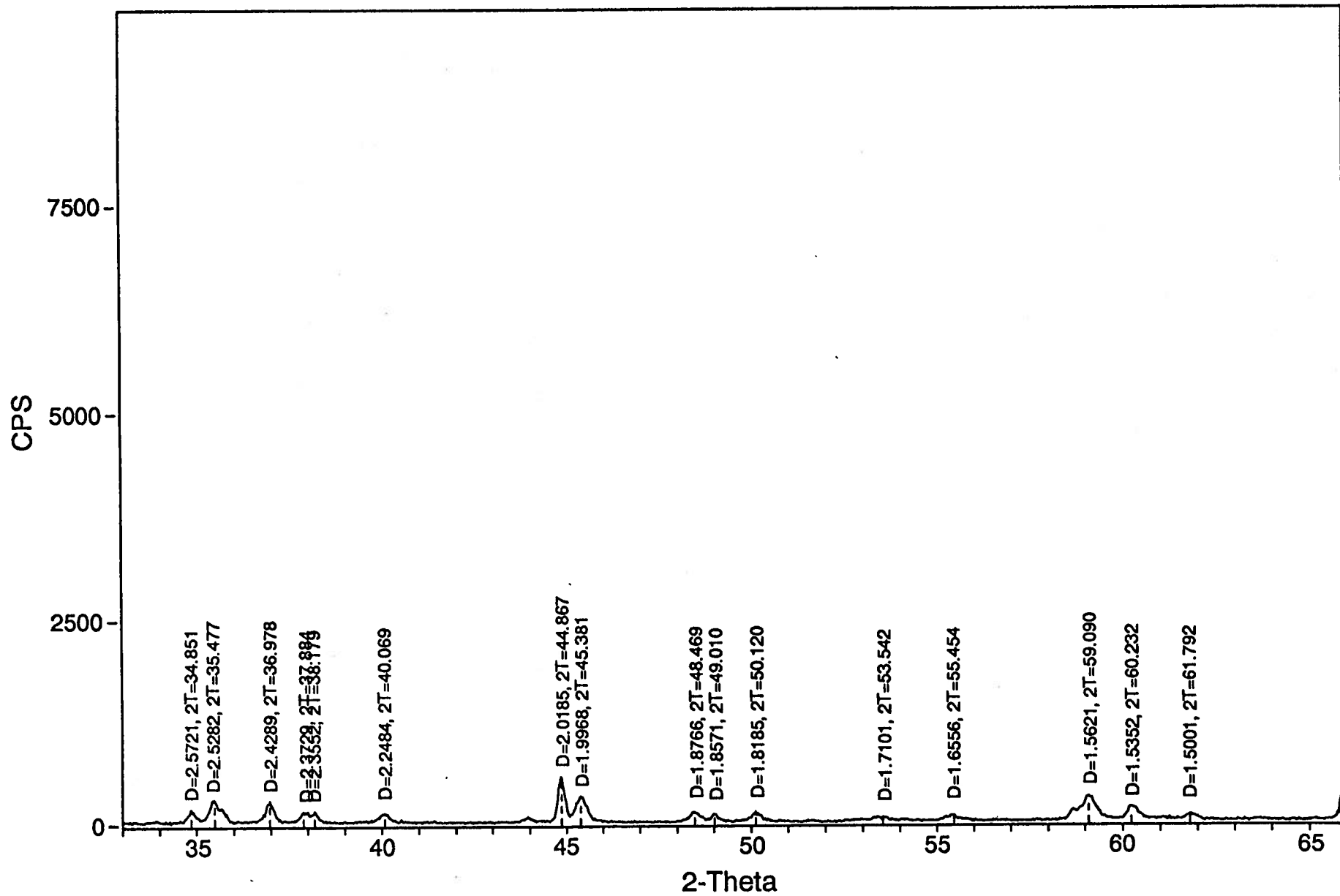


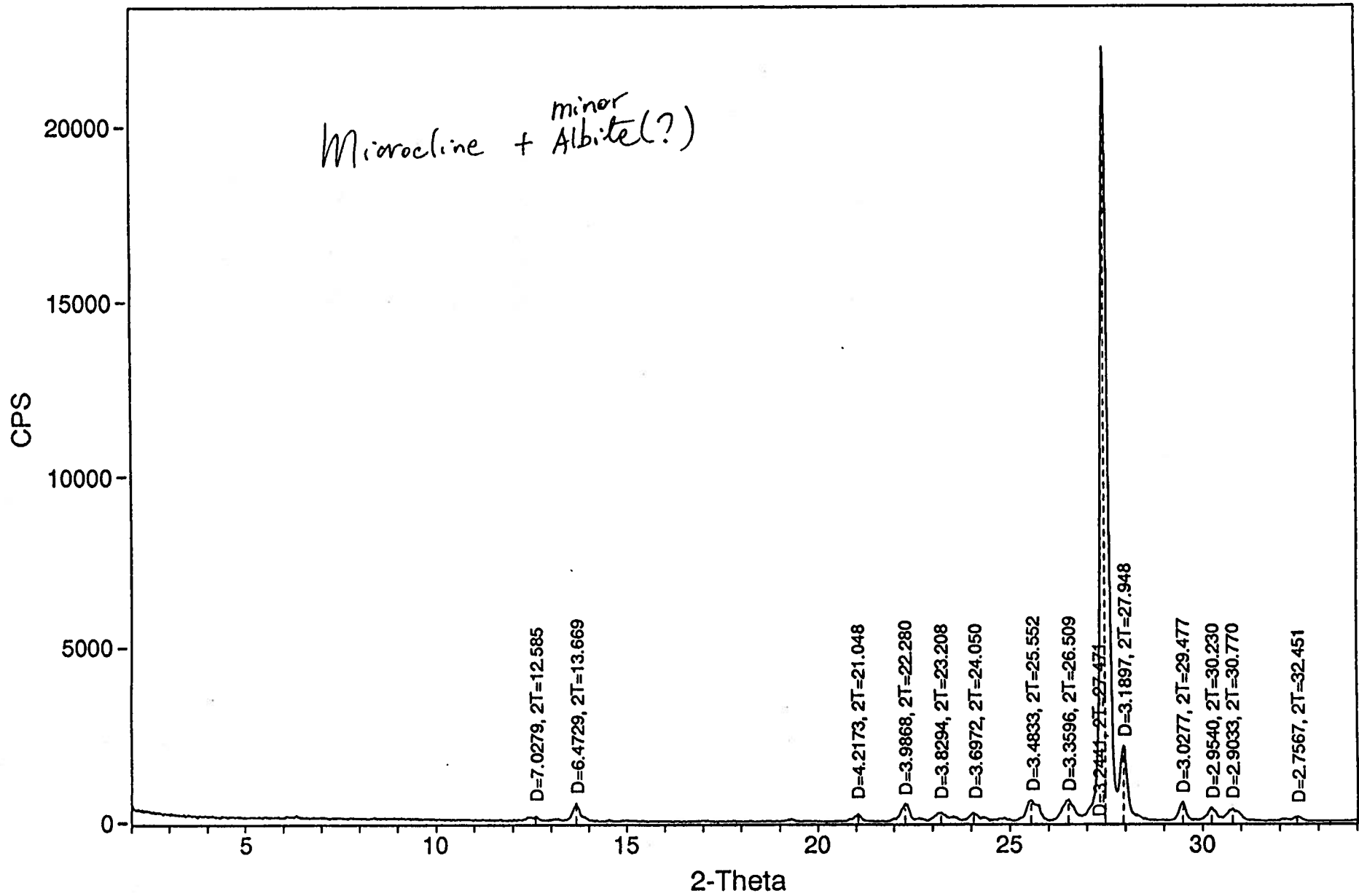
ID: C:\CO2\CLINO.MDI: CO2 Clinochlore

File: CLINO.MDI

Scan: 2-65.99/.03/1/#2134, Anode:CU

Zero=0.0



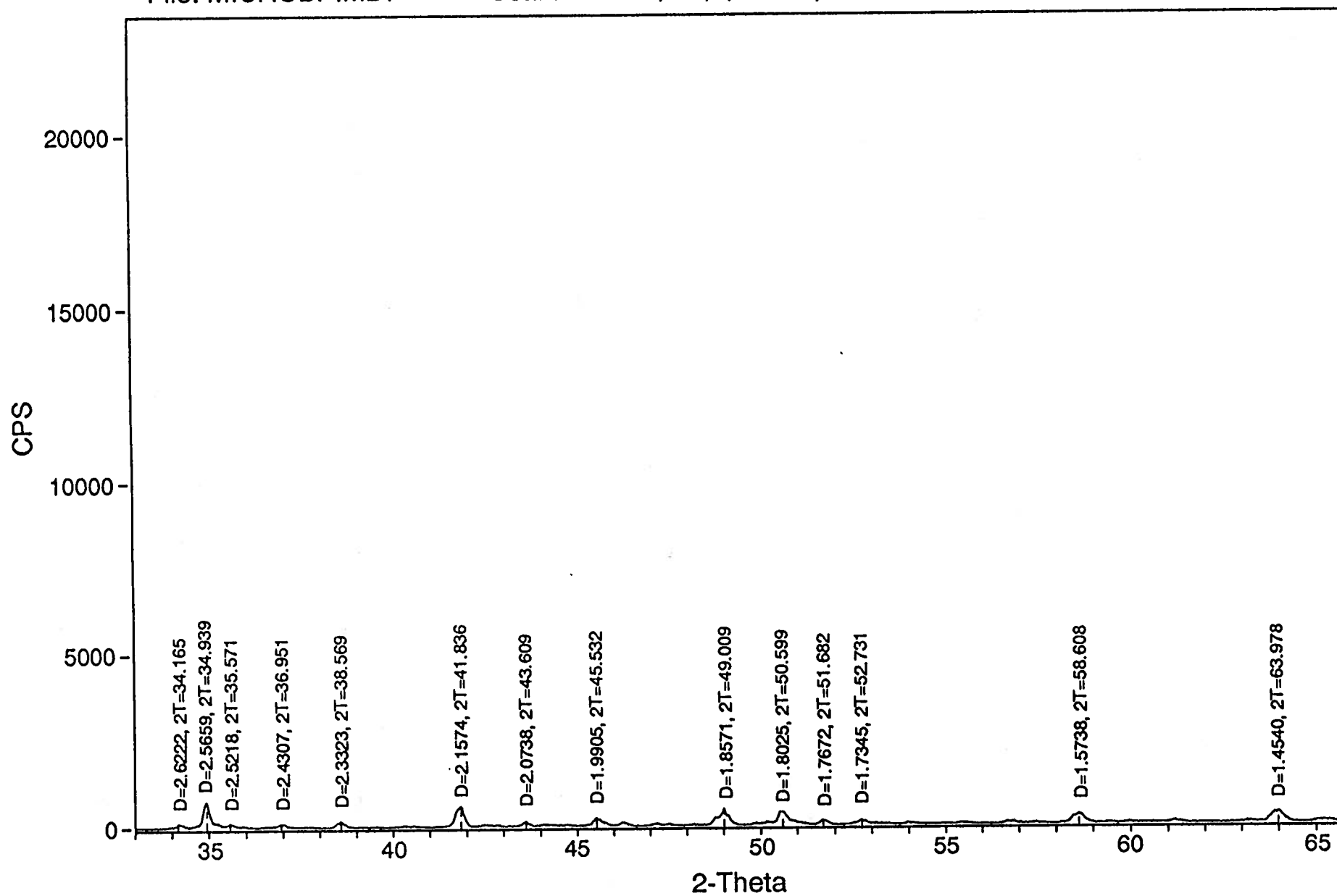


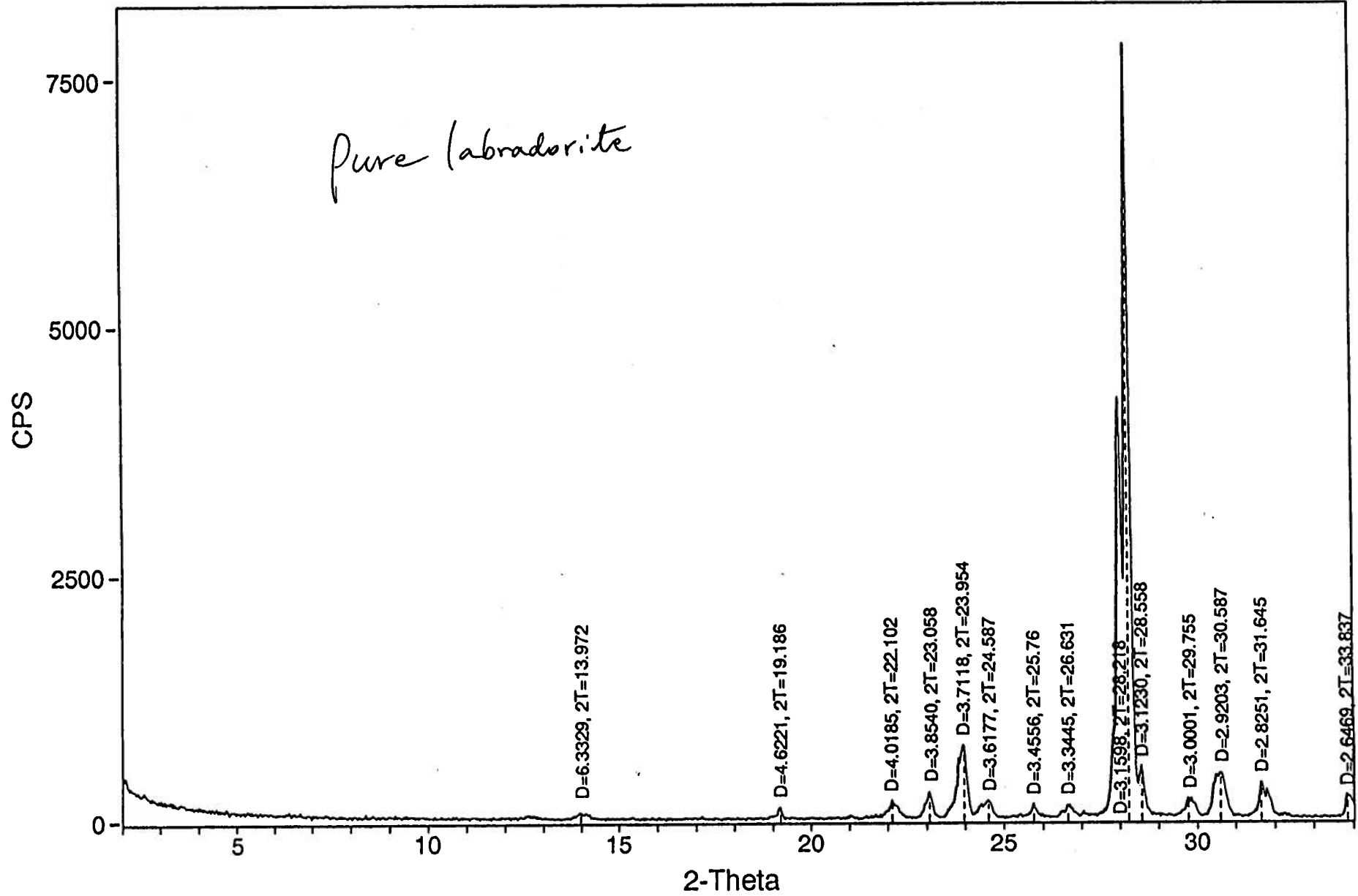
ID: C:\CO2\MICROBP.MDI: Microcline Back Pack

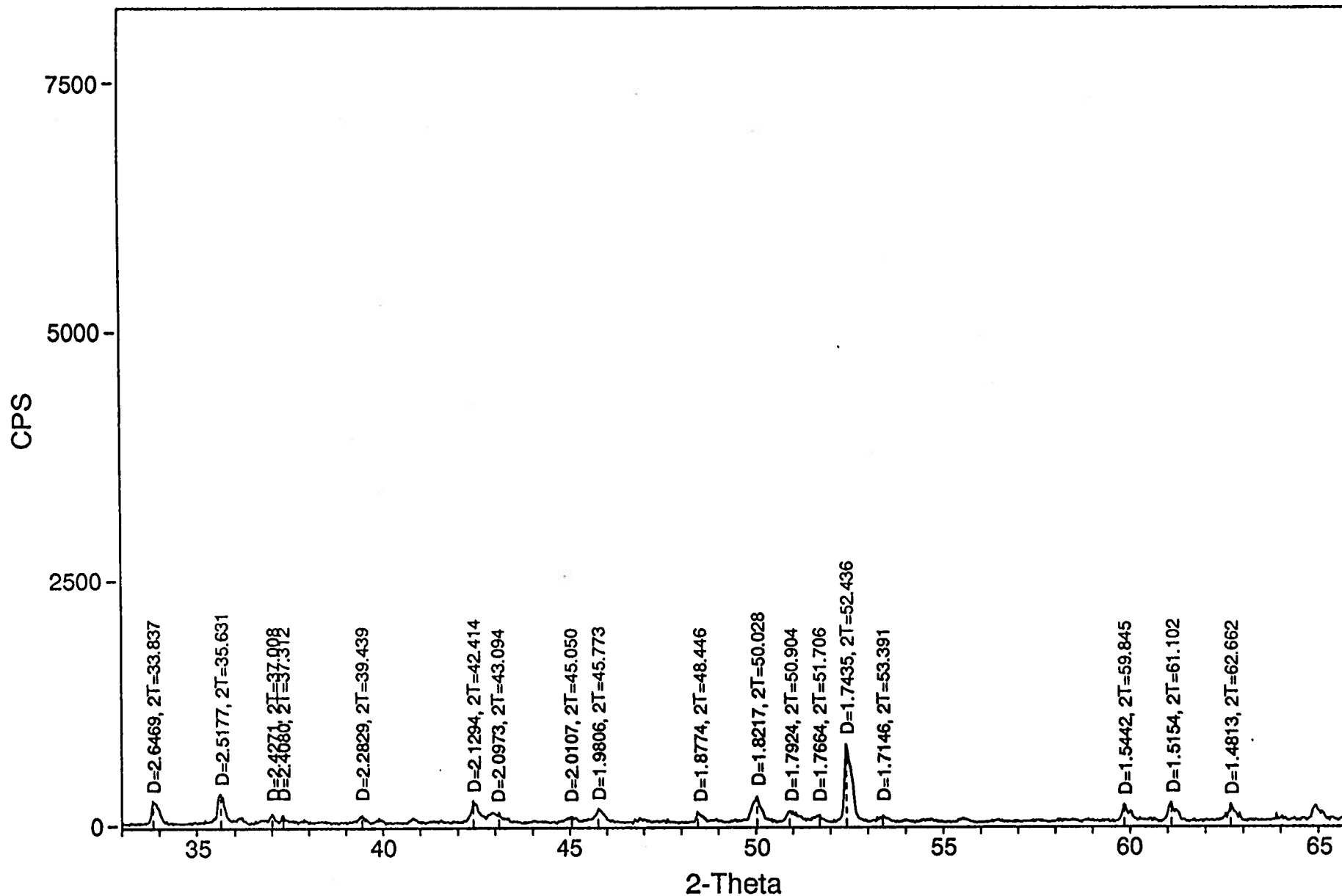
File: MICROBP.MDI

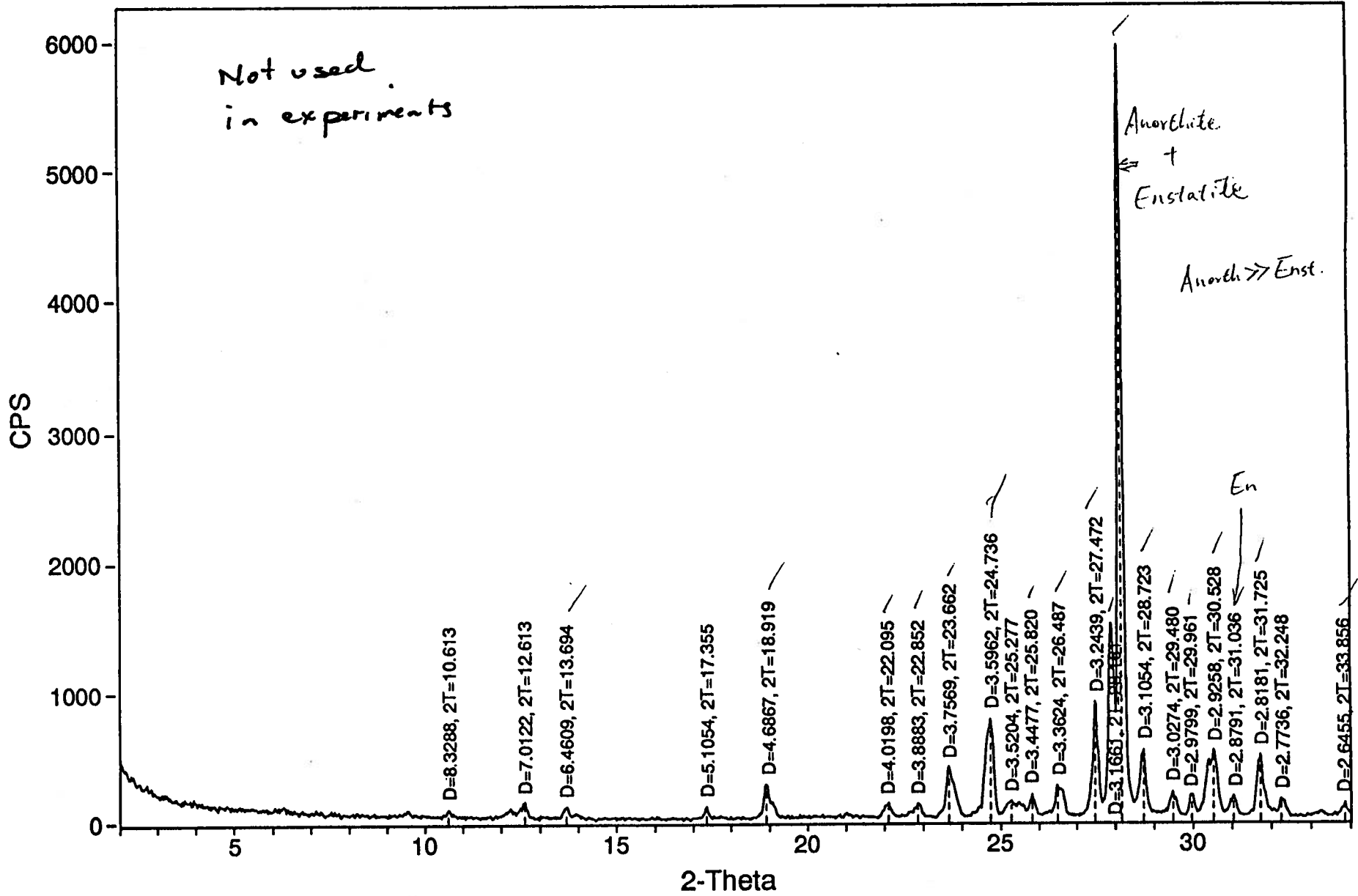
Scan: 2-65.99/.03/1/#2134, Anode:CU

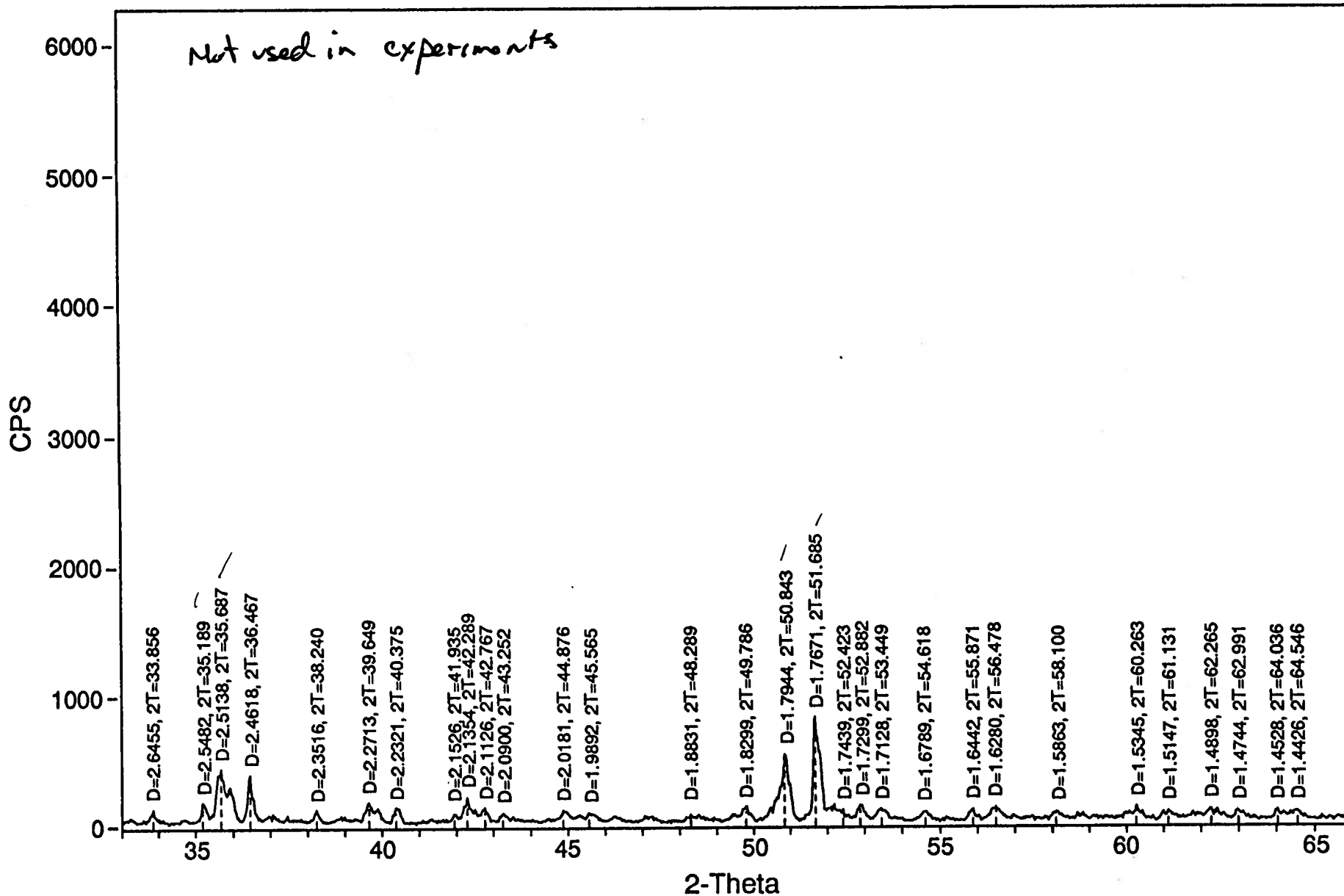
Zero=0.0



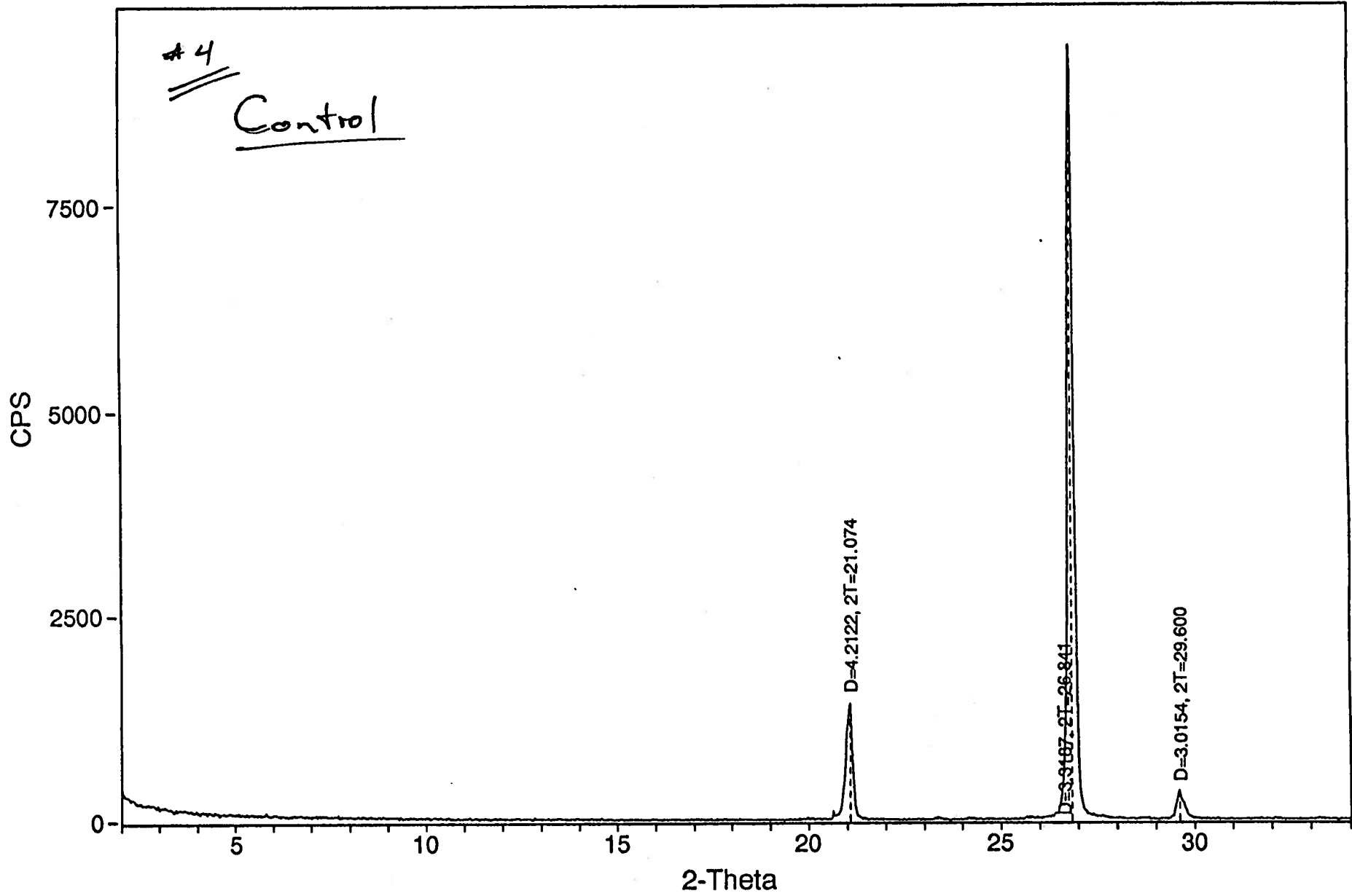


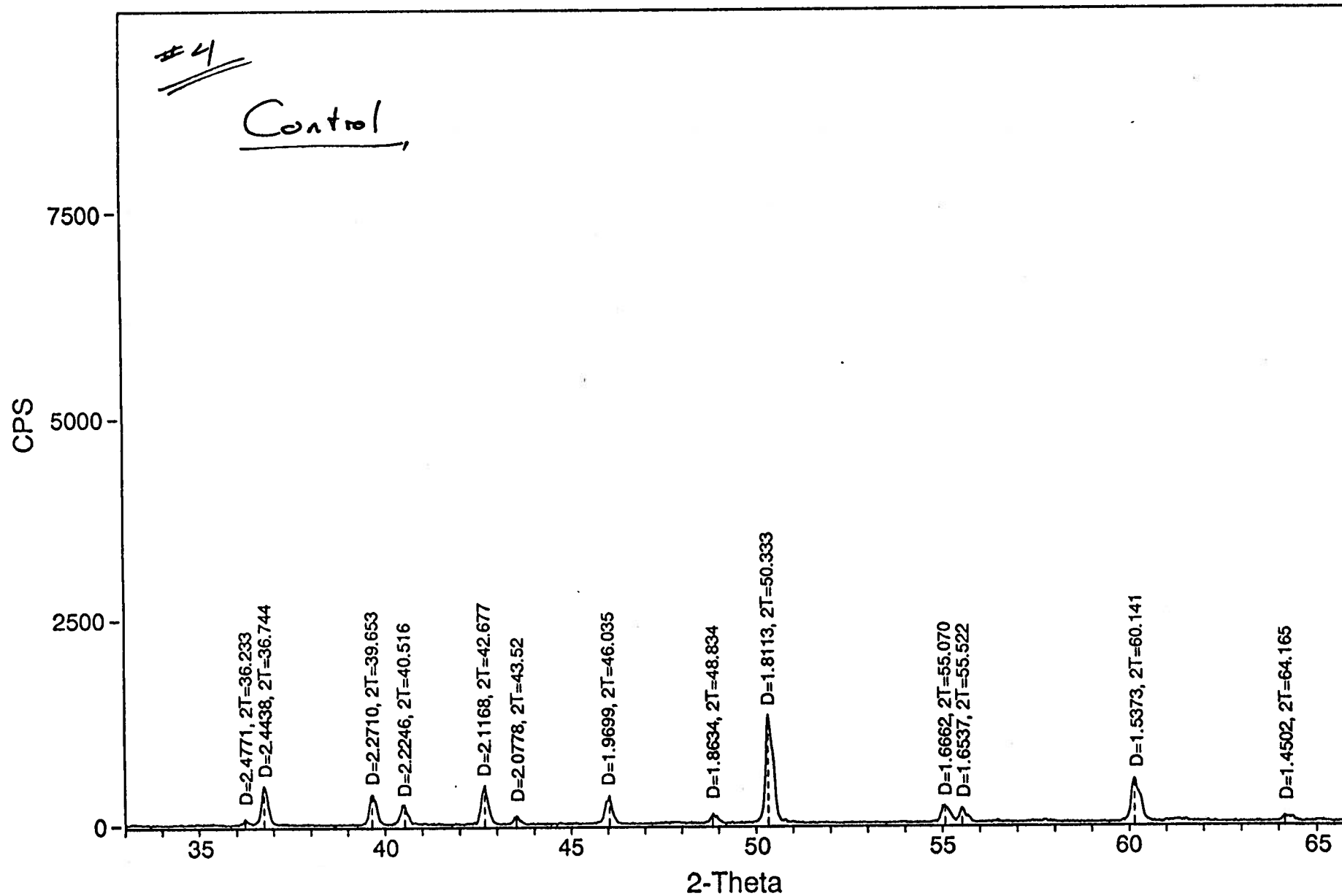






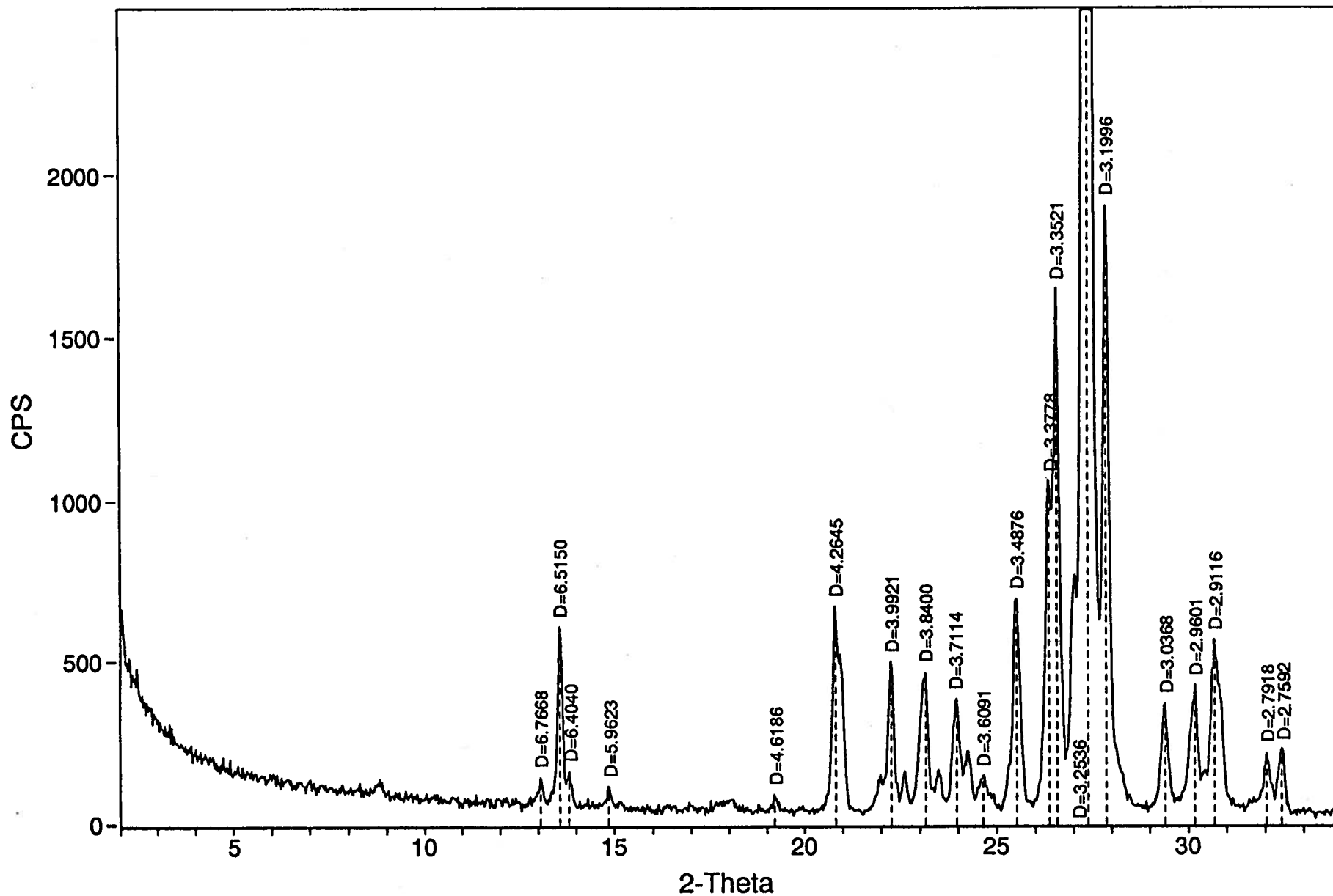


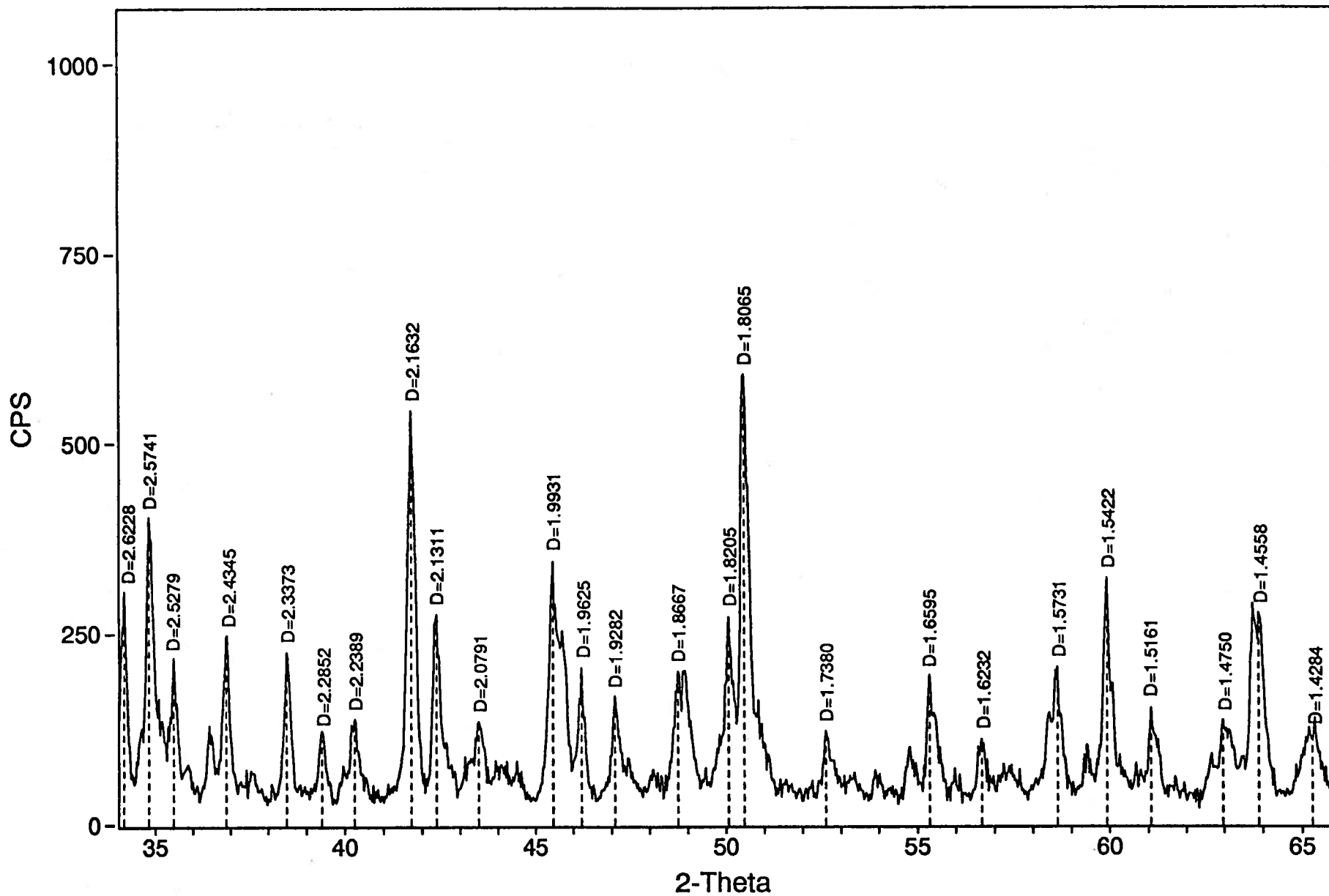


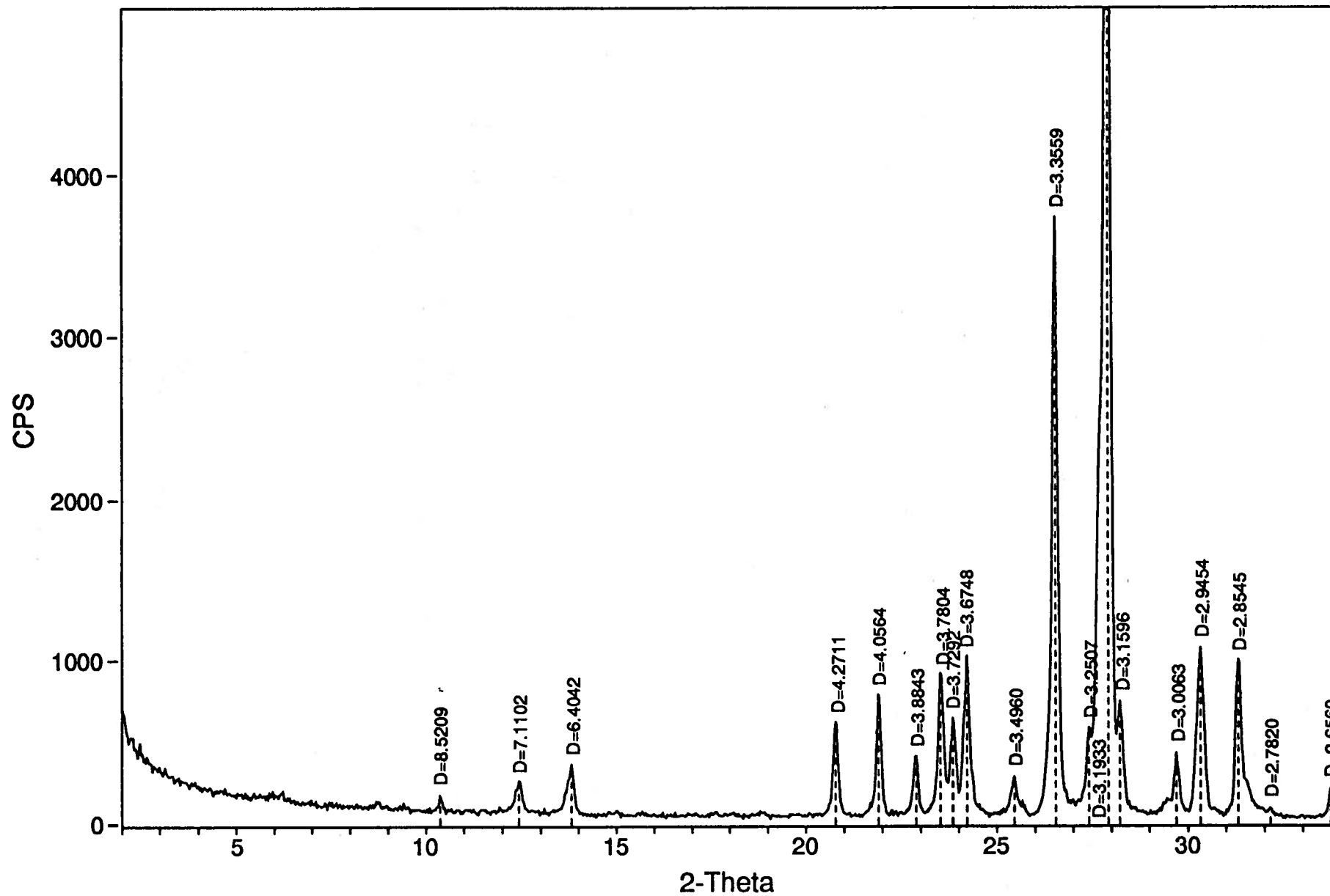


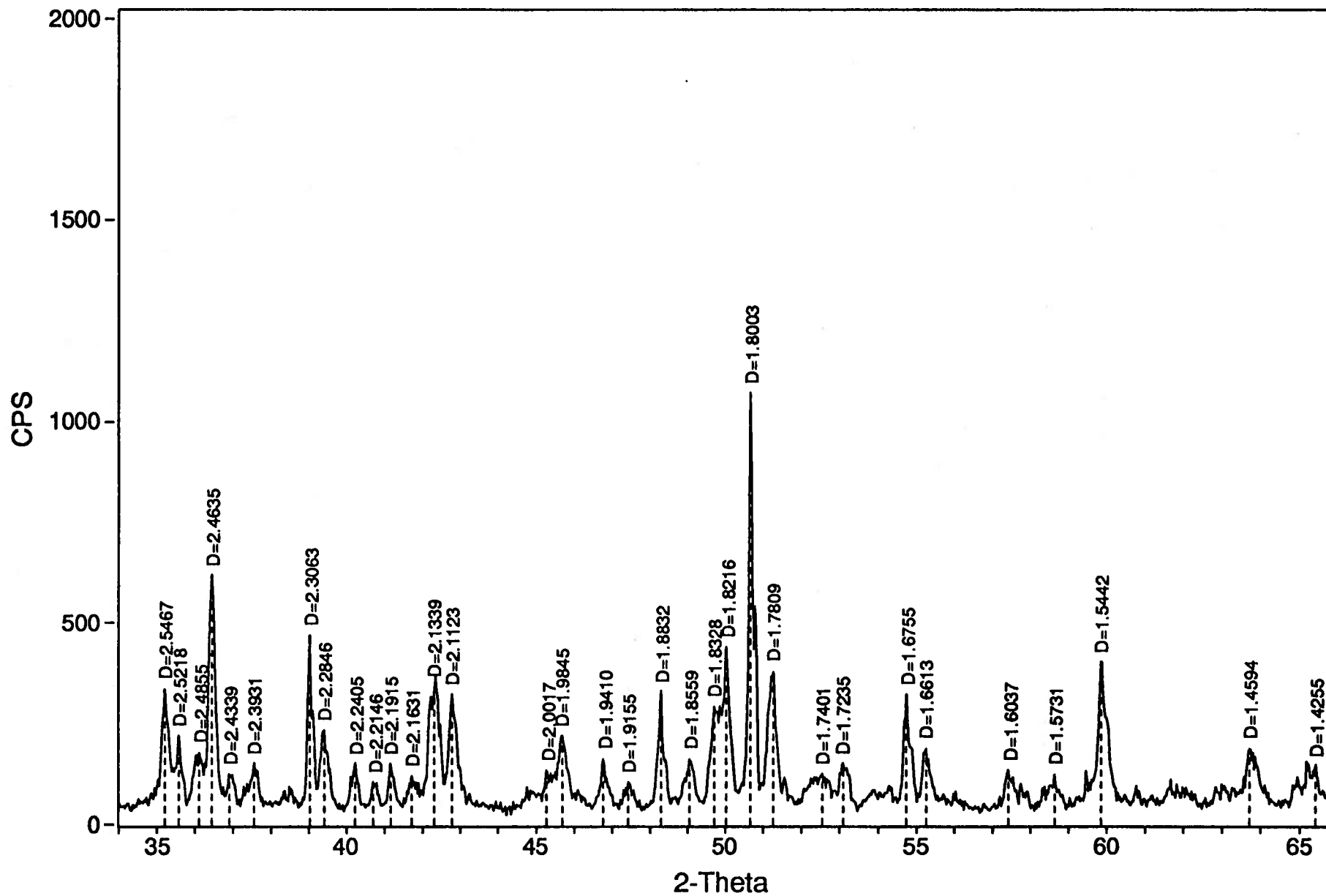
## **APPENDIX 11.6.2**

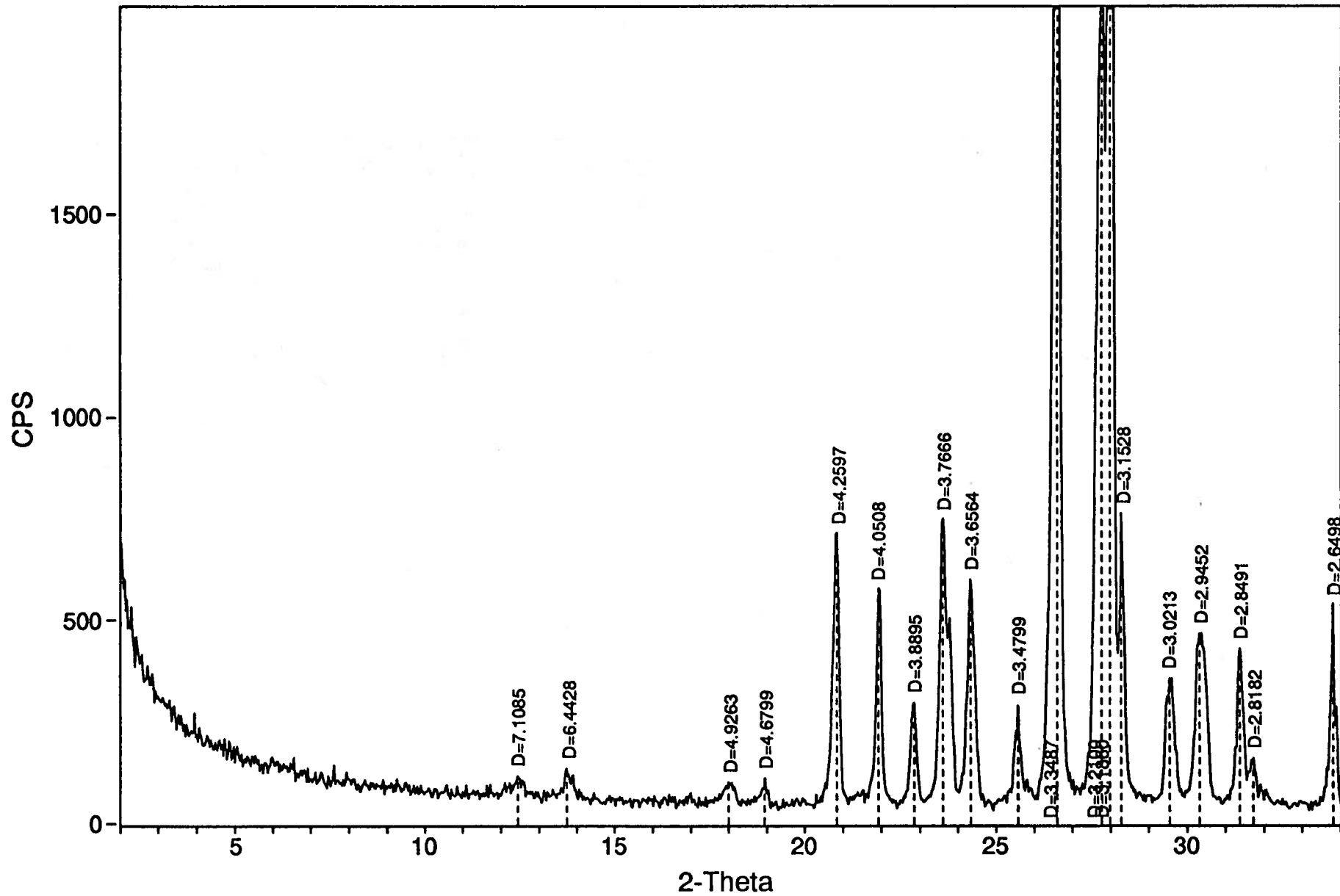
### **X-Ray Diffractograms of Reaction Products**



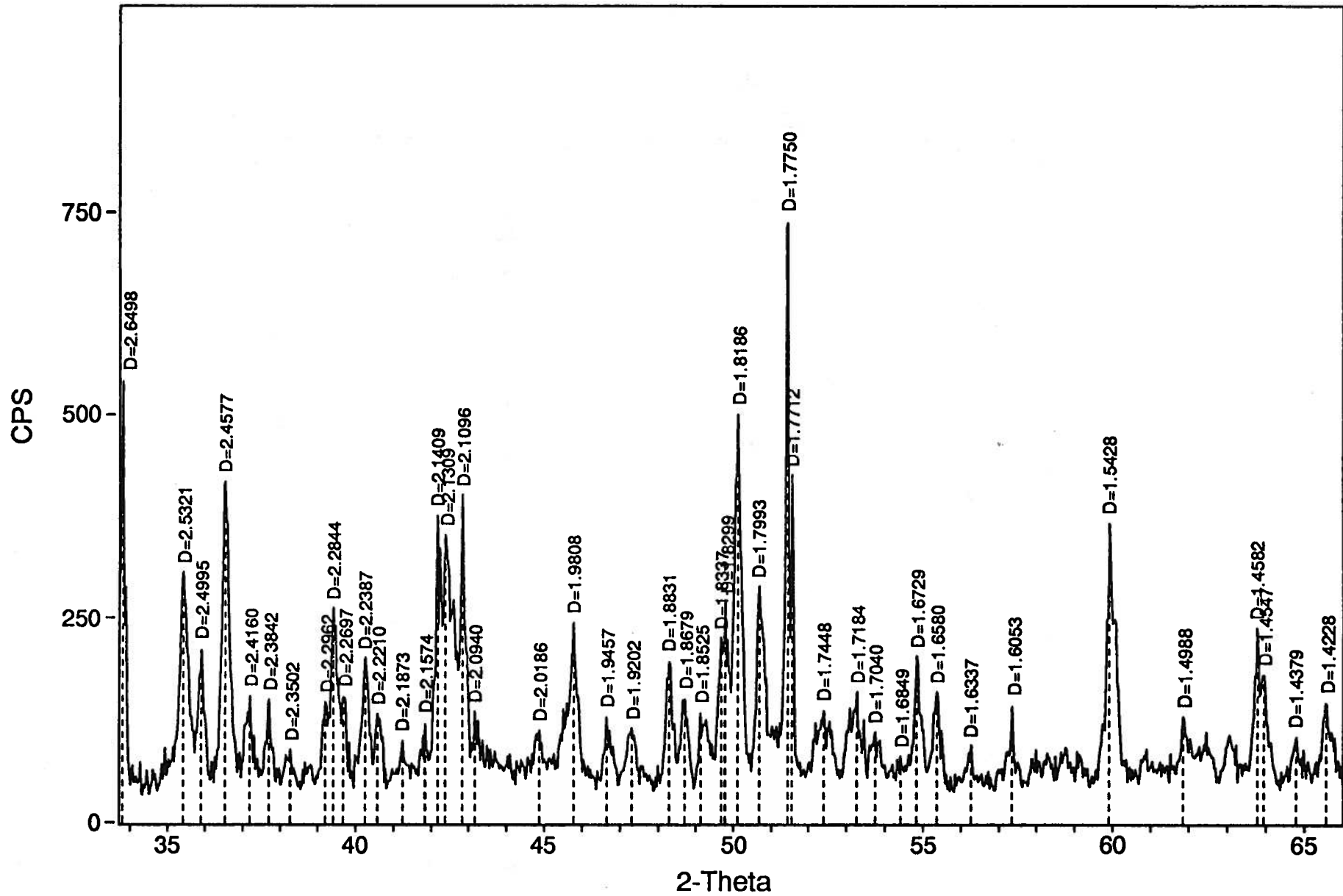


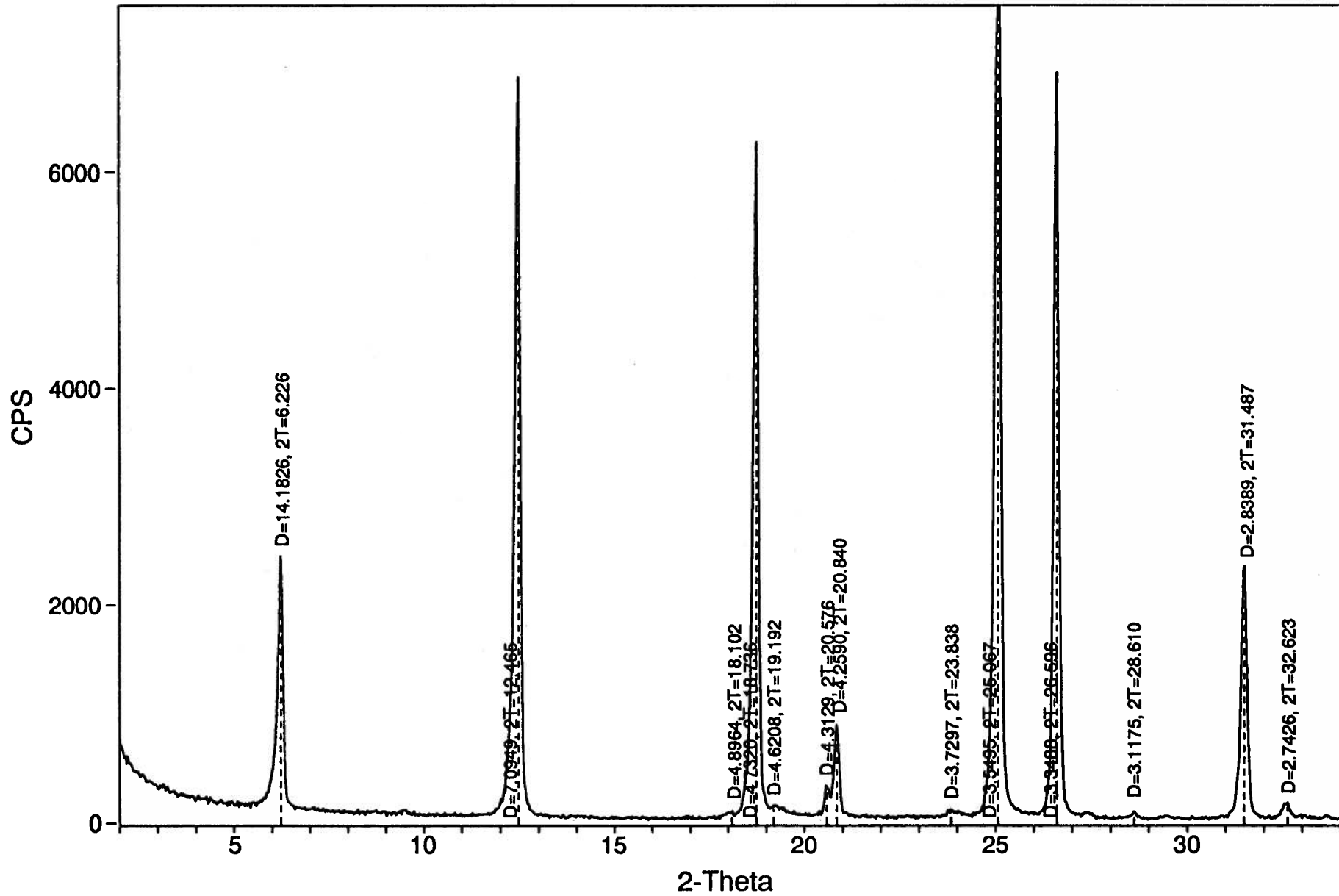


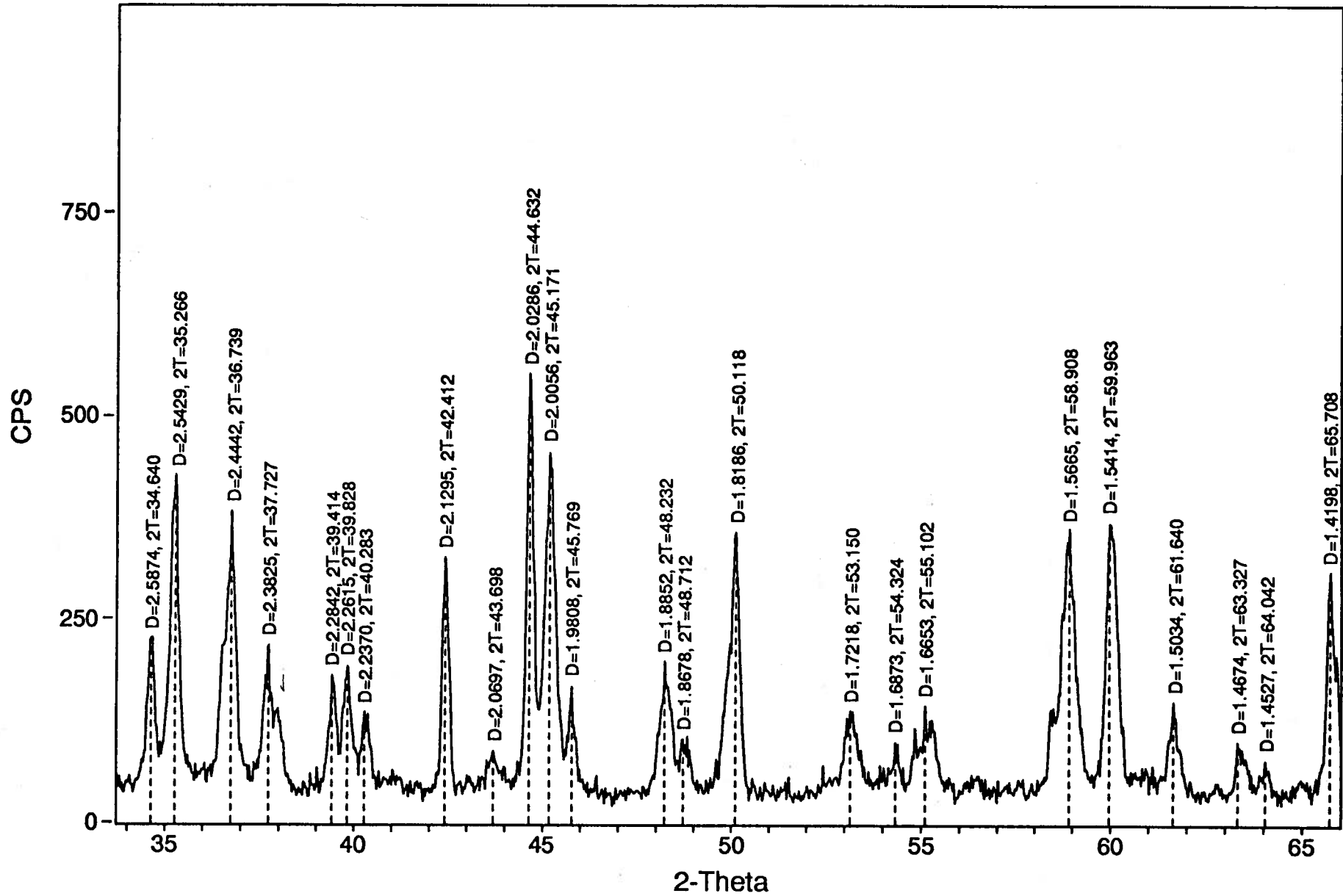












ID: C:\CO2\POST437.MDI: Postrun Autoclave 437

File: POST437.MDI

Scan: 2-65.99/.03/1/#2134, Anode:CU

Zero=0.0

